

Draft Environmental Impact Statement

Northern San Juan Basin Coal Bed Methane Project
Air Quality Impact Assessment Technical Support Document



U.S. Department of Interior
Bureau of Land Management
San Juan Field Office



U.S. Department of Agriculture
Forest Service
San Juan National Forest

June 2004

**Air Quality Impact Assessment Technical Support Document
Northern San Juan Basin Coalbed Methane Environmental Impact Statement**

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List of Acronyms

| | |
|------------------|-----------------------------------------------------------------------------------------------------------------|
| ANC | acid neutralizing capacity |
| AQRV | air quality related value(s) |
| BLM | USDI-Bureau of Land Management |
| BTEX | benzene, toluene, ethyl benzene and xylene |
| CALMET | California Meteorological Model; a diagnostic meteorological model used within the CALPUFF modeling system |
| CALPUFF | California Puff Model; a non-steady-state puff dispersion modeling system |
| CBM | coal bed methane |
| CDPHE-APCD | Colorado Department of Public Health and Environment – Air Pollution Control Division |
| CFR | Code of Federal Regulations |
| CO | carbon monoxide |
| DEM | digital elevation model |
| dv | deciview |
| EIS | Environmental Impact Statement |
| EPA | U.S. Environmental Protection Agency |
| EROS | Earth Resources Observation System |
| FAA | Federal Aviation Administration |
| FR | Federal Register |
| FLAG | Federal Land Managers' Air Quality Related Values Workgroup |
| ft | foot/feet |
| g/hp-hr | gram(s) per horsepower per hour |
| HAP | hazardous air pollutant(s) |
| HNO ₃ | nitric acid |
| hp | horsepower |
| hr | hour(s) |
| IMPROVE | Interagency Monitoring of PROtected Visual Environments |
| IWAQM | Interagency Workgroup on Air Quality Models |
| ISCST3 | Industrial Source Complex – Short Term atmospheric dispersion model |
| kg/ha-yr | kilogram(s) per hectare per year |
| km | kilometer(s) |
| lb/hr | pounds per hour |
| m | meter(s) |
| MACT | maximum achievable control technology |
| MEI | maximally exposed individual |
| MESOPUFF II | Mesoscale Puff Model, version 2; a non-steady-state, short term, regional scale puff dispersion modeling system |
| MLE | most likely exposed |
| MMBtu/hr | million British thermal units per hour |
| MM4 | Mesoscale Model (version 4) |
| MM5 | Mesoscale Model (version 5) |
| N/A | not applicable |
| NAAQS | National Ambient Air Quality Standards |
| NEPA | National Environmental Policy Act |

List of Acronyms (continued)

| | |
|------------------------------|----------------------------------------------------------------------------|
| NH ₃ | ammonia |
| NMED-AQB | New Mexico Environment Department – Air Quality Bureau |
| NMOGA | New Mexico Oil and Gas Association |
| NSJB | Northern San Juan Basin |
| NO ₂ | nitrogen dioxide |
| NO ₃ ⁻ | nitrate ion |
| NOx | oxides of nitrogen |
| NWS | National Weather Service |
| PM _{2.5} | fine particulate matter (less than 2.5 microns in effective diameter) |
| PM ₁₀ | inhalable particulate matter (less than 10 microns in effective diameter) |
| POSTUTIL | a post-processing analysis program used within the CALPUFF modeling system |
| ppb | parts per billion |
| ppm | parts per million |
| PSD | prevention of significant deterioration |
| RAWS | Remote Automatic Weather Station |
| RFS | reasonably foreseeable sources |
| RMP | Resource Management Plan |
| SO ₂ | sulfur dioxide |
| SO ₄ ⁼ | sulfate ion |
| SUIT | Southern Ute Indian Tribe |
| t/yr | ton(s) per year |
| USDA | United States Department of Agriculture |
| USDI | United States Department of the Interior |
| USGS | United Stated Geological Survey |
| UTM | Universal Transverse Mercator |
| VOC | volatile organic compounds |
| µeq/l | microequivalent(s) per liter |
| µg/m ³ | microgram(s) per cubic meter |

1.0 Introduction

This document describes the technical approach that was used for evaluating potential near field and far field air quality impacts associated with proposed increases in natural gas production within the San Juan Basin north of the Southern Ute Indian Reservation in southwestern Colorado. The increase in natural gas production in this area would be from both conventional and coal bed methane (CBM) wells.

This document is organized in the following manner. Section 2 presents the regulatory framework for this proposed development. Section 3 provides a detailed description of the emission inventories that were developed as part of this study, as well as a discussion of the criteria that were used to establish the emission inventories for the far field impact analysis. Section 4 presents information on background air quality levels within the study area, and Section 5 presents information on the meteorological data that was used in the analysis. Section 6 presents the modeling methodology for the near field analysis, as well as the cumulative far field analysis for air quality related values (AQRV) in adjacent Class I Areas. Section 7 summarizes the potential impacts for both the near and far field analyses. Finally, Section 8 describes potential mitigation measures which could be implemented to further reduce the predicted visibility impacts from actually occurring.

1.1 Project Description and Alternatives

The Northern San Juan Basin (NSJB) Coalbed Methane Environmental Impact Statement (EIS) Study Area encompasses approximately 125,000 acres of public and private land just north of the Southern Ute Indian Reservation northern boundary in southeastern La Plata County and southwestern Archuleta County, Colorado. Figure 1-1 presents a map indicating the extent of the cumulative far field air quality impact analysis area.

Approximately 12,500 conventional and CBM wells have been constructed throughout the entire study area to date. Approximately 11,000 new wells would be constructed throughout the entire study area, including up to 500 new wells under the NSJB EIS maximum development scenario. Table 1-1 presents a summary of NSJB EIS alternatives considered and the associated number of wells that would be constructed. In this analysis, emission inventories were developed for all five alternatives, although quantitative air quality impact analyses were conducted only for Alternatives 1 (Proposed Action), 2 (Maximum Development) and 5 (No Action).

Figure 1-1. Map of the Study Area

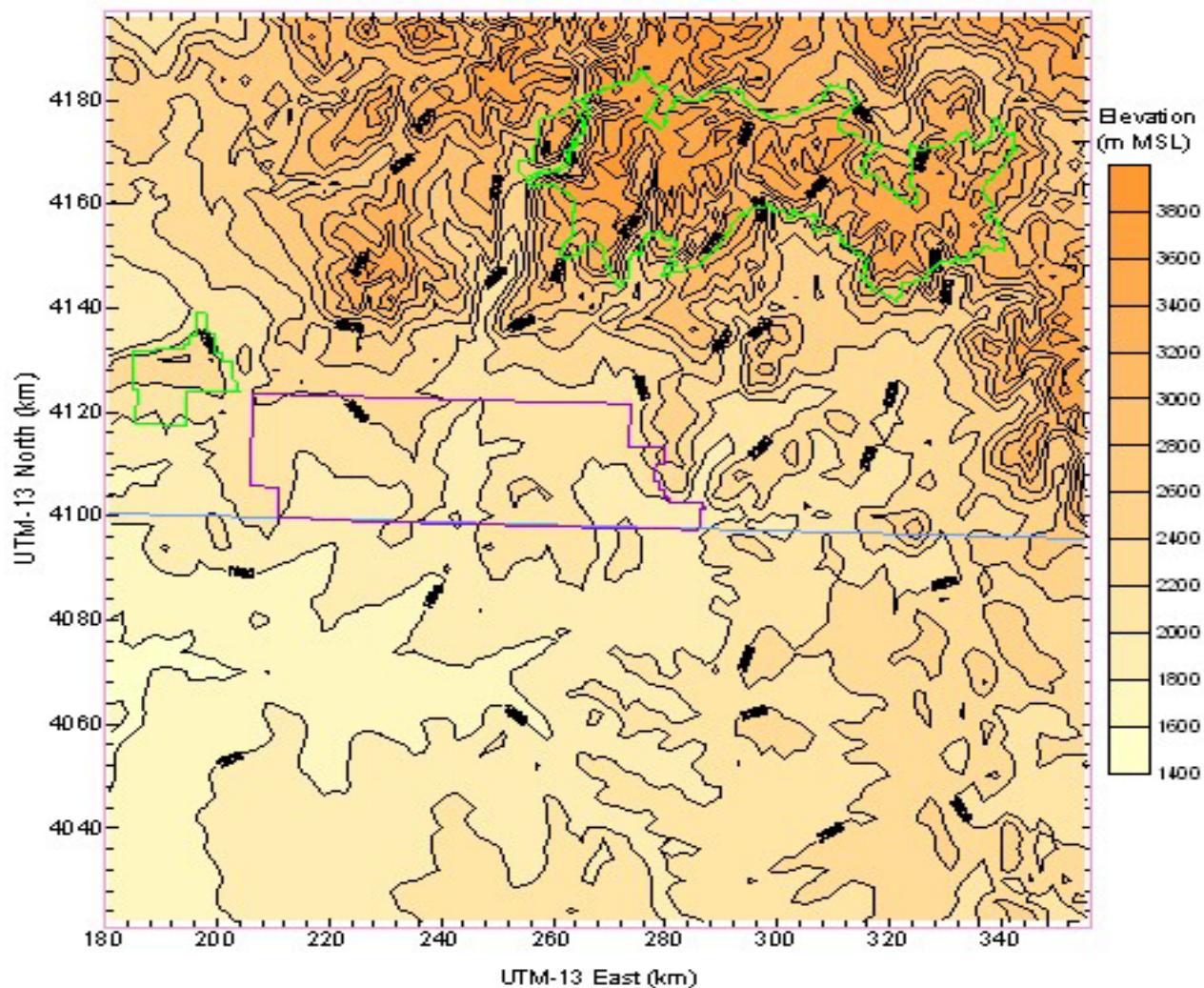


Table 1-1. List of Alternatives Considered

| Alternative | Description | Number of Wells |
|-------------|-------------------------------------------------------------------|-----------------|
| 1 | Industry's Proposed Action | 296 |
| 2 | Maximum Development | 522 |
| 3 | No Well Development in the HD Mountains Inventoried Roadless Area | 212 |
| 4 | Continuation of Current Management Direction | 185 |
| 5 | No Action | 118 |

2.0 Regulatory Framework

The U.S. Environmental Protection Agency (EPA) establishes and revises the National Ambient Air Quality Standards (NAAQS) as necessary to protect public health and welfare, setting the absolute upper limits for specific air pollutant concentrations at all locations where the public has access. In addition, the State of Colorado may establish and implement similar standards which are more stringent than the NAAQS (such as the Colorado 3-hour [hr] sulfur dioxide [SO₂] ambient air quality standard). Although the EPA recently revised both the ozone and the fine particulate matter (PM_{2.5}) NAAQS, these revised limits will not be implemented by the Colorado Department of Public Health and Environment – Air Pollution Control Division (CDPHE-APCD) until the Colorado State Implementation Plan is formally approved by EPA. In the meantime, EPA is responsible for implementing and enforcing these revised standards. This analysis of potential CBM development impacts must demonstrate compliance with all applicable local, state, tribal and federal air quality standards. Table 2-1 presents a summary of the applicable EPA and CDPHE-APCD air quality standards.

Table 2-1. Applicable Ambient Air Quality Standards and PSD Increment Values

| Pollutant | Averaging Time | National Ambient Air Quality Standards ($\mu\text{g}/\text{m}^3$) | Colorado Ambient Air Quality Standards ($\mu\text{g}/\text{m}^3$) | PSD Class I Increment ($\mu\text{g}/\text{m}^3$) | PSD Class II Increment ($\mu\text{g}/\text{m}^3$) |
|-------------------|----------------|---------------------------------------------------------------------|---------------------------------------------------------------------|----------------------------------------------------|-----------------------------------------------------|
| carbon monoxide | 1-hr | 40,000 | 40,000 | N/A | N/A |
| | 8-hr | 10,000 | 10,000 | N/A | N/A |
| nitrogen dioxide | Annual | 100 | 100 | 2.5 | 25 |
| ozone | 1-hr | 235 | 235 | N/A | N/A |
| | 8-hr | 157 | 157 | N/A | N/A |
| PM ₁₀ | 24-hr | 150 | 150 | 8 | 30 |
| | Annual | 50 | 50 | 4 | 17 |
| PM _{2.5} | 24-hr | 65 | 65 | N/A | N/A |
| | Annual | 15 | 15 | N/A | N/A |
| sulfur dioxide | 3-hr | 1,300 | 700 | 25 | 512 |
| | 24-hr | 365 | 365 | 5 | 91 |
| | Annual | 80 | 80 | 2 | 20 |

$\mu\text{g}/\text{m}^3$ – micrograms per cubic meter

N/A – not applicable

The air quality of the EIS Study Area is in attainment with all ambient air quality standards, as demonstrated by the relatively low measured concentration levels (see Section 4 for a discussion of existing air quality in the region). Given the EIS Study Area's current attainment status, future development projects (under any alternative) which have the potential to emit more than 250 tons per year (t/yr) of any criteria pollutant (or certain listed sources that have the potential to emit more than 100 t/yr) would be required to submit a pre-construction prevention of significant deterioration (PSD) Permit Application, including a regulatory PSD Increment Consumption Analysis under the federal New Source Review and permitting regulations. Development projects subject to the PSD regulations must also demonstrate the use of Best Available Control Technology and show that the combined impacts of all applicable sources would not exceed the PSD increments for nitrogen dioxide (NO_2), inhalable particulate matter (PM_{10}) or SO_2 . Finally, the permit applicant must also demonstrate that cumulative impacts from all existing and proposed sources would comply with the applicable ambient air quality standards throughout the operational lifetime of the permit applicant's project.

In addition, a regulatory PSD Increment Consumption Analysis may be conducted at any time by the CDPHE-APCD or EPA, in order to demonstrate that the applicable PSD increment has not been exceeded by all applicable major or minor increment consuming emission sources. The determination of PSD increment consumption is a legal responsibility of the applicable air quality regulatory agencies (with EPA oversight).

For example, the CDPHE-APCD (1999) conducted a detailed review of NO_2 PSD increment consumption in southwest Colorado, indicating that Class I increment values "are probably not violated" at the Mesa Verde National Park or the Weminuche Wilderness Area, but that preliminary results "suggest that there is one isolated hot spot in La Plata County where there is an apparent Class II PSD increment violation." The CDPHE-APCD worked closely with the emission source operator to better understand the specific situation, and has resolved the source-specific PSD Class II increment situation.

Mandatory federal Class I areas were designated by the U.S. Congress on August 7, 1977, including those existing wilderness areas greater than 5,000 acres in size and national parks greater than 6,000 acres in size. All other locations in the country where the ambient air quality is within the NAAQS (including attainment and unclassified areas) are designated as PSD Class II areas with less stringent requirements. In addition, sources subject to the PSD permit review procedures are required to demonstrate that impacts to AQRVs will be below Federal Land Managers' Air Quality Related Values Workgroup (FLAG) "Limits of Acceptable Change" (FLAG 2000). The AQRVs to be evaluated include degradation of visibility, deposition of acidic compounds in mountain lakes and effects on sensitive flora and fauna within the PSD Class I areas.

Therefore, most of the EIS Study Area is currently designated as PSD Class II, while Mesa Verde National Park and the Weminuche Wilderness Area are protected by more stringent NO_2 , PM_{10} , and SO_2 PSD Class I increment thresholds, as shown in Table 2-1.

In addition, the CDPHE-APCD also requires various different pre-construction and operation permits including:

- any emission source with the potential to emit air pollutants in excess of 2 t/yr must submit an Air Pollution Emission Notice to CDPHE-APCD;
- all emission sources with the potential to emit oxides of nitrogen (NOx) or carbon monoxide (CO) in excess of 10 t/yr, or 5 t/yr of PM₁₀, are required to obtain a permit before construction can begin;
- all emission sources with potential emissions in excess of 100 t/yr of CO, 40 t/yr of NOx, or 15 t/yr of PM₁₀ must also include a new source modeling analysis in their permit application. CDPHE-APCD (2002) modeling guidelines specify the requirements for conducting modeling, including cumulative impact analyses;
- all emission sources with the potential to emit any “criteria” air pollutant in excess of 50 t/yr must also provide the opportunity for the public to comment on the permit application; and
- a Title V (40 CFR Part 70) operating permit is required for all sources with the potential to emit air pollutants in excess of 100 t/yr.

Since these pre-construction and operating permit programs are included in the Colorado State Implementation Plan, they have been approved (and are therefore enforceable) by EPA.

This USDI – Bureau of Land Management (BLM) National Environmental Policy Act (NEPA) analysis compares potential air quality impacts from the Proposed Action and Alternatives to applicable ambient air quality standards, PSD increments, and AQRVs, but it does not represent a regulatory air quality permit analysis. Comparisons to the PSD Class I and II increments are intended to evaluate a “threshold of concern” for potentially significant adverse impacts, but do not represent a regulatory PSD Increment Consumption Analysis.

3.0 Emission Inventory Development

This section presents data regarding emission inventories that were developed as part of the air quality impact analysis. Emission inventories were developed to evaluate air quality effects from production activities in both the near field (adjacent to the development) and far field (PSD Class I Areas). Also, estimates of air quality impacts from construction were estimated based on an analysis that was conducted as part of the Southern Ute Indian Tribe (SUIT) EIS (BLM 2000).

Separate emission inventories were developed for both the near field and the far field cumulative impact analyses. The emission inventories addressed three groups of sources: 1) proposed action (and alternatives); 2) existing sources; and 3) other reasonably foreseeable sources (RFS). Emissions from existing sources were treated differently in the near and far field modeling because of the different focus of these analyses. The purpose of the near field analysis was to compare predicted concentrations to the NAAQS and PSD increments, and all existing sources were included in the modeling. The purpose of the far field analysis was to: 1) estimate total concentrations (modeled plus measured background concentrations) for comparison with the NAAQS in the two Class I Areas; 2) estimate potential PSD increment consumption from each alternative in the two Class I Areas; and 3) estimate the potential AQRV changes in the two Class I Areas. The calculation of potential AQRV impacts is referenced to measured existing conditions at the Mesa Verde National Park and Weminuche Wilderness Area Class I areas. Because of this approach, only those existing sources not represented by the measured background conditions were included in the far field AQRV impact analyses. Section 3.1 presents the emission inventories used in the near field analysis. Section 3.2 contains the inventories used in the cumulative far field analysis.

3.1 Near Field Emissions

3.1.1 Proposed Action and Alternatives

This subsection presents the development of the proposed action and alternative emission inventories, as well as quantification of potential emissions.

In the EIS Study Area, the primary sources of air pollutants emitted during the production phase are natural gas-fired compressors, small natural gas-fired heaters (used in conjunction with separation and dehydration units), and small natural gas-fired engines associated with well operations (pump jack engines). Compressors are used for the production and pipeline transport of natural gas produced by the wells. Small wellhead engines may be used for water disposal as well as other uses. The compressors and small engines would emit NO_x, CO, volatile organic compounds (VOC) and hazardous air pollutants (HAP). The heaters would emit small quantities of NO_x and CO. Other than the VOC emissions from the compressor engines, there would be negligible reactive hydrocarbon emissions associated with this development because of the nature of the produced gas.

At present, detailed site-specific engineering data are not available regarding the exact nature of equipment that would be used, or the exact locations where the equipment would be installed. For purposes of this air quality impact assessment, reasonable but conservative assumptions were made regarding these potential emission sources.

Criteria Pollutants

Emissions associated with the proposed project's operational phase will be almost totally due to added natural gas-fired compressors and small wellhead engines. Operators in the area provided estimates of additional compressor capacity requirements and general locations (regions) where additional compression might be installed. Because the new compressors and small wellhead engines would burn natural gas which contains no sulfur compounds, the only criteria pollutants emitted from these sources would be NOx, CO and small amounts of VOC. Quantitative estimates of these emissions were developed based on the compressor capacity (in horsepower, or hp), and appropriate emission factors for gas compressor engines (in grams per horsepower per hour, or g/hp-hr). The emission inventory was developed for typical maximum emissions. It was assumed that all of the new compressors and small wellhead engines would operate simultaneously for all hours of the year. This represents a conservative but upper bound of potential criteria pollutant emissions.

Emissions from Central Compression

In developing the emission inventory, some modeling assumptions were required. BLM provided assumed central compressor locations, along with the total capacity (hp) of each site; however, no detailed engineering designs have been developed. Therefore, assumptions were required to develop a physical description of each source prior to modeling. The first assumption was regarding the number of engines to be located at each central compressor facility. In order to ensure that the modeling was conservative, for those sites with a capacity in excess of 2,000 hp, total capacity was broken into smaller individual units. This was based on a review of previous central compressor facilities in the region to ensure that the calculated plume rise would be not overstated, which otherwise would have resulting in predicted concentrations being under estimated. Thus, the individual capacities listed in the emission inventory tables are reasonable assumptions, but should not be interpreted as the exact size of the equipment that would be installed. The next assumption made was the physical separation between sources. It was assumed that the individual compressor engines would be separated by 10 meters (m) or approximately 33 feet (ft).

These sources were explicitly included in the near field modeling, with stack parameters based on combustion calculations and engineering data from existing facilities.

Estimates of compressor pollutant emissions were based on the compressor requirements developed by the project proponents. Emissions were calculated based on the expected additional compressor capacity (hp) and appropriate emission factors for natural gas fired compressor engines (g/hp-hr). For compressor engines having a site rated capacity in excess of 500 hp, an emission factor of 1.5 g/hp-hr of NOx was used. This emission factor is assumed to be applicable for all

operating loads, and is representative of continuous operation using well-maintained, low emitting, or well-controlled compressor engines. It should also be noted that the total emission estimates reflect potential continuous operation, and that actual development emissions are likely to be less.

As described in a previous BLM natural gas development air quality impact assessment (BLM 1999), potential NOx control measures include:

Nonselective Catalytic Reduction. This control technology is applicable to relatively new engines and requires the installation of catalysts in the engine exhaust. The catalyst removes between 80 and 90 percent of the uncontrolled NOx emissions, for an operating emission rate of 1.0 to 5.0 g/hp-hr. The cost effectiveness of this control technology applied to a 2,500 to 4,000 hp rich-burn engine ranges from \$315 to \$395 per ton of NOx removed.

Lean Combustion. This technology involves the increase of the air-to-fuel ratio to lower the peak combustion temperature, thus reducing the formation of NOx (applicable for new engines and retrofit applications). The controls are between 80 and 90 percent efficient, for an operating emission rate of 1.5 to 4.0 g/hp-hr. The cost effectiveness of this control technology applied to a 2,500 to 4,000 hp rich-burn engine ranges from \$480 to \$500 per ton of NOx removed.

Selective Catalytic Reduction. This is a post combustion control technology, which is only applicable to exhaust streams with significant oxygen content (a lean burn engine). The controls are between 80 and 90 percent efficient, for an operating emission rate of 1.0 to 2.5 g/hp-hr. The cost effectiveness of this control technology applied to a 2,500 to 4,000 hp lean-burn engine ranges from \$700 to \$890 per ton of NOx removed.

For CO an emission factor of 2.0 g/hp-hr was used, and is representative for engines that have low NOx emissions. The emission factor for VOCs was assumed to be 1.0 g/hp-hr, and is the value assumed by engine manufacturers. VOC emissions also include formaldehyde, a HAP. Although the VOC emission factor is believed to be conservative, it does have a large degree of uncertainty.

Emissions from Small Wellhead Engines

Emissions estimates for small wellhead engines for proposed NSJB sources were developed by first identifying potential well locations. In general, it was assumed that 50 percent of the wells in the study region would have an associated small wellhead engine. The exception was that one operator (Huber) felt that they would need an engine at each well. The emission inventory for this source category was developed by assuming that 50 percent of the wells had a small wellhead engine, while those wells associated with Huber operations each had an engine (100 percent). Based on existing engines throughout the NSJB area, the typical size of these small engines is 48 hp (site rated capacity). Emissions were estimated using AP-42 emission factors (EPA 2000a) of 10 g/hp-hr for NOx and 8.6 g/hp-hr for CO. These potential emission sources were explicitly included in the near field modeling using the assumed well locations provided by BLM. Stack parameters were developed using combustion calculations and using historical engineering data from existing facilities.

For the near field modeling, it was assumed that these emission sources would operate at maximum capacity continuously, which represents a conservative upper estimate of potential air quality impacts.

Emissions from Separator and Dehydration Units

Additional NOx and CO emissions would also occur from new natural gas-fired heaters as part of the separators and dehydration units. These units would be located at individual wells and at the central compressor locations. For modeling, heater emissions were included by aggregating these sources at the compressor locations as individual sources, and were assumed to operate at full capacity continuously. Again, this represents a reasonable but conservative upper bound of potential emissions.

Because the natural gas produced under this proposal would come from coal bed methane (almost pure methane), no hydrocarbon condensate or natural gas liquids would be produced. Table 3-1 provides the typical composition of coal bed methane natural gas. As a result, minimum reactive VOC emissions would be associated with the proposed development.

Table 3-1. Typical Coalbed Methane Gas Composition

| Component | Volume (percent) | Molecular Weight | Weight (percent) |
|------------------|-----------------------------|-------------------------|-----------------------------|
| carbon dioxide | 12.000 | 44.010 | 27.230 |
| nitrogen gas | 0.032 | 20.016 | 0.033 |
| methane | 86.560 | 16.040 | 71.550 |
| ethane | 0.580 | 30.067 | 0.899 |
| propane | 0.098 | 44.092 | 0.220 |
| iso-butane | 0.012 | 58.118 | 0.036 |
| n-butane | 0.012 | 58.118 | 0.036 |
| iso-pentane | 0.002 | 72.144 | 0.007 |
| n-pentane | 0.001 | 72.144 | 0.004 |
| n-hexane | 0.001 | 86.169 | 0.009 |
| | | Non-reactive VOC | 99.7 |

Source: BP America, Inc. (2002)

Hazardous Air Pollutants

Formaldehyde is the only HAP that would be emitted in significant quantities from emission sources associated with natural gas development, and results from using natural gas as a fuel in internal combustion compressor engines.

Potential formaldehyde emissions were calculated for central compressor engines using an emission factor of 0.3 g/hp-hr. This represents a reasonable but conservative upper level estimate of formaldehyde emissions from lean burn natural gas-fired compressor engines (Wyoming Department of Environmental Quality 2004).

Formaldehyde emissions for small wellhead engines were calculated using an AP-42 emission factor of 0.13 g/hp-hr. This represents typical formaldehyde emissions from rich burn natural gas fired engines (EPA 2000a).

There is no universally accepted regulatory or industry emission factor for formaldehyde. Studies are ongoing to determine a reliable formaldehyde emission factor for natural gas-fired internal combustion engines, which may ultimately result in other factors than those used in this study. Because formaldehyde emissions are relatively low and emissions would be distributed over a relatively large region, a cumulative HAP analysis was not necessary. Also, the State of Colorado emission inventory does not contain HAP emission information, nor data necessary to estimate these emissions. Instead, HAP modeling was performed only for the proposed action (and alternative) sources. Because maximum impacts are likely to occur close to compressor sites, this analysis identified maximum potential near field HAP impacts.

EPA has recently developed and promulgated a maximum achievable control technology (MACT) regulation for Reciprocating Internal Combustion Engines to address formaldehyde emissions (EPA 2004). This regulation would require emission controls on certain types of engines. As a result of this regulation, by the time the proposed compressor engines would actually be installed, there will be a regulatory requirement, and actual emissions will be less than those assumed in this analysis.

Since these wells will not produce any hydrocarbon liquids or condensate, there would be no emissions of benzene, toluene, ethyl benzene or xylene (BTEX) associated with flashing or tank emissions. Also, because the gas is composed primarily of methane, and contains few heavier components, there would be no BTEX emissions from glycol dehydration units. EPA has also promulgated a MACT regulation for HAP emissions from natural gas production equipment, such as dehydration and separator equipment (EPA 1999). Since this regulation is only applicable to major HAP natural gas production sources (i.e., sources that emit in excess of 10 t/yr for a single HAP, or 25 t/yr for cumulative HAPs), it is not applicable to the proposed action (or alternative) sources.

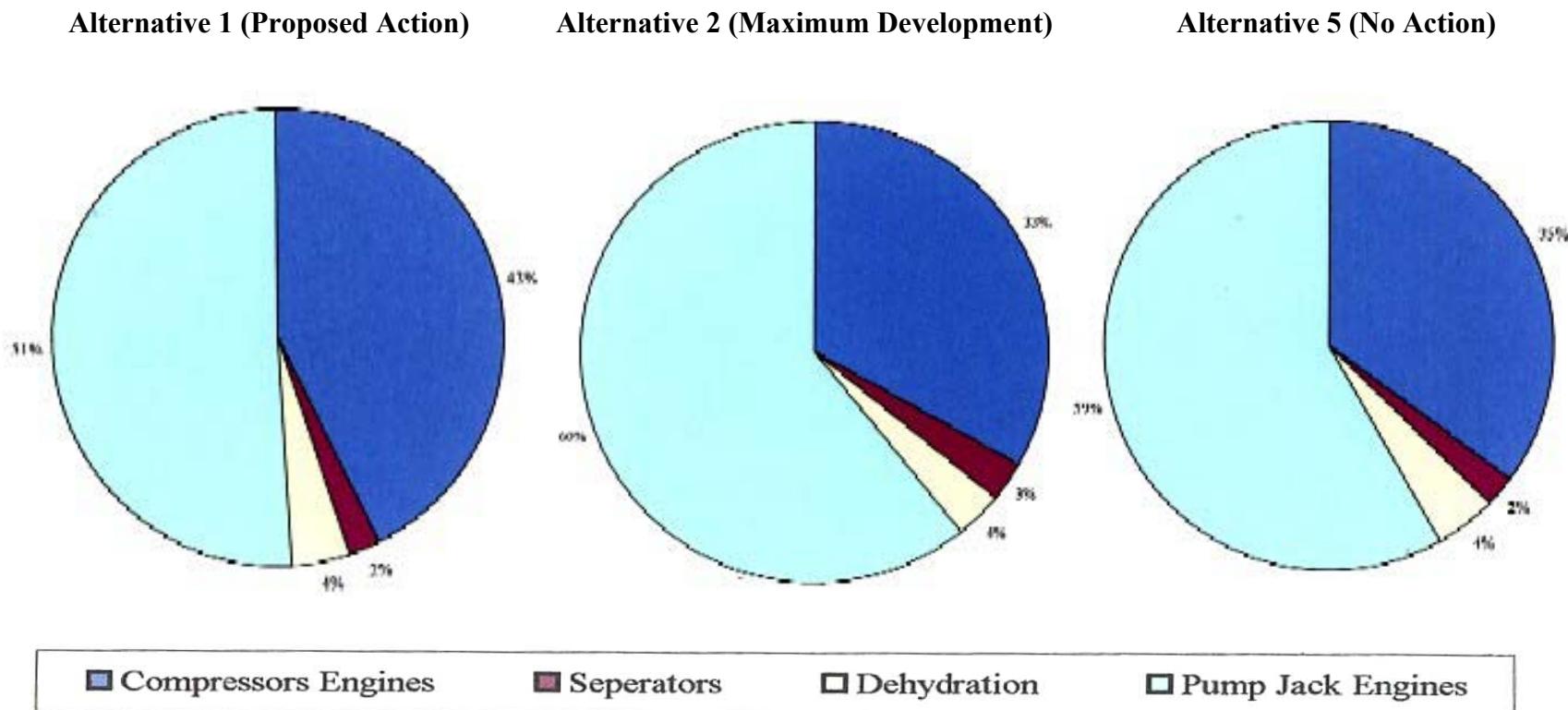
Quantification of Emissions

Five different development scenarios were identified and are summarized in Table 3-2. Although emission estimates were calculated for all alternatives, quantitative modeling was only performed for Alternatives 1, 2 and 5. As indicated under Alternative 1 (Proposed Action), it was assumed that an additional 41,000 hp of central compression and 14,352 hp of small wellhead engines would be needed. For this case, an increase in NOx emissions of 1,440 t/yr was estimated under full development. For CO and HAPs, the increase in emissions would be 1,531 and 104 t/yr, respectively. Under Alternative 2 (Maximum Development), it was assumed that 46,000 hp of additional compression and 25,248 hp of small wellhead engines would be needed. For this case, the increase in NOx, CO and HAPs emissions would be 2,087, 2,122, and 122 t/yr, respectively. Under Alternative 5 (No Action), the increase in central compression capacity was estimated to be 14,240 hp and the increase in capacity of small wellhead engines was estimated to be 6,384 hp. The potential increase in emissions (t/yr) was estimated to be 588 for NOx, 604 for CO and 36 for HAPs.

Table 3-2. Summary of Emissions by Alternative

| Proposed Alternative | Central Compression Capacity (hp) | Wellhead Engine Capacity (hp) | Total Capacity (hp) | Compressors | | | Wells | | Dehydration | | Wellhead Engines | | | Total Emissions | | |
|----------------------|-----------------------------------|-------------------------------|---------------------|-------------|-----------|-------------|------------|-----------|-------------|-----------|------------------|-----------|-------------|-----------------|-----------|-------------|
| | | | | NOx (t/yr) | CO (t/yr) | HAPs (t/yr) | NOx (t/yr) | CO (t/yr) | NOx (t/yr) | CO (t/yr) | NOx (t/yr) | CO (t/yr) | HAPs (t/yr) | NOx (t/yr) | CO (t/yr) | HAPs (t/yr) |
| 1 | 41,000 | 14,352 | 55,352 | 616 | 821 | 94 | 32 | 27 | 61 | 52 | 731 | 631 | 9.7 | 1,440 | 1,531 | 104 |
| 2 | 46,000 | 25,248 | 71,248 | 688 | 917 | 105 | 57 | 48 | 74 | 63 | 1,267 | 1,095 | 16.7 | 2,087 | 2,122 | 122 |
| 3 | 28,640 | 10,416 | 39,056 | 502 | 669 | 77 | 23 | 19 | 44 | 37 | 560 | 483 | 7.4 | 1,128 | 1,209 | 84 |
| 4 | 30,400 | 9,072 | 39,472 | 436 | 581 | 67 | 21 | 17 | 31 | 26 | 476 | 411 | 6.3 | 963 | 1,036 | 73 |
| 5 | 14,240 | 6,384 | 20,624 | 206 | 275 | 32 | 13 | 11 | 26 | 22 | 342 | 296 | 5.0 | 588 | 604 | 36 |

Figures 3-1 through 3-3. Relative NOx Emissions by Alternative and Source Category



Figures 3-1 through 3-3 present the relative contribution of NOx emissions from each source category. Appendix A presents detailed information on the development of these inventories, including detailed emission inventory tables for each alternative.

3.1.2 Existing Sources Not Represented by the Background Data

Criteria Pollutants

A cumulative analysis was performed to determine maximum combined near field impacts of the proposed action and alternatives (project sources) and non-project sources for comparison with the State and NAAQS. Information on existing sources was obtained from: 1) the State of Colorado; 2) the State of New Mexico; and 3) the SUIT and EPA regarding sources on tribal land. A cumulative near field analysis was conducted because current background monitoring data may not be representative of potential maximum impacts from existing sources. Consequently, an emission inventory for all existing sources was developed and used in the cumulative near field modeling analysis. The inventory was originally developed for the SUIT EIS (BLM 2000) and was updated for this analysis.

All existing Colorado sources within the Study Area were included in the near field emission inventory, and was compiled using information prepared by the CDPHE-APCD. Because the Division has rescinded permit authority for sources located within the boundaries of the Southern Ute Indian Reservation, an attempt was made to remove duplicate entries when compared to the tribal inventory (described below). However, it is possible that there was some double counting of emissions between the Colorado and tribal inventories, representing a reasonable but conservative upper bound of potential emissions. Appendix B presents the detailed Colorado emission source inventory.

For existing New Mexico sources, an emission inventory was obtained from the State of New Mexico Environment Department – Air Quality Bureau (NMED-AQB) web site (NMED-AQB 2003). This inventory contained some sources that were located outside of the Study Area, as well as some sources located within the State of Colorado (which were deleted from the New Mexico analysis inventory). In addition, the remaining New Mexico sources were also screened to determine which could also be excluded because they would have insignificant cumulative impacts throughout the Study Area. The determination of insignificant impacts was accomplished as follows.

First, generic emission units were developed based on existing and proposed new source sizes. Four source sizes were considered: 1) less than 10 t/yr; 2) between 11 to 50 t/yr; 3) between 51 to 100 t/yr; and 4) greater than 101 t/yr.

Second, these generic source categories were modeled using representative meteorological data (as described in Section 5.1), a 1 kilometer (km) receptor grid, and assuming averaging times applicable for the NAAQS (i.e., an annual averaging time for NO₂). Screening modeling (using the Industrial Source Complex – Short Term, or ISCST3, atmospheric dispersion model; EPA 1995) for typical sources in northwestern New Mexico was conducted using for a full year of meteorological data collected at the Bayfield Gas Plant (RTP Environmental 2002). Typical source parameters were used based on the NMED-AQB inventory.

Third, based on the screening modeling results, the distance for each source size category to the EPA “significance level” was determined (i.e., 1.0 µg/m³ for NO₂).

Finally, these distances were used to determine which sources in New Mexico would be included in the near field cumulative analysis. Sources located beyond the calculated screening distances were excluded, while those within these distances were included. Appendix C presents the detailed New Mexico emission source inventory.

The SUIT near field emission inventory for sources located within the exterior boundaries of the Southern Ute Indian Reservation was developed using several different data sources. Compilation of this inventory was not simple because the tribe does not have a major or minor source permit program, and therefore no detailed emission data were available. Although EPA has instituted a Title V (40 CFR Part 71) permitting program on tribal land, it does not have a minor source permit program. Therefore, there is no existing single emission inventory for sources on tribal land.

For this analysis, EPA Region 8 permit files were first reviewed to develop the emission inventory, including review of individual permit applications as well as processed EPA permits. It is important to note that EPA's permits on the SUIT Reservation generally do not have enforceable emission limits. This is because there is no existing minor source permit program, and EPA Region 8 cannot impose any new permitting requirements under Title V of the Clean Air Act. The second source of data was the SUIT EIS inventory for existing sources. This inventory was developed as part of the SUIT EIS analysis for existing emission sources within the boundaries of the SUIT Reservation (BLM 2000). Appendix D presents the detailed Tribal emission source inventory.

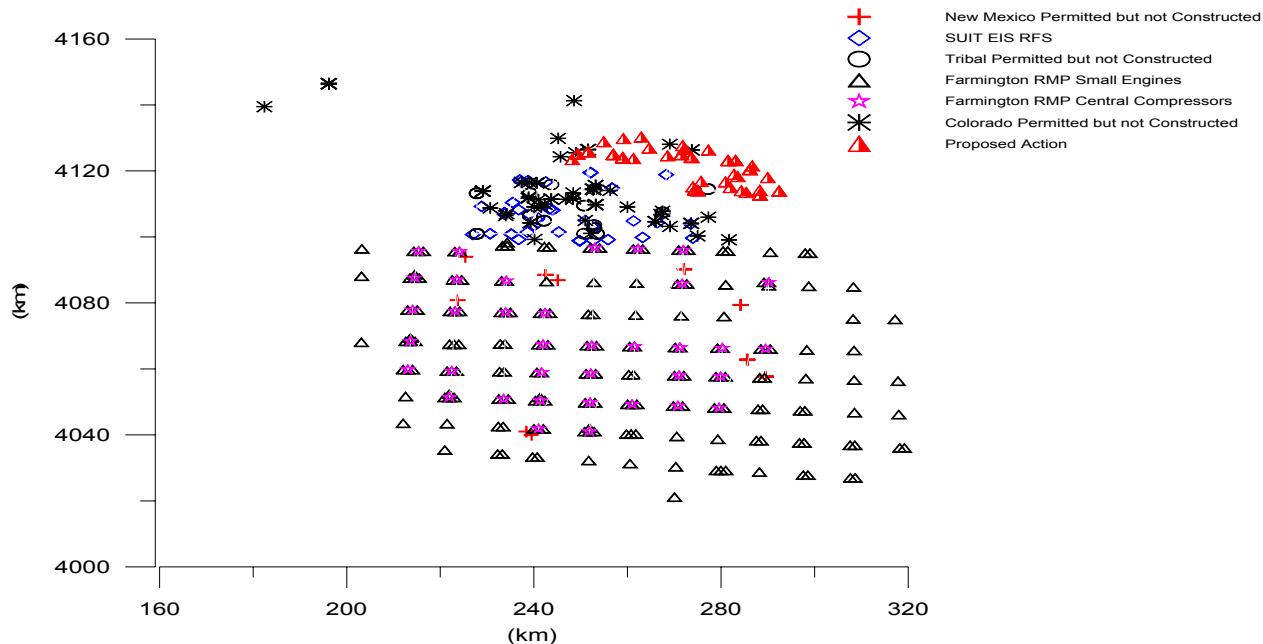
3.1.3 Reasonably Foreseeable Sources

In addition to the proposed action (and alternative) emission sources and the existing sources, the near field modeling analysis also included other RFS. These include sources that are assumed to become operational during the lifetime of the proposed activities, but have not previously been identified as existing, proposed action or alternative sources. Quantification of emissions from RFS sources is very difficult because of their speculative nature. The starting point for this inventory was the proposed action inventory developed for the SUIT EIS (BLM 2000). This included data on criteria pollutant emissions, source locations, and physical (stack) parameters. While the SUIT EIS examined three levels of potential central compressor emission controls (at 1.0, 1.5 and 2.0 g/hp-hr), this analysis assumed a level of 1.5 g/hp-hr as reasonably foreseeable. The SUIT inventory was also reviewed to determine if any of the proposed sources have been actually installed. For cases where this occurred, these sources were included in the existing Tribal near field emission source inventory. Appendix E presents the detailed RFS emission source inventory.

3.2 Far Field Emissions

This subsection presents information regarding emission inventories for the cumulative far field analysis. This methodology is consistent with emission inventory development process for other EIS', such as the SUIT EIS (BLM 2000). Figure 3-4 presents emission source locations for the proposed action (and alternatives), New Mexico, Colorado, Tribal, and other RFS sources, as well as potential Farmington, New Mexico Resource Management Plan (RMP) sources (BLM 2003).

Figure 3-4. Cumulative Far Field Emission Source Locations



The purpose of the far field analysis was to identify potential direct or cumulative air quality impacts in the downwind Mesa Verde National Park and Weminuche Wilderness mandatory federal PSD Class I areas, both located in Colorado. The primary purpose of this analysis was to determine potential NO₂ impacts, potential visibility impacts from secondary nitrate particulate matter (as well as NO₂ gas), potential total nitrogen deposition, and potential lake chemistry impacts within the Class I areas from far field NOx emission sources.

There were four groups of sources included in the far field modeling:

- proposed action (and alternative) sources;
- existing sources not represented by the background measurements (including permitted but not yet constructed sources);
- other RFS; and
- Farmington, New Mexico RMP sources.

3.2.1 Proposed Action and Alternatives

The far field proposed action (and alternative) emission inventory was identical to that used in the near field analysis (see Section 3.1.1).

3.2.2 Existing Sources Not Represented by the Background Data

The determination of which emission sources to include in the far field modeling analysis was based on the last complete year of background monitoring data, as well as an analysis of IMPROVE (Interagency Monitoring of PROtected Visual Environments; 2003) speciated aerosol monitoring data for Mesa Verde and the Weminuche PSD Class I Areas (see Section 4.2). The

purpose of this analysis was there were any aerosol trends which would question the reliability of using 1999 background monitoring data as an emission source cutoff date. Based on the information presented in Section 4.1, it was concluded that within the limits of uncertainty of the IMPROVE data, there were no significant trends in background conditions, and 1999 was the appropriate cutoff date to identify those operational sources to be included in the cumulative modeling inventory. The following criteria were used to determine inclusion of sources in the modeling. If any emission source was operational one year before 1999, it was assumed to be represented by the background monitoring data, and therefore excluded from the modeling inventory. This approach insured that source impacts were included in at least one year of monitoring data.

For sources that had obtained an emission permit, but may not have become operational (referred to as permitted but not constructed), the following criteria were used to determine if the source would be included in the far field emission source inventory. For permitted sources with the potential to emit greater than 250 t/yr, if the permit was more than 18 months old but the source had not yet become operational, it was excluded from the modeling inventory. For sources with potential emissions between 100 to 250 t/yr the criteria was one year, and for sources less than 100 t/yr the criteria was six months.

In reviewing CDPHE-APCD permit application files, all permitted but not constructed facilities were identified as natural gas-fired sources. Therefore, no SO₂ or primary particulate matter emissions were included in the far field analysis for this source group. However, review of the Colorado inventory identified a large number of missing stack parameters, therefore best engineering judgment was used to complete this information. When an assumed value was used, it was documented in the emission inventory files. Appendix B presents the detailed Colorado existing sources not represented by the background measurements, as well as permitted but not yet constructed sources which were included in the far field modeling analysis.

Similarly, in reviewing NMED-AQB permit application files, all permitted but not constructed facilities were identified as natural gas-fired sources. Therefore, no SO₂ or primary particulate matter emissions were included in the far field analysis for this source group. Appendix C presents the detailed New Mexico existing sources not represented by the background measurements, as well as permitted but not yet constructed sources which were included in the far field modeling analysis.

In reviewing the EPA Region 8 Tribal permit application files, all permitted but not constructed facilities were identified as natural gas-fired sources. Therefore, no SO₂ or primary particulate matter emissions were included in the far field analysis for this source group. Review of the Tribal permits identified a large number of missing stack parameters, therefore best engineering judgment was used to complete this information. When an assumed value was used, it was documented in the emission inventory files. Appendix D presents the detailed Tribal existing sources not represented by the background measurements, as well as permitted but not yet constructed sources which were included in the far field modeling analysis. The existing tribal emission sources identified from the SUIT EIS analysis were all excluded in the far field analysis because they were operational before 1998 (Brown 2002).

As part of the EPA Region 8 Tribal permit review, data were compiled on actual and potential emissions, start date and emission factors. An important finding of this review is the level of controls EPA Region 8 requires for compressor engines located on the SUIT reservation. Of the 70 compressor engines permits which included emission rate and compressor capacity data (allowing calculation of a corresponding emission factor, the average emission factor was 2.6 g/hp-hr. The lowest emission factor was 0.5 g/hp-hr. The highest emission factor was 17.2 g/hp-hr. Review of the individual engine data indicated that of the 70 engines, only eight were uncontrolled engines (with permitted emissions in the range of 7 to 17.2 g/hp-hr), and all of the remaining engines were permitted at less than 3 g/hp-hr. The size of these compressor engines ranged from 17 to 2,800 hp.

3.2.3 Reasonably Foreseeable Sources

In addition to the proposed action (and alternative) and the existing emission sources, the far field modeling analysis also included other RFS. These are sources that may become operational during the lifetime of the proposed activities, but were not identified as existing, proposed action or alternative emission sources. Quantification of emissions from other RFS is very difficult because of their speculative nature. The RFS inventory was based on the proposed action inventory developed for the SUIT EIS, which contained data on criteria pollutant emissions, source location and physical parameters. Appendix E presents the detailed other RFS sources which were included in the far field modeling analysis. For this source group category, the near field and far field emission inventories were the same.

3.2.4 Farmington, New Mexico RMP Sources

The other RFS sources that were included in the far field modeling were potential oil and gas sources identified in the Farmington, New RMP. This inventory was developed by reviewing the RMP (BLM 2003) and its Technical Support Document (SAIC 2003). The Farmington RMP air quality impact analysis did not quantify potential PSD Class I AQMV impacts.

The original Farmington RMP emission inventory was reviewed and modified for use in this far field impact analysis. First, the original RMP analysis assumed that small wellhead engines would be installed on 50 percent of the wells, that each small wellhead engine would have a capacity of 68.5 hp, and a corresponding NO_x emission factor of 9.62 g/hp-hr. Data obtained from New Mexico Oil and Gas Association (NMOGA) indicated the weighted average size of small wellhead engines installed in the region is 68.5 hp, although with an average emission rate of 6.4 t/yr. Operational data supplied by NMOGA also indicated the utilization rate of these engines was 54 percent (NMOGA 2003), therefore this utilization factor was applied to the far field impact analysis.

No information was provided in the RMP regarding the potential locations for small wellhead engines, however the RMP document did estimate the potential number of wells located in each geographic section. This information was used to scale the small wellhead engine emissions based on the proposed development described in the RMP. It was assumed that nearly half of the wells would be equipped with a 68.5 hp engine. However, due to operational limitations on the number of sources allowed in the air quality dispersion model (California Puff Model, or CALPUFF), 26.2

small wellhead engines were combined into common modeling point source locations, each with a total emission rate of 90 t/yr.

Model sensitivity testing was conducted to ensure this simplification of describing the emissions for this source type as input to CALPUFF would not affect the predicted impacts. This analysis kept total emissions constant but changed the emission density over the source region. The sensitivity testing involved modeling critical receptors using 26.2 engines represented as a single modeling source. This resulted in 190 source locations in CALPUFF. The second run reduced the number of sources that were combined to 11.3, which resulted in 442 source locations being modeled in three separate CALPUFF runs. The results indicated that increasing the number of emission source locations increased potential visibility impacts by only 0.1 deciview (dv). Therefore, it was demonstrated this modeling simplification would not significantly change the modeling results or conclusions.

Although not included in the original RMP analysis, it was also assumed that each well would be equipped with a three-phase separator. Total separator NOx emissions from the RMP proposed action were estimated to be 1,425 t/yr, assuming continuous operation throughout the entire year. This is a reasonable but conservative assumption because no actual separator operations information was available, and emissions from the separators were combined with the small wellhead engines due to the model limitations. Therefore, it was assumed that 70 separators (with total NOx emissions of 7.5 t/yr) were with each small wellhead engine modeling point source location.

The original RMP analysis also provided an estimate of total central compressor capacity of 360,000 horsepower, although no information was provided regarding the number of central compressor stations, the size of individual stations, or their locations. In order to perform this modeling, the following assumptions were made to distribute potential central compressors throughout the RMP area. First, it was assumed that 36 central compressor stations would be installed, each having a capacity of 10,000 hp. Based on an emission factor of 1.5 g/hp-hr, it was assumed that total NOx emissions from each central compressor station would be 145 t/yr. It was further assumed that each central compressor station would be comprised of four 2,500 hp engines. Stack parameters were based on this size engine. Source locations were estimated by placing one compressor stations in each of the 36 townships with the highest number of existing wells. Because the distance from the source region to each PSD Class I area exceeds 10-km, the modeling results would not be sensitive to exact source locations.

Dehydration units also were not included in the original RMP analysis, however, produced natural gas would be required to undergo some level of dehydration before it is sold. Dehydration burners having a capacity of 2 million British thermal units per hour (MMBtu/hr) would be required to treat every 100 million standard cubic feet of gas processed (NMOGA 2003). It was estimated that 1,062,700 million British thermal units of natural gas would be produced per year in the RMP region, which would require 2.43 MMBtu/hr of heat capacity for dehydration. This equates to nearly 10 t/yr of total dehydration NOx emissions, which were included in the modeling by adding 0.29 t/yr to each central compressor station. Appendix F presents the detailed Farmington, New Mexico sources which were included in the far field modeling analysis.

3.3 Construction Emissions

Construction emissions associated with the proposed action (and alternatives) would occur mainly due to the installation of new wells involving three sequential phases:

- well pad and resource road construction;
- rig-up, drill and rig-down; and
- well completion and testing.

The SUIT Air Quality analysis performed a detailed emission inventory for the construction phase of development (BLM 2000). No new information was available to revise estimates of those construction emissions. Therefore, Tables 3-3 through 3-5 present emission summaries (in pounds per hour, or lb/hr) from the previous study which are directly applicable to this analysis.

Table 3-3. Well Pad Site and Resource Road Construction Phase Emission Inventory

ASSUMPTIONS:

Number of days to complete the activity 3 days
Hours of operation per day 8 hours
Total number of work hours to complete the activity.....24 hours

| Activities | Emission Rates (lb/hr) | | | | |
|----------------------------------------|------------------------|-----------------|-----------------|-------------|-------------|
| | PM ₁₀ | SO ₂ | NO _x | CO | VOC |
| FUGITIVE DUST EMISSIONS | | | | | |
| Well pad construction | 2.62 | 0.00 | 0.00 | 0.00 | 0.00 |
| Resource road construction | 3.15 | 0.00 | 0.00 | 0.00 | 0.00 |
| Traffic on unpaved haul roads | 37.83 | 0.00 | 0.00 | 0.00 | 0.00 |
| Subtotal | 43.60 | 0.00 | 0.00 | 0.00 | 0.00 |
| EQUIPMENT AND VEHICLE EMISSIONS | | | | | |
| Truck tail pipe emissions | 0.91 | 1.01 | 10.87 | 3.17 | 0.95 |
| Heavy construction equipment | 0.31 | 0.24 | 3.04 | 1.24 | 0.38 |
| Subtotal | 1.22 | 1.25 | 13.91 | 4.41 | 1.33 |
| Maximum Hourly Emissions | 44.82 | 1.25 | 13.91 | 4.41 | 1.33 |

Table 3-4. Well Site Rig-Up, Drill and Rig-Down Phase Emission Inventory

ASSUMPTIONS:

Number of days of vehicle/equipment traffic 8 days
Hours of operation per day for traffic 8 hours
Total number of traffic hours 64 hours
Number of days of drill rig engine operation 6 days
Hours of operation per day for drill rig engines 24 hours
Total numbers of drill engine operating hours
incorporating load factor for time operated 144 hours

| Activities | Emission Rates (lb/hr) | | | | |
|---------------------------------|------------------------|-----------------|-----------------|-------------|-------------|
| | PM ₁₀ | SO ₂ | NO _x | CO | VOC |
| Traffic on unpaved haul roads | 25.34 | 0.00 | 0.00 | 0.00 | 0.00 |
| Subtotal | 25.34 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | | | | |
| Truck tail pipe emissions | 0.67 | 0.75 | 8.09 | 2.36 | 0.71 |
| | | | | | |
| Operation of drill rig engines | 1.07 | 1.02 | 15.11 | 3.27 | 1.22 |
| Subtotal | 1.74 | 1.77 | 23.20 | 5.63 | 1.93 |
| | | | | | |
| Maximum Hourly Emissions | 27.08 | 1.77 | 23.20 | 5.63 | 1.93 |

Table 3-5. Well Completion and Testing Phase Emission Inventory

ASSUMPTIONS:

Number of days of vehicle/equipment operation:.....25 days
Hours of operation per day for vehicle/equipment operation: 8 hours
Total number of hours of vehicle/equipment operation: 200 hours
Number of days to complete well flaring: 7 days
Hours of operation per day for well flaring: 24 hours
Total number of hours of gas flaring 168 hours

| Activities | Emission Rates (lb/hr) | | | | |
|---------------------------------|------------------------|-----------------|-----------------|--------------|-------------|
| | PM ₁₀ | SO ₂ | NO _x | CO | VOC |
| Traffic on unpaved haul roads | 11.25 | 0.00 | 0.00 | 0.00 | 0.00 |
| Subtotal | 11.25 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | | | | |
| Tail pipe emissions from trucks | 0.16 | 0.18 | 1.94 | 0.57 | 0.17 |
| Gas flaring | 0.18 | Neg. | 2.02 | 11.01 | 1.88 |
| Subtotal | 0.34 | 0.18 | 3.96 | 11.58 | 2.05 |
| | | | | | |
| Maximum Hourly Emissions | 11.59 | 0.18 | 3.96 | 11.58 | 2.05 |

4.0 Air Quality Data

4.1 Near Field Background Data

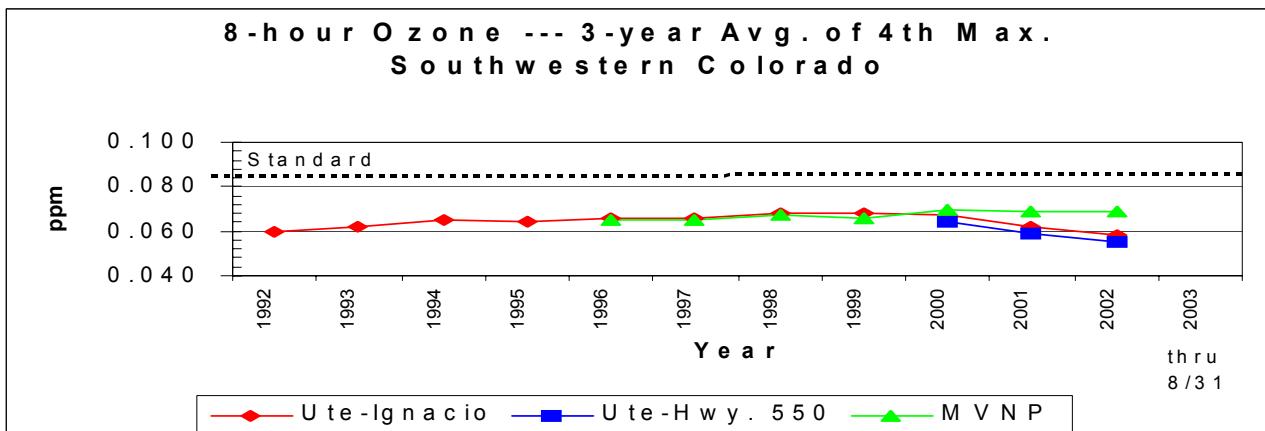
Air quality is considered to be good throughout the EIS Study Area with existing sources of air pollution distributed over a large area. The most complete air quality measurement data available within the project area are from the SUIT monitoring station near Ignacio, Colorado, which has been operational since 1987. The maximum measured pollutant concentrations are summarized in Table 4-1, and demonstrate air quality has consistently been well below applicable NAAQS. This station is operated according to PSD Monitoring Guidelines, and its data are routinely audited by EPA Region 8.

Although the maximum recorded 1 hr ozone concentration ($237 \mu\text{g}/\text{m}^3$, measured in 1994) slightly exceeded the NAAQS (at $235 \mu\text{g}/\text{m}^3$), the second highest measured concentration ($182 \mu\text{g}/\text{m}^3$, also measured in 1994) was considerably below the standard. Since that time, the maximum 1 hr ozone concentration has been even less. In addition, Figure 4-1 presents a summary of the running three year average of the 4th highest 8 hr ozone concentrations measured in southwestern Colorado. As indicated in this figure, the maximum 4th highest three year average concentration was approximately 0.070 parts per million (ppm; nearly $137 \mu\text{g}/\text{m}^3$), and indicates this region complies with the 8 hr ozone NAAQS of 0.08 ppm ($157 \mu\text{g}/\text{m}^3$).

There are no historical data on ambient carbon monoxide within the EIS Study Area. The CDPHE-APCD recommends assuming a concentration of 2 ppm ($2,286 \mu\text{g}/\text{m}^3$) for both the 1 and 8 hr averaging periods as a representative value for rural southern Colorado (CDPHE-APCD 2001).

The Ignacio air quality measurement data are considered to be representative of the air quality in the non-industrialized portions of southern Colorado. Since Ignacio is the largest population center within the SUIT Reservation, the effects of vehicle emissions at this station are likely to be greater than at other rural locations throughout the EIS Study Area.

Figure 4-1. Running Three Year Average of 4th Maximum 8 hour Ozone Values



Source: CDPHE-APCD (2003)

Table 4-1. Background Air Pollutant Concentrations (Regional)

| Pollutant | Year | Averaging Time | Maximum Concentration ($\mu\text{g}/\text{m}^3$) | Second Maximum Concentration ($\mu\text{g}/\text{m}^3$) | Applicable Ambient Air Quality Standard ($\mu\text{g}/\text{m}^3$) |
|-------------------|-----------|----------------|----------------------------------------------------|-----------------------------------------------------------|----------------------------------------------------------------------|
| carbon monoxide | | 1-hr | 2,286 ⁽¹⁾ | 2,286 ⁽¹⁾ | 40,000 |
| | | 8-hr | 2,286 ⁽¹⁾ | 2,286 ⁽¹⁾ | 10,000 |
| nitrogen dioxide | 1997 | Annual | 9.4 | N/A | 100 |
| | 1998 | Annual | 9.4 | N/A | 100 |
| | 1999 | Annual | 9.4 | N/A | 100 |
| | 2000 | Annual | 7.5 | N/A | 100 |
| ozone | 1996 | 1-hr | 164 | 163 | 235 |
| | 1997 | 1-hr | 149 | 147 | 235 |
| | 1998 | 1-hr | 157 | 153 | 235 |
| | 1999 | 1-hr | 153 | 151 | 235 |
| | 2000 | 1-hr | 151 | 147 | 235 |
| | 1997-1999 | 8-hr | 137 ⁽²⁾ | N/A | 157 |
| PM_{10} | 1991 | 24-hr | 50 | 25 | 150 |
| | 1991 | Annual | 11.0 | N/A | 50 |
| | 1992 | Annual | 10.2 | N/A | 50 |
| | 1993 | Annual | 11.3 | N/A | 50 |
| | 1994 | Annual | 10.8 | N/A | 50 |
| | 1995 | Annual | 14.1 | N/A | 50 |
| | 1996 | Annual | 14.6 | N/A | 50 |
| $\text{PM}_{2.5}$ | 2003 | 24-hr | 26 ⁽³⁾ | 20 ⁽³⁾ | 65 |
| | | Annual | 6 ⁽³⁾ | N/A | 15 |
| sulfur dioxide | 1992 | 3-hr | 57 | 55 | 700 |
| | | 24-hr | 23 | 23 | 365 |
| | | Annual | 1.8 | N/A | 80 |

Source: BLM (2000)

$\mu\text{g}/\text{m}^3$ – micrograms per cubic meter

N/A – not applicable

⁽¹⁾ CDPHE-APCD (2001) assumed values

⁽²⁾ Maximum 4th highest 3-yr running average concentration

⁽³⁾ CDPHE-APCD (2003) data collected in Durango, Colorado.

4.2 PSD Class I Background Data

Criteria Pollutants

Representative background ambient air pollutant concentrations provided by the State of Colorado (CHPDE-APCD 2001), based on typical rural air quality estimates, were used to describe existing air quality within Mesa Verde National Park and the Weminuche Wilderness PSD Class I areas. These levels are summarized in Table 4-2.

Table 4-2. Background Air Pollutant Concentrations (Mesa Verde and Weminuche)

| Pollutant | Averaging Time | Mesa Verde National Park ($\mu\text{g}/\text{m}^3$) | Weminuche Wilderness Area ($\mu\text{g}/\text{m}^3$) |
|------------------|----------------|-------------------------------------------------------|--------------------------------------------------------|
| carbon monoxide | 1-hr | 2,286 | 2,286 |
| | 8-hr | 2,286 | 2,286 |
| nitrogen dioxide | Annual | 9 | 9 |
| PM ₁₀ | 24-hr | 30 | 9 |
| | Annual | 6 | 4 |
| sulfur dioxide | 3-hr | 21 | 21 |
| | 24-hr | 13 | 13 |
| | Annual | 5 | 5 |

Source: CDPHE-APCD (2001)

Visibility

Background visibility conditions were determined based on speciated aerosol samples collected using IMPROVE (2003) monitoring protocols at Mesa Verde National Park and Weminuche Wilderness Area, as well as daily average relative humidity values measured at the Albino Canyon, New Mexico, Remote Automatic Weather Station (RAWS; WRCC 2003). Measured concentrations of sulfate ion, nitrate ion, organic carbon, elemental carbon, soil and coarse mass were incorporated into a Microsoft Excel[®] Daily FLAG Refined Analysis Spreadsheets (Archer 2003), which calculated daily background visibility (extinction) conditions based on the FLAG (2000) reconstructed extinction methodology. Missing speciated aerosol concentration and daily relative humidity data were substituted by linearly interpolation between valid data.

Figure 4-2 presents the visibility frequency distribution expressed in deciviews for Mesa Verde National Park from 1989 through 1999. This is done for the 90th (clearest), 80th, 50th, 20th, and 10th (haziest) percentile days in each year. The horizontal lines present the temporal trend (least square

fit) for each percentile level. While there is some inter-annual variation about the mean, there does not appear to be a discernible trend in visibility conditions. The standard deviation around the annual means is about 0.5 dv at all percentile levels. This variation is below the 1.0 dv “just noticeable change” visibility threshold. This finding suggests that visibility has not significantly changed at Mesa Verde National Park mandatory federal PSD Class I Area.

Figure 4-3 presents the visibility frequency distribution expressed in deciviews for the Weminuche Wilderness Area from 1989 through 1999. There appears to be a slight visibility reduction trend for the clearest days, and a slight visibility improvement for the haziest days. The standard deviation about the annual means is approximately 0.6 dv at all percentile levels, which is below the 1.0 dv “just noticeable change” visibility threshold.

Figure 4-2. 1989-99 Visibility Frequency Distribution (Mesa Verde)

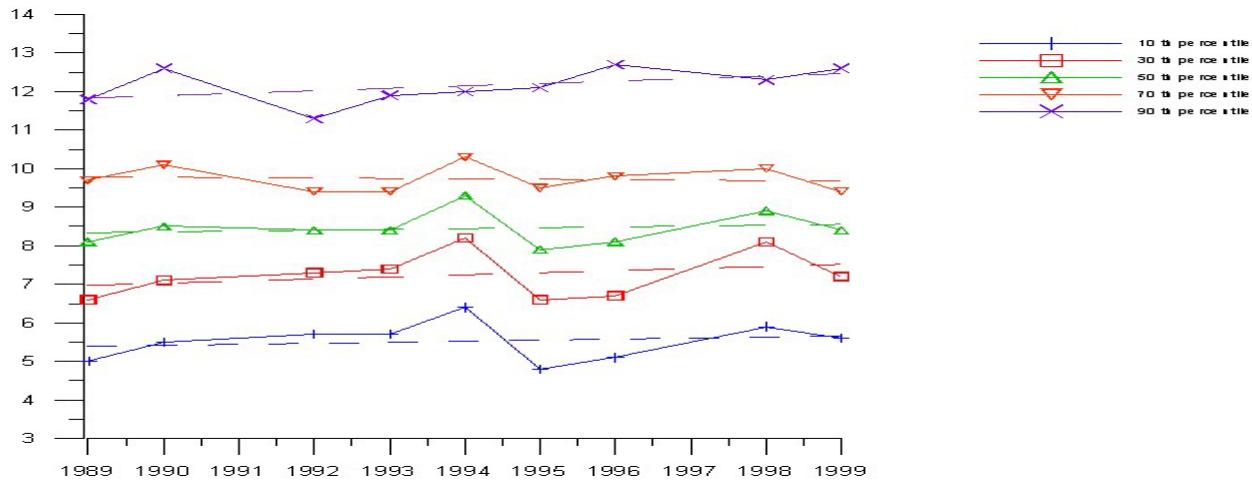
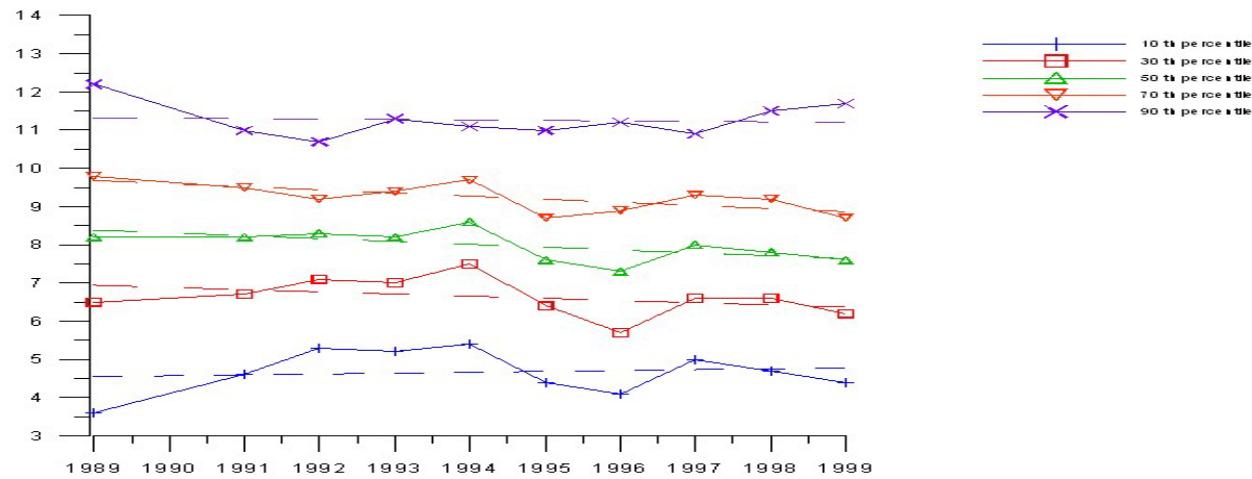


Figure 4-3. 1989-99 Visibility Frequency Distribution (Weminuche)



Lake Chemistry

Four lakes of concern were identified within the Weminuche Wilderness Area, while the USDI-National Park Service has not identified any sensitive lakes within Mesa Verde National Park. The Weminuche sensitive lakes and their background acid neutralizing capacity (ANC; reported in microequivalents per liter, or $\mu\text{eq/l}$) values are presented in Table 4-3.

Table 4-3. Weminuche Wilderness Area Sensitive Lakes

| Sensitive Lake | Background Acid Neutralizing Capacity ($\mu\text{eq/l}$) |
|---------------------|------------------------------------------------------------|
| Big Eldorado Lake | 27.7 |
| Lower Sunlight Lake | 79.8 |
| Upper Grizzly Lake | 24.3 |
| Upper Sunlight Lake | 25.8 |

Source: USDA-Forest Service (2001)

5.0 Meteorological Data

5.1 Near Field Meteorological Data

Calendar year 2002 (December 16, 2001 through December 16, 2002) meteorological data used for the ISCST3 modeling analysis were obtained from the Bayfield Gas Plant (RTP Environmental 2002) meteorological tower located in La Plata County, Colorado. This meteorological monitoring system was installed in December 2001 and is still in operation. Wind speed, wind direction and ambient temperature were measured at a height of 10 m above the surface. Atmospheric stability was calculated based on the standard deviation of wind direction and mean wind speed (EPA 2000b). Mixing height was estimated using Holzworth average minimum and maximum mixing heights for the region (EPA 2000c). Because the stack heights for the proposed sources are low, mixing height was not a critical model variable for the near field analysis.

5.2 Cumulative Far Field Meteorological Data

The winds throughout in the EIS Study Area are complex and highly variable as a result of terrain features. Consequently, winds throughout the study area were determined using the California Meteorological Model (CALMET), with its diagnostic wind field module, rather than being driven by direct observations (Scire, et al 2000a).

The CALMET meteorological data developed for the SUIT EIS modeling effort were used in this analysis. Additional review was conducted to determine if any new data could be used to supplement the data used in the SUIT analysis. While newer meteorological data were identified at the Florida and Bayfield gas processing facilities, these data were not incorporated due to operational constraints. A Mesoscale Model, version 5 (MM5) modeling run conducted by EPA was also considered, but it was not available in a computer usable format.

The primary source of meteorological data used in the SUIT EIS to initiate the CALMET wind field was the 1990 Mesoscale Model, version 4 (MM4) data base (NCDC 1995). This data set consists of modeled hourly values of wind speed, wind direction, temperature and pressure on an 80-km grid that covers the continental United States, southern Canada and northern Mexico. These data were prepared to supplement observational data in areas where observational data are sparse. The use of these data is consistent with recommendations from the Interagency Work Group on Air Quality Modeling (IWAQM 1998) Phase 2 report.

In addition to the MM4 data, CALMET requires hourly surface observations of wind speed, wind direction, temperature, cloud cover, ceiling height, surface pressure, relative humidity and precipitation type (i.e., snow, rain, etc.) These data are routinely collected by National Weather Service (NWS) and Federal Aviation Administration (FAA) surface observation stations. Upper air data are also required, and include twice-daily observations of vertical profiles of wind speed, wind direction, temperature and pressure. Table 5-1 presents a list of available meteorological data for 1990 within the modeling domain.

Table 5-1. Regional Meteorological Data Sources

| Location | Data |
|-------------------------------|------------------------------------------------|
| Surface Observations | |
| Grand Junction, Colorado | Hourly surface (CD144) observations (NWS) |
| Gallup, New Mexico | Hourly surface observations (FAA) |
| Upper Air Observations | |
| Grand Junction, Colorado | Twice-daily upper air (TD6201) soundings (NWS) |
| Albuquerque, New Mexico | Twice-daily upper air (TD6201) soundings (NWS) |

Hourly precipitation measurements are required for wet deposition calculations in CALPUFF. In developing the SUIT EIS, Earth Tech, Inc. compiled gridded precipitation data; those data were also utilized in this analysis (BLM 2000).

6.0 Air Quality Modeling

6.1 Near Field Production

The selection of an appropriate dispersion model for analysis of the proposed action (and alternatives) near field air quality impacts was based upon the available meteorological data, local environment, the physical characteristics of proposed sources, and anticipated buildings and structures. Taking these factors into account, the ISCST3 dispersion model (Version 02035) was used for both the construction and production phase near field impact analyses. The ISCST3 model is a Gaussian dispersion model designed for applications involving multiple sources within an industrial facility, and has been designated an EPA-approved Guideline model (EPA 1995).

6.1.1 Receptor Grid

A nested fine and coarse receptor grid was used in this analysis. The fine receptor grid was designed to identify maximum impacts from sources associated with the proposed action (and alternatives). This grid was constructed around each proposed new central compressor station. Receptors were located at a distance of approximately 100 m from the facility or fence line, and extend to a distance of 500 m, creating a rectangular grid having a resolution of 100 m. Since the physical height of the compressor stations is similar to the stack height, it is important to consider aerodynamic downwash when estimating potential maximum impacts. Under such conditions, the largest impacts would likely occur close to the facility's fence line. Thus, this receptor grid was designed to ensure that the concentrations resulting from such effects were quantified. A computer program was used to calculate receptor locations around each assumed new emission source, and to generate the fine receptor grid when sources of the proposed development would be less than 1 km apart. A plot showing the network of fine receptor grids is shown in Figure 6-1.

The coarse receptor grid was created to cover the entire EIS Study Area so that maximum near field impacts throughout the region could be evaluated. This grid was laid out using a rectangular grid with 500 m resolution. As shown in Figure 6-2, the fine grids around individual compressor stations are embedded within this coarse grid. Terrain elevations were extracted from the United States Geological Survey (USGS 1987) digital elevation model (DEM) files for each receptor point.

Modeling results were reviewed to ensure that the receptor grids identified the location and magnitude of the maximum impacts.

Figure 6-1. Near Field Fine Receptor Grid

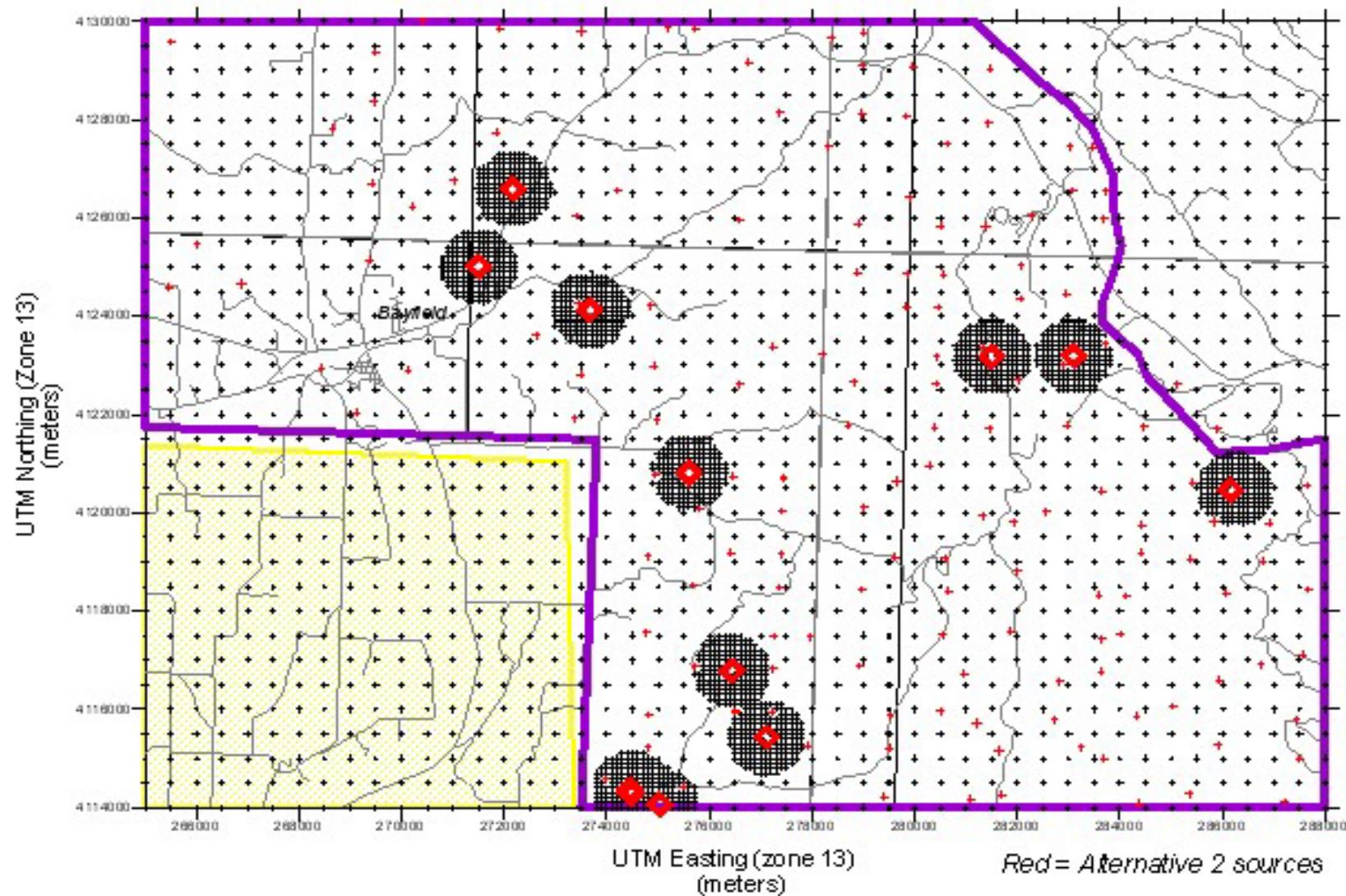
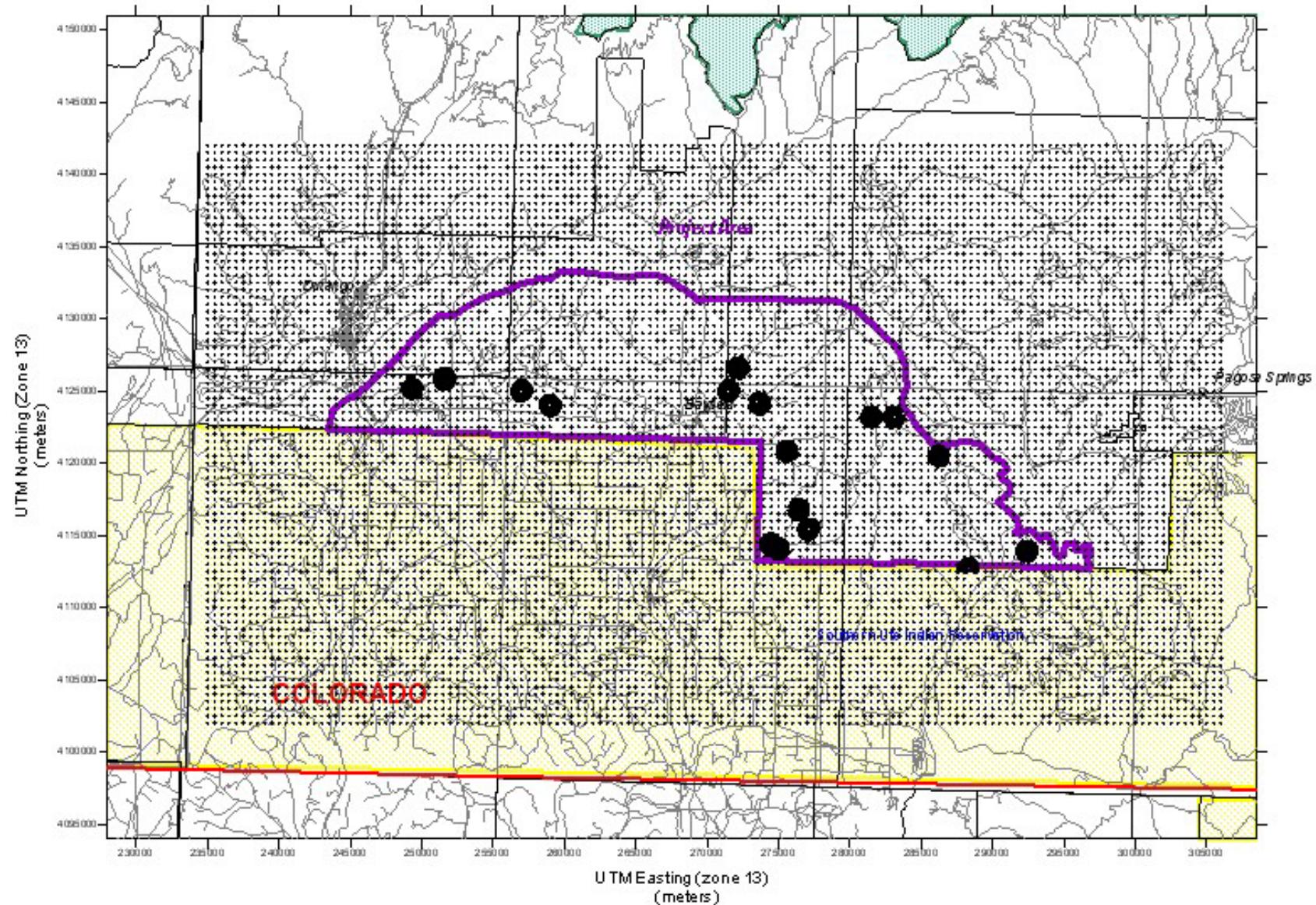


Figure 6-2. Near Field Coarse Receptor Grid



6.1.2 Model Options

The regulatory default options outlined in the Guideline on Air Quality Models (EPA 1986) were used for the near field ISCST3 modeling. These options are as follows:

- use stack-tip downwash for point sources (except when Schulman-Scire building downwash is applicable);
- use buoyancy-induced dispersion;
- do not use gradual plume rise (except when building downwash is applicable);
- use calms processing routine;
- use default wind speed exponents; and
- use default vertical potential temperature gradients

The ISCST3 rural dispersion coefficients were used, consistent with the rural land use in the EIS Study Area.

6.1.3 Building Downwash

The ISCST3 model provides the option to simulate aerodynamic plume downwash on the lee side of buildings (and other obstacles) that may be adjacent to the source. Downwash can produce elevated ground level concentrations close to these structures. The occurrence of downwash depends on the interaction between the height of the stack, the distance between the stack and nearby buildings, the dimensions of the buildings, as well as meteorological conditions.

Estimates of assumed building dimensions for the proposed compressor stations were developed as part of the emission inventory. Because of the lack of detailed engineering data, building dimensions have been assumed to apply uniformly regardless of wind direction. Downwash was not considered for the Colorado, New Mexico, Tribal and other RFS inventory sources because building dimensions were not available in those inventories.

6.1.4 Conversion of NO_x into NO₂

Emissions of NO_x as a result of burning natural gas would be primarily in the form of nitrogen oxide, which can be photochemically converted into NO₂ in the presence of ambient ozone. EPA's regulatory default NO₂/NO_x conversion ratio of 0.75 (EPA 2003a) was used to estimate NO₂ concentrations for comparison with the annual State and NAAQS. Potential NO₂ impacts were therefore calculated by multiplying the NO_x emission rate by 0.75 prior to inclusion in the ISCST3 model. Given the rural nature of the EIS Study Area, this procedure can be viewed as a reasonable but conservative application.

6.2 Far Field Production

The non-steady-state CALPUFF modeling system (including CALMET) was used in the far field analysis. EPA has identified these as preferred Guideline Models (Scire, et al 2000a and 2000b) for both air quality concentration assessments and in determining potential AQRV impacts at source-receptor distances of 50 to several hundred kilometers (EPA 2003b).

6.2.1 CALMET

CALMET is a diagnostic meteorological model that produces three-dimensional wind fields based on large-scale diagnostic flows, ground-level observations, terrain (such as slope flow and terrain blocking) and water body effects. Meteorological observations are used to determine the wind field in areas where the observations are representative, whereas diagnostic winds are given more weight in areas away from observations. The CALMET meteorological model consists of a diagnostic wind field module and a micrometeorological module for determining boundary layers over water and land. The diagnostic wind field module uses a two-step approach to compute wind fields. In the first step, an initial guess wind field is adjusted for kinematic effects of terrain, slope flow and terrain blocking, to produce an initial wind field. The second step consists of an objective analysis procedure to adjust the initial wind field (based on observational data) to produce a final wind field.

In this study, a Lambert Conformal Projection Coordinate System was used to account for the curvature of the Earth.

The major features and options of the meteorological model are summarized in Table 6-1. The techniques used in the CALMET model are briefly described in the following subsections. Hourly CALMET results were combined on a monthly basis and the output files were archived for subsequent air quality impact analysis using CALPUFF.

Table 6-1. Features of the CALMET Meteorological Model

| Boundary Layer Modules of CALMET | Diagnostic Wind Field Module of CALMET |
|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| Over Land Boundary Layer - Energy Balance Method Over Water Boundary Layer - Profile Method Produces Gridded Fields of: <ul style="list-style-type: none">● Surface Friction Velocity● Convective Velocity Scale● Monin-Obukhov Length● Mixing Height● Pasquill-Gifford Stability Class● Air Temperature (3-D)● Precipitation Rate | Slope Flow: <ul style="list-style-type: none">● Kinematic Terrain Effects● Terrain Blocking Effects● Divergence Minimization● Produces Gridded Fields of U, V, W Wind Components● Input Includes Domain-Scale Winds, Observations● Coarse-Grid Prognostic Model Winds● Lambert Conformal Projection |

6.2.1.1 Modeling Domain

This study utilized the SUIT EIS modeling domain, including portions of southwestern Colorado and northwestern New Mexico, as well as Mesa Verde National Park and the Weminuche Wilderness Area (Figure 1-1). The modeling domain also includes topographical features which would modify the wind flow, including some peak elevations that are more than 2 km above some emission source base elevations.

A spatial resolution of 2 km was used to represent the sharp variations of the terrain elevations in the area. All USGS elevation records located within each grid cell of the modeling domain were averaged to produce a single mean elevation for each grid point. A 2 km grid resolution produced a reasonable number of cells while providing adequate representation of terrain features.

6.2.1.2 Model Options

Terrain

The terrain files used in this analysis were obtained from the SUIT modeling analysis (BLM 2000), derived from the 3 arc-second DEM (USGS 1990), formatted and distributed by the Earth Resources Observation System (EROS) Data Center. USGS 1:250,000 scale topographic maps are the primary source of 1 degree DEMs. These data are provided in files covering 1 degree by 1 degree blocks of latitude and longitude, corresponding to a square of approximately 108 km. The 1 degree DEMs were produced by the Defense Mapping Agency using cartographic and photographic sources (USGS 1987).

One degree DEM data consists of an array of 1201 by 1201 elevations referenced on the geographic (latitude/longitude) coordinate system of the World Geodetic System 1972 Datum. Elevations are in meters relative to mean sea level, with the elevations along each profile spaced at 3 arc seconds (corresponding to approximately 90 m).

Land Use

The USGS land use data in the Study Area were cataloged to produce a grided field of dominant land use categories. The land use data were obtained in Composite Theme Grid format from the EROS Data Center Land Use and Land Cover web site with a resolution of 30 m. (USGS 1990).

Land use data were combined to produce a 2 km resolution grided field of fractional land use categories. The 37 USGS land use categories were then converted into 14 CALMET land use categories. Surface properties such as albedo, Bowen ratio, roughness length and leaf area index were computed proportionally to the fractional land use. Table 6-2 presents the default CALMET land use categories along with their associated geophysical parameters.

6.2.2 CALPUFF

The CALPUFF modeling system (Scire, et al 2000b) Version 5 was used for determining potential air quality impacts within the two distant mandatory federal PSD Class I Areas. CALPUFF, and its meteorological model, CALMET (Scire, et al 2000a), are designed to address the influence of complex terrain on air pollutant transport, and to predict potential impacts at locations 50 to several hundred kilometers away from multiple emission sources. CALPUFF is a non-steady-state Gaussian puff model, and includes algorithms for: building downwash effects; chemical transformation; wet, dry and total atmospheric deposition; as well as assessing the impact of primary and secondary particulate matter (and NO₂ gas) on visibility. The EPA (2003b) has designated CALPUFF as a Guideline model for this type of analysis.

Table 6-2. Default CALMET Land Use Categories and Geophysical Parameters

| Land Use Type | USGS Description | Surface Roughness | Albedo | Bowen Ratio | Soil Heat Flux | Leaf Area Index |
|--------------------|-----------------------------------|-------------------|--------|-------------|----------------|-----------------|
| 10 | Urban or Built-up Land | 1.0 | 0.18 | 1.5 | 0.25 | 0.2 |
| 20 | Agricultural Land – Non-irrigated | 0.25 | 0.15 | 1.0 | 0.15 | 3.0 |
| -20 ⁽¹⁾ | Agricultural Land – Irrigated | 0.25 | 0.15 | 0.5 | 0.15 | 3.0 |
| 30 | Rangeland | 0.05 | 0.25 | 1.0 | 0.15 | 0.5 |
| 40 | Forest Land | 1.0 | 0.10 | 1.0 | 0.15 | 7.0 |
| 50 | Water | 0.001 | 0.10 | 0.0 | 1.0 | 0.0 |
| 51 | Small Water Body | 0.001 | 0.10 | 0.0 | 1.0 | 0.0 |
| 55 | Large Water Body | 0.001 | 0.10 | 0.0 | 1.0 | 0.0 |
| 60 | Wetland | 1.0 | 0.10 | 0.5 | 0.25 | 2.0 |
| 61 | Forested Wetland | 1.0 | 0.10 | 0.5 | 0.25 | 2.0 |
| 62 | Non-forested Wetland | 0.2 | 0.10 | 0.1 | 0.25 | 1.0 |
| 70 | Barren Land | 0.05 | 0.30 | 1.0 | 0.15 | 0.05 |
| 80 | Tundra | 0.20 | 0.30 | 0.5 | 0.15 | 0.0 |
| 90 | Perennial Snow or Ice | 0.20 | 0.70 | 0.5 | 0.15 | 0.0 |

⁽¹⁾ Negative values indicate “irrigated” land use

Separate CALPUFF modeling runs were made for several discrete emission source groups (as described in Table 6-3). This allowed individual source group impacts to be evaluated for both the Mesa Verde National Park and Weminuche Wilderness PSD Class I Areas. In addition, the individual emission source impacts were combined using a post-processing program to estimate cumulative impacts. CALPUFF was run for an entire year using the hourly meteorological modeling results from CALMET (see Section 6.2.1).

Table 6-3. CALPUFF Emission Source Categories

| Source Type | Source Groups Considered ⁽¹⁾ |
|--------------------------------------|-----------------------------------------------------------------------------------------------------|
| Proposed Action Sources | Alternative 1 (Proposed Action) Alternative 2 (Maximum Development) Alternative 5 (No Action) |
| Existing Sources | Colorado Permitted New Mexico Permitted Tribal Permitted |
| Other Reasonably Foreseeable Sources | SUIT EIS (Proposed) Farmington (NM) RMP |

⁽¹⁾ Each source group was evaluated in a separate CALPUFF modeling run

6.2.2.1 Modeling Domain

The CALPUFF modeling domain was the same size and resolution as the CALMET meteorological grid. In the vertical dimension, ten separate layers were used, including a finer resolution near the mixed layer and a coarser resolution above the mixed layer. The ten vertical levels used in this analysis were set at 10, 30, 70, 120, 230, 450, 800, 1250, 1850 and 2600 m above the terrain.

6.2.2.2 Receptor Grid

Discrete receptors were located along the external boundaries of Mesa Verde National Park and the Weminuche Wilderness Area, each with a resolution of 1 km. Gridded receptors were placed throughout the two Class I Areas with a grid resolution of 2 km. Discrete receptors were also placed at individual lake locations within the Weminuche Wilderness Area, which were identified by the USDA-Forest Service as potentially sensitive to atmospheric deposition. The lake receptors included:

- Big Eldorado Lake;
- Lower Sunlight Lake;
- Upper Sunlight Lake; and
- Upper Grizzly Lake.

Terrain elevations and receptor locations used for Mesa Verde National Park and the Weminuche Wilderness area are illustrated in Figures 6-3 and 6-4, respectively.

Figure 6-3. Far Field Analysis Receptor Grid (Mesa Verde)

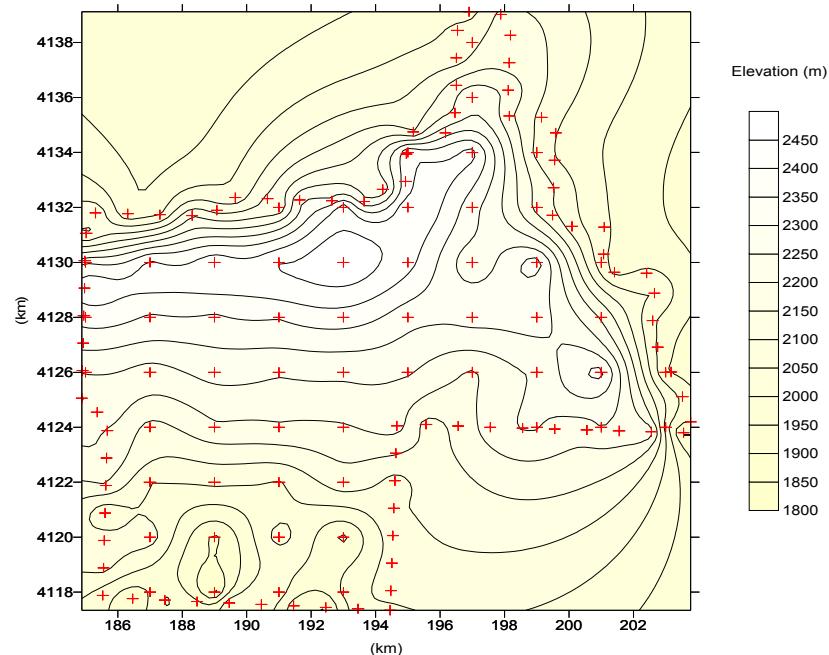
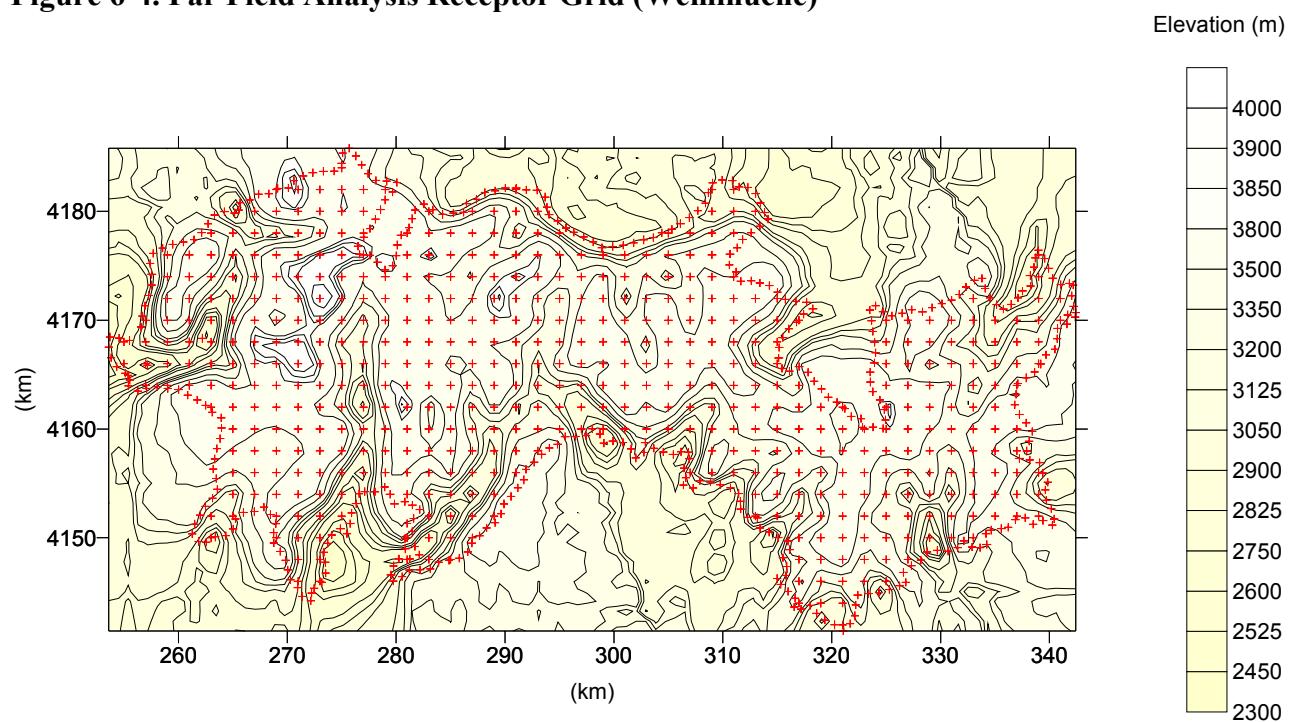


Figure 6-4. Far Field Analysis Receptor Grid (Weminuche)



6.2.2.3 Model Options

The CALPUFF model was run with the following technical options selected:

- Gaussian near field distribution;
- transitional plume rise;
- stack tip downwash;
- Pasquill-Gifford dispersion coefficients (rural areas);
- transition of sigma y to time-dependent (Heffter) puff growth rates;
- wet deposition;
- dry deposition;
- chemical transformation of SO₂ to sulfate ion (SO₄⁻), and NOx/NO₂ to nitric acid (HNO₃) and nitrate ion (NO₃⁻), modeled using the MESOPUFF II chemical mechanism (EPA 1994);
- wet and dry deposition effects modeled using the default dry deposition model, dry deposition parameters and scavenging coefficients; and
- EPA default conversion rate of 0.75 was used to estimate the transformation of NOx into NO₂ (see Section 6.1.4).

Terrain and Land Use

The CALPUFF terrain and land use values were identical to those used for the CALMET meteorological model (see Section 6.2.1.2).

6.2.2.4 Background Ammonia Levels

When calculating the chemical transformation of SO₂ and NOx emissions to secondary particulate matter (ammonium sulfate and ammonium nitrate), CALPUFF requires an assumed concentration of background ammonia (NH₃) levels. Since ammonia is not directly measured in the atmosphere, it was computed using a procedure developed for the Southwestern Wyoming Technical Air Forum (Earth Tech, Inc. 2001). This methodology assumes that the amount of ammonia available for forming secondary nitrate may be thought as the residual after secondary sulfate forms (sulfate has a greater affinity to ammonia than nitrate). Therefore, sulfate and nitrate concentrations collected at IMPROVE monitoring sites can be used to estimate the minimum amount of available background ammonia, assuming that all available ammonia is used to produce the measured sulfate and nitrate.

This can be expressed as follows for concentrations in parts per billion (ppb):

$$[\text{NH}_3]_{\text{ppb}} = [\text{NO}_3^-]_{\text{ppb}} + 2 [\text{SO}_4^{=}]_{\text{ppb}}$$

or for concentrations in $\mu\text{g}/\text{m}^3$:

$$[\text{NH}_3]_{\mu\text{g}/\text{m}^3} = 0.274 [\text{NO}_3^-]_{\mu\text{g}/\text{m}^3} + 0.354 [\text{SO}_4^{=}]_{\mu\text{g}/\text{m}^3}$$

Therefore, the background ammonia concentration used in CALPUFF was computed by analyzing sulfate and nitrate monitoring data collected at the Mesa Verde and Weminuche Class I Areas since March 1988 (IMPROVE 2003).

The first step in the analysis was to create a database that contained all years of data sorted by sampling date. For each valid IMPROVE sample, the background ammonia concentration was computed using the procedure outlined above. When the reported nitrate concentrations were below the reported minimum detection limit, the concentration was set to the detection limit. Using the individual computed ammonia concentration, the monthly and annual average ammonia were computed. A limitation of this analysis is that the nitrate analytical procedure was modified in 1996. It is not known to what extent this change affected the detection limit, analytical accuracy and precision and sample recovery. However, examination of the calculated mean and standard deviation suggests that the variation before and after this change results in the same level of scatter in the data and, at least for this analysis, this was not a significant issue.

Table 6-4 presents the computed monthly, seasonal and annual background ammonia concentrations for the Mesa Verde and Weminuche Class I Areas. As a result of the low seasonal variability in the calculated background ammonia concentrations, an annual average of 0.38 ppb was used for both the Mesa Verde and Weminuche Class I areas in the CALPUFF modeling analysis.

Table 6-4. CALPUFF Background Ammonia Concentrations

| Monthly Average | Mesa Verde (ppb) | Weminuche (ppb) | Average (ppb) |
|-------------------------|-----------------------------|----------------------------|--------------------------|
| January | 0.31 | 0.20 | 0.26 |
| February | 0.31 | 0.22 | 0.26 |
| March | 0.36 | 0.31 | 0.34 |
| April | 0.40 | 0.36 | 0.38 |
| May | 0.46 | 0.42 | 0.44 |
| June | 0.50 | 0.44 | 0.47 |
| July | 0.54 | 0.44 | 0.49 |
| August | 0.55 | 0.45 | 0.50 |
| September | 0.55 | 0.45 | 0.50 |
| October | 0.42 | 0.36 | 0.39 |
| November | 0.32 | 0.20 | 0.26 |
| December | 0.33 | 0.18 | 0.26 |
| Seasonal Average | | | |
| Winter | 0.32 | 0.20 | 0.26 |
| Spring | 0.40 | 0.36 | 0.38 |
| Summer | 0.53 | 0.44 | 0.49 |
| Fall | 0.43 | 0.34 | 0.38 |
| Annual Average | 0.42 | 0.34 | 0.38 |

6.2.2.5 Visibility Calculations

Potential visibility impacts were performed using the FLAG (2000) published procedure to calculate a change in extinction (reported in dv) at mandatory federal PSD Class I Areas. Background extinction conditions were determined based on speciated aerosol samples collected using IMPROVE (2003) monitoring protocols at Mesa Verde National Park and Weminuche Wilderness Area, as well as daily average relative humidity values measured at the Albino Canyon, New Mexico, RAWS location (WRCC 2003) as described in Section 4.2 above. Since potential carbon, primary particulate matter, and sulfur emissions would not be significant from the proposed action (or alternatives), permitted but not yet constructed sources, or other RFS, the visibility impact analysis was based on the maximum daily nitrate ion (NO_3^-) and nitrogen dioxide gas (NO_2) concentrations predicted to occur anywhere within each Class I area.

Microsoft Excel[©] Daily FLAG Refined Analysis Spreadsheets (Archer 2003) for the Mesa Verde National Park and Weminuche Wilderness areas were used to determine the change in extinction as if the maximum daily predicted impacts had occurred during the aerosol sampling period (1988 through 2002). The number of days in excess of a 1.0 dv “Just Noticeable Change,” reported as a range of values for the entire aerosol sampling period, was used as the significance threshold. This threshold is based on the original development of the deciview scale (Pitchford and Malm 1994), and is supported by EPA’s Final Regional Haze Regulation (64 FR 126, July 1, 1999) decision to use of 1.0 dv as the significance level when preparing periodic reasonable progress reports. However, at the request of the USDA-Forest Service, this analysis also reports the predicted range of days in excess of 0.5 dv (1/2 of a “Just Noticeable Change.”)

6.2.2.6 Atmospheric Deposition Calculations

Total predicted dry nitrogen deposition impacts were calculated using the CALPUFF default dry deposition model, dry deposition parameters, and scavenging coefficients. Total predicted wet nitrogen deposition fluxes were computed from the modeled nitrogen species, with a molecular weight adjustment to convert the fluxes to the same units. For total wet nitrogen deposition, the adjustment factors were:

$$\text{Total N} = 0.291667 [\text{SO}_4^{=}] + 0.451613 [\text{NO}_3^{-}] + 0.222222 [\text{HNO}_3] + 0.823529 [\text{NH}_3]$$

Since no large SO₂ emission sources were identified in the proposed action (or alternatives), the permitted but not yet constructed, and other RFS emission source inventories, it was assumed that the change in sulfur deposition would be insignificant. Nitrate ion is assumed to be present as ammonium nitrate secondary particulate matter.

Wet and dry deposition were combined to estimate total nitrogen deposition using the POSTUTIL post processing program. The annual total deposition from each CALPUFF emission source group was calculated separately so that total deposition could be combined for the scenarios of interest. The USDA-Forest Service (Fox, et al 1989) has established a 3 kilogram per hectare per year (kg/ha-yr) total nitrogen deposition acceptable threshold for PSD Class I areas, below which no reductions in emissions would be necessary.

A USDA-Forest Service (2000) has also established a screening methodology to calculate the potential change in ANC at sensitive lakes located within PSD Class I areas. Four sensitive lakes were identified within the Weminuche Wilderness Area, although no sensitive lakes were identified within Mesa Verde National Park. For Upper Grizzly Lake, the minimum measured background ANC was 24.3 µeq/l; the USDA-Forest Service has indicated a threshold of 1 µeq/l change for lakes with background ANC levels less than 25 µeq/l. Since background ANC levels at the remaining three lakes were all above 25 µeq/l, the applicable threshold is a 10 percent change in ANC.

6.3 Construction Impacts

This subsection was originally developed as part of the SUIT Air Quality Analysis (BLM 2000). It is included here for completeness, and is applicable to the proposed action (and alternative) construction impacts.

Construction emissions would primarily occur due to the installation of new wells, which involves three separate, sequential phases:

- well pad and resource road construction;
- rig-up, drill, and rig-down; and
- well completion and testing.

For this analysis, information is not available regarding the actual locations of new wells that would result from the proposed action (or alternatives), nor the likely chronological sequence of their construction. Construction of the additional gas wells and associated equipment from the assumed development would occur over a prolonged period and, for the most part, the resulting air emissions would occur sequentially rather than concurrently. Neither the actual timing of the construction activity at any location nor the chronological sequence of such activities within the overall project can be forecast. For this reason, the impact analysis for the construction phase of the proposed development focused on evaluation of an assumed reasonable, but conservative, construction scenario from a group of four wells.

The scenario selected for the modeling analysis included concurrent, parallel construction of four wells arrayed at the corners of a square with sides of 0.5 mile (805 m). Each of the three project construction activities was assumed to occur simultaneously at all four of these well sites (i.e., resource road and well pad construction at the four locations were assumed to occur on the same three days, etc.) This is a highly unlikely development scenario. Consequently, actual construction impacts are likely to be less than the predicted pollutant concentrations. The assumptions that were used in this analysis are:

- well installation and the associated road building activity would be the primary source of construction phase emissions for the proposed action (and alternatives);
- development of each well and pad was assumed to proceed in a sequential fashion;
- some sizing (hp ratings) and load factors for construction equipment were estimated based on assumptions used in previous analyses for similar projects;
- EPA emission factors were used for estimating construction dust generation and equipment exhaust emissions; and
- SO₂ emissions from natural gas flaring were assumed to be negligible (e.g., the gas would be “sweet.”)

Maximum background concentrations recorded at the Ignacio air quality monitoring site were assumed to represent the combined contributions of non-project emissions throughout the study area. Maximum near-field pollutant concentrations predicted by the ISCST3 model for the selected reasonable, but conservative, well construction emission scenarios were added to the maximum background concentration to produce maximum total concentrations for comparison with the State and NAAQS. These maximum predicted total concentration values (background plus modeled) are expected to overestimate actual construction impacts because these two events would occur under very different meteorological conditions, which are not expected to coincide.

Potential annual average impacts were not predicted, since construction emissions would result from a series of short-duration activities (nearly 36 days total). In addition, the actual number of wells that would be constructed during any particular year is unknown, and due to the wide geographic distribution of these sources, the cumulative annual average concentration is likely to be small. Past experience has shown that maximum predicted concentrations for shorter averaging times (1 to 24 hr) typically govern compliance with ambient standards for construction activities.

The maximum emission rates for each stage of construction were used in the modeling. The highest emission rates for PM₁₀ and SO₂ would occur during the well pad/resource road construction and rig up/drilling/rig down phases, respectively. This modeling approach, with

respect to emissions, is conservative. Hourly meteorological input data for the near-field ISCST3 simulations were developed by the CALMET model. Receptors were located at a minimum distance of 0.12 miles (200 m) from the roads and the well pad. Shorter source-receptor distances were considered inappropriate because the heavy equipment operators would not allow closer public access for safety reasons. The interval between receptors was 100 m. Each well pad was modeled as a volume source with horizontal dimensions of 300 ft x 300 ft. Each resource road (0.5 miles long) was modeled as 66 volume sources (66 segments) with horizontal dimensions of 40 ft x 40 ft.

The actual orientation of potential future pads and resource roads is unknown. However, the relative locations of sources with respect to wind direction could affect the dispersion modeling results. Accordingly, an initial set of test modeling runs was conducted to determine the orientation of project construction sources that would produce the highest predicted impact for each pollutant and averaging time. To accomplish this objective, a small hypothetical volume source was modeled with a year of meteorological data to determine the specific wind direction associated with the highest predicted concentrations for 3 and 24 hr averaging times. The sole purpose of this modeling was to determine the reasonable, but conservative orientation of the well pad and resource road sources to maximize the predicted impacts for different pollutants and averaging times.

Next, these initial test results were used to rotate the four well pad and resource road combinations to maximize the potential emissions of PM₁₀ and SO₂ that would occur along the wind directions identified in the initial simulations. The “maximum impact” alignments of emission sources were then assumed in all subsequent simulations for a particular pollutant averaging time combination.

Receptors for the tests consisted of polar and Cartesian grid receptor networks starting at a distance of 200 m from the source. A variable hourly emission rate option was used for fugitive dust (PM₁₀) since the mechanical disturbance caused by construction equipment would only occur during the 8 hr workday. On the other hand, potential emissions due to well flaring were assumed to occur on a 24 hr basis.

7.0 Assessment of Air Quality Impacts

7.1 Near Field Impacts

7.1.1 State and NAAQS

A modeling analysis of total cumulative air quality impacts was performed to demonstrate that the combined effects of the proposed action (and alternatives), existing (including permitted but not operating sources), and other RFS would not violate applicable State and NAAQS. Total pollutant concentrations were represented by adding the maximum measured background pollutant concentrations for a given averaging period at the Ignacio monitoring station (or other values suggested by CDPHE-APCD) to the maximum predicted concentrations for determining compliance with the State and NAAQS. Compliance with the CO (1- and 8-hr) as well as NO₂ (annual) standards was demonstrated.

Carbon monoxide

Modeling was conducted to demonstrate compliance with the CO 1-hr NAAQS of 40,000 µg/m³ and the 8-hr NAAQS of 10,000 µg/m³ (Table 7-1). Modeling was performed for Alternatives 1, 2 and 5, and for all of these cases, the maximum predicted concentration was less than the EPA significance levels (2,000 µg/m³ for 1-hr and 500 µg/m³ for 8-hr) for potential cumulative impacts. Since the predicted concentrations were below these thresholds, additional cumulative modeling was not conducted because it is very unlikely that these sources in combination with other existing sources would violate the State and NAAQS. This is consistent with EPA and CDPHE-APCD modeling guidelines.

Nitrogen dioxide

Given the large number of NOx emission sources and receptors in the modeling domain, the NO₂ modeling analysis examined separate NOx subgroups, then combined these subgroups with a simple post processing procedure for comparison to the State and NAAQS. This approach is reasonable but conservative since impacts from existing compressors and other SUIT sources were also represented by the maximum background measurements. In addition, due to the complexity of the source inventories, some sources may have been included in more than one of the source group inventories. The separate NOx subgroups as modeled were:

- the Proposed Action (Alternative 1), Alternatives 2 and 5;
- existing State of Colorado Sources;
- existing State of New Mexico Sources;
- existing Tribal Sources; and
- other RFS (SUIT EIS and Farmington RMP) Sources.

Table 7-2 presents the maximum predicted direct and cumulative (including other existing sources, RFS and background) concentrations where the proposed action (and alternative) sources would have their maximum impacts. As indicated in this table, the cumulative impacts are well below the

applicable NO₂ annual State and NAAQS of 100 µg/m³ (Alternative 1 is 38.7 µg/m³, Alternative 2 is 38.4 µg/m³ and Alternative 5 is 37.1 µg/m³).

Table 7-1. Maximum Predicted CO Direct Near Field Impacts (µg/m³)

| | Alternative 1 (Proposed Action) | Alternative 2 (Maximum Development) | Alternative 5 (No Action) |
|---------------------------------------|------------------------------------|----------------------------------------|------------------------------|
| Maximum Direct 1-hr Impact | 991 | 1,218 | 646 |
| EPA Cumulative Significance Threshold | 2,000 | 2,000 | 2,000 |
| Maximum 1-hr Background | 2,286 | 2,286 | 2,286 |
| Total 1-hr Impact | 3,277 | 3,504 | 2,932 |
| 1-hr NAAQS | 40,000 | 40,000 | 40,000 |
| Location of Maximum 1-hr Impact | | | |
| UTM Easting (m) | 274,400 | 250,000 | 250,000 |
| UTM Northing (m) | 4,114,200 | 4,124,900 | 4,124,900 |
| Maximum Direct 8-hr Impact | 389 | 431 | 382 |
| EPA Cumulative Significance Threshold | 500 | 500 | 500 |
| Maximum 8-hr Background | 2,286 | 2,286 | 2,286 |
| Total 8-hr Impact | 2,675 | 2,717 | 2,668 |
| 8-hr NAAQS | 10,000 | 10,000 | 10,000 |
| Location of Maximum 8-hr Impact | | | |
| UTM Easting (m) | 289,610 | 271,800 | 271,800 |
| UTM Northing (m) | 4,120,600 | 4,126,100 | 4,126,100 |

UTM - Universal Transverse Mercator

Table 7-2. Maximum Predicted NO₂ Direct Near Field Impacts (µg/m³)⁽¹⁾

| | Alternative 1 (Proposed Action) | Alternative 2 (Maximum Development) | Alternative 3 (No Action) |
|---------------------------------------------|------------------------------------|----------------------------------------|------------------------------|
| Maximum Direct Annual Impact ⁽²⁾ | 24.8 | 24.8 | 23.6 |
| PSD Class II Increment | 25 | 25 | 25 |
| Maximum Annual Background | 9.4 | 9.4 | 9.4 |
| Other Existing and RFS Impact | 4.5 | 4.2 | 4.1 |
| Total Annual Impact | 38.7 | 38.4 | 37.1 |
| Annual NAAQS | 100 | 100 | 100 |
| Location of Maximum Annual Impact | | | |
| UTM Easting (m) | 289,000 | 288,400 | 288,400 |
| UTM Northing (m) | 4,115,000 | 4,112,800 | 4,112,800 |

⁽¹⁾ At those locations where the proposed action (or alternative) has their maximum predicted impact

⁽²⁾ The maximum predicted impact occurs near the same source in both Alternative 1 and 2.

Table 7-3 presents the maximum total cumulative concentrations where all sources would have their maximum impacts. The majority of the contributions come from existing (Tribal and Colorado) emission source inventories. As indicated, the maximum total cumulative impacts (including background) are just below the applicable NO₂ annual State and NAAQS of 100 µg/m³ (Alternative 1 is 93.0 µg/m³, Alternative 2 is 93.2 µg/m³ and Alternative 5 is 92.8 µg/m³). Therefore, compliance of the annual NO₂ NAAQS is demonstrated. These modeling results are a reasonable but conservative estimate as a result of combining the maximum modeled impacts with the maximum observed background concentrations, and by using EPA's regulatory default NOx to NO₂ conversion rate. In a rural environment, it is likely that the actual conversion rate would be less than the default value of 0.75; consequently, actual impacts are likely to be less than the model estimates.

Table 7-3. Maximum Total NO₂ Cumulative Far Field Impacts (µg/m³) ⁽¹⁾

| | Alternative 1 (Proposed Action) | Alternative 2 (Maximum Development) | Alternative 3 (No Action) |
|-----------------------------------|------------------------------------|----------------------------------------|------------------------------|
| Maximum Direct Annual Impact | 0.83 | 0.99 | 0.61 |
| Maximum Annual Background | 9.4 | 9.4 | 9.4 |
| Other Existing and RFS Impact | 82.8 | 82.8 | 82.8 |
| Total Annual Impact | 93.0 | 93.2 | 92.8 |
| Annual NAAQS | 100 | 100 | 100 |
| Location of Maximum Annual Impact | | | |
| UTM Easting (m) | 253,500 | 253,500 | 253,500 |
| UTM Northing (m) | 4,108,500 | 4,108,500 | 4,108,500 |

⁽¹⁾ At the location of maximum cumulative impact

Figures 7-1 through 7-3 graphically present the spatial distribution of the annual NO₂ concentrations for these alternatives. It is important to note that only a limited area around the maximum total NO₂ cumulative impact exceed 75 µg/m³ and these areas are outside the area of the proposed development. In addition, most of the study area shows predicted impacts below 10 µg/m³.

Figure 7-1. Cumulative Annual Average NO₂ Impacts from Alternative 1 (Proposed Action)

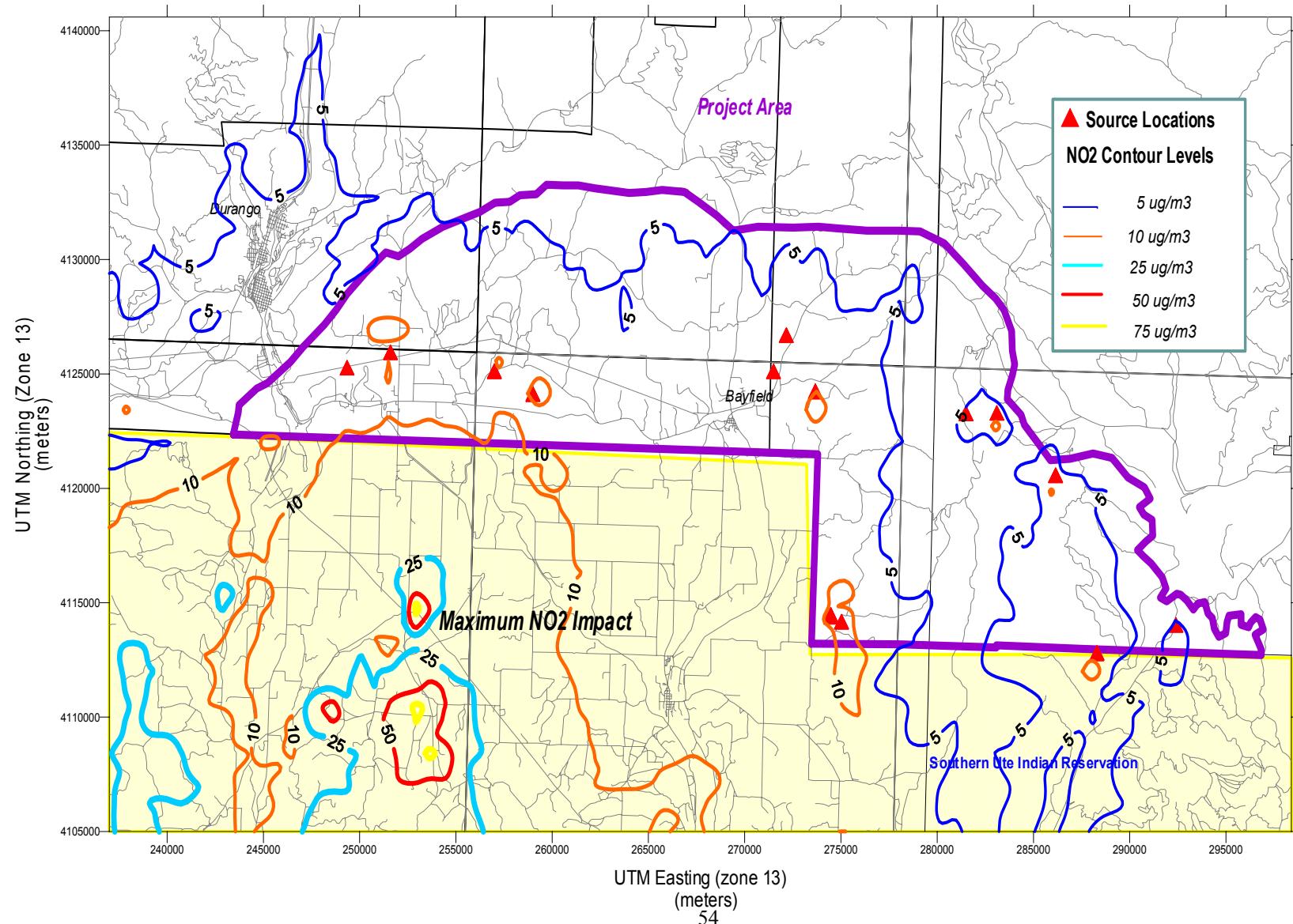


Figure 7-2. Cumulative Annual Average NO₂ Impacts from Alternative 2 (Maximum Development)

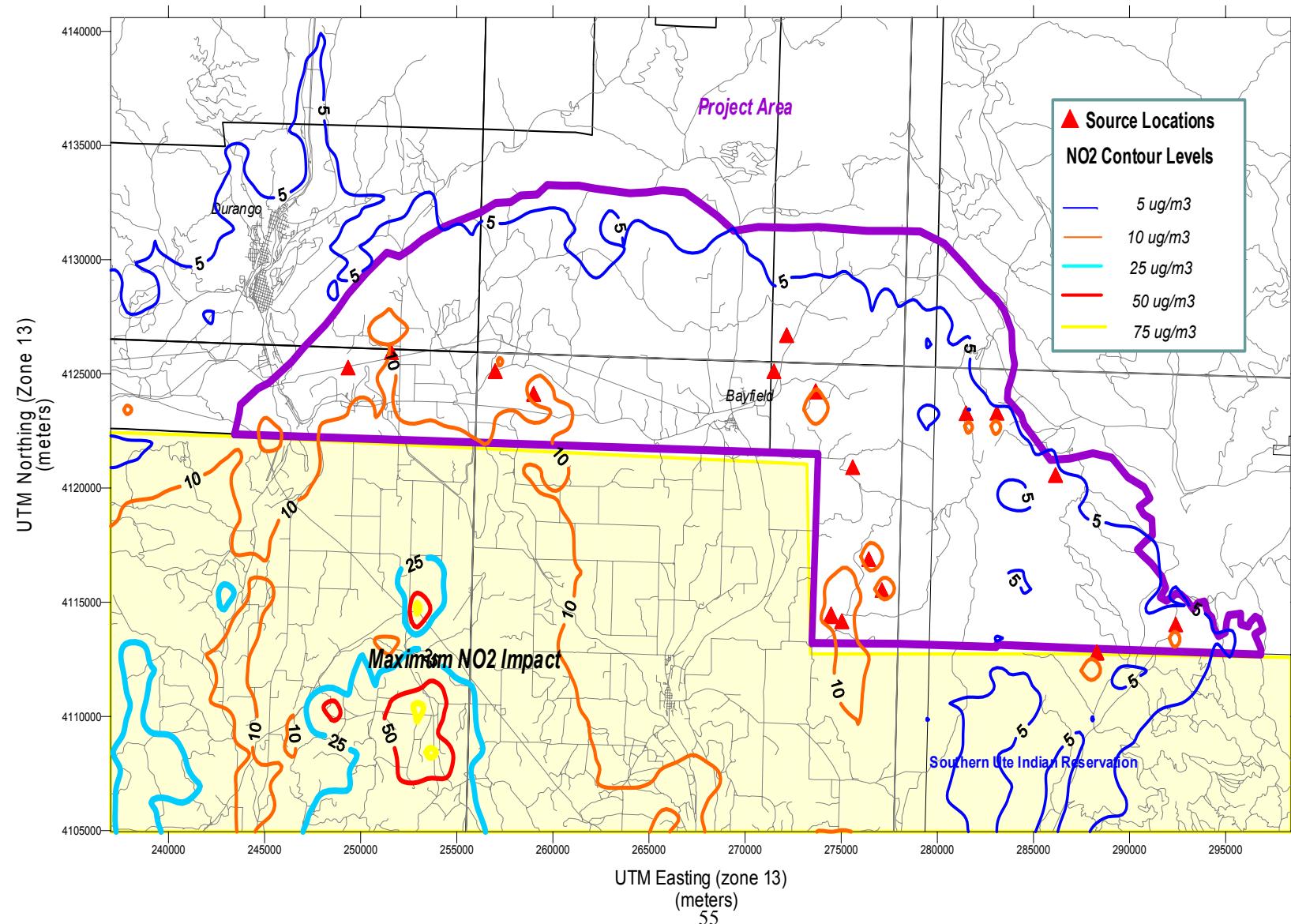
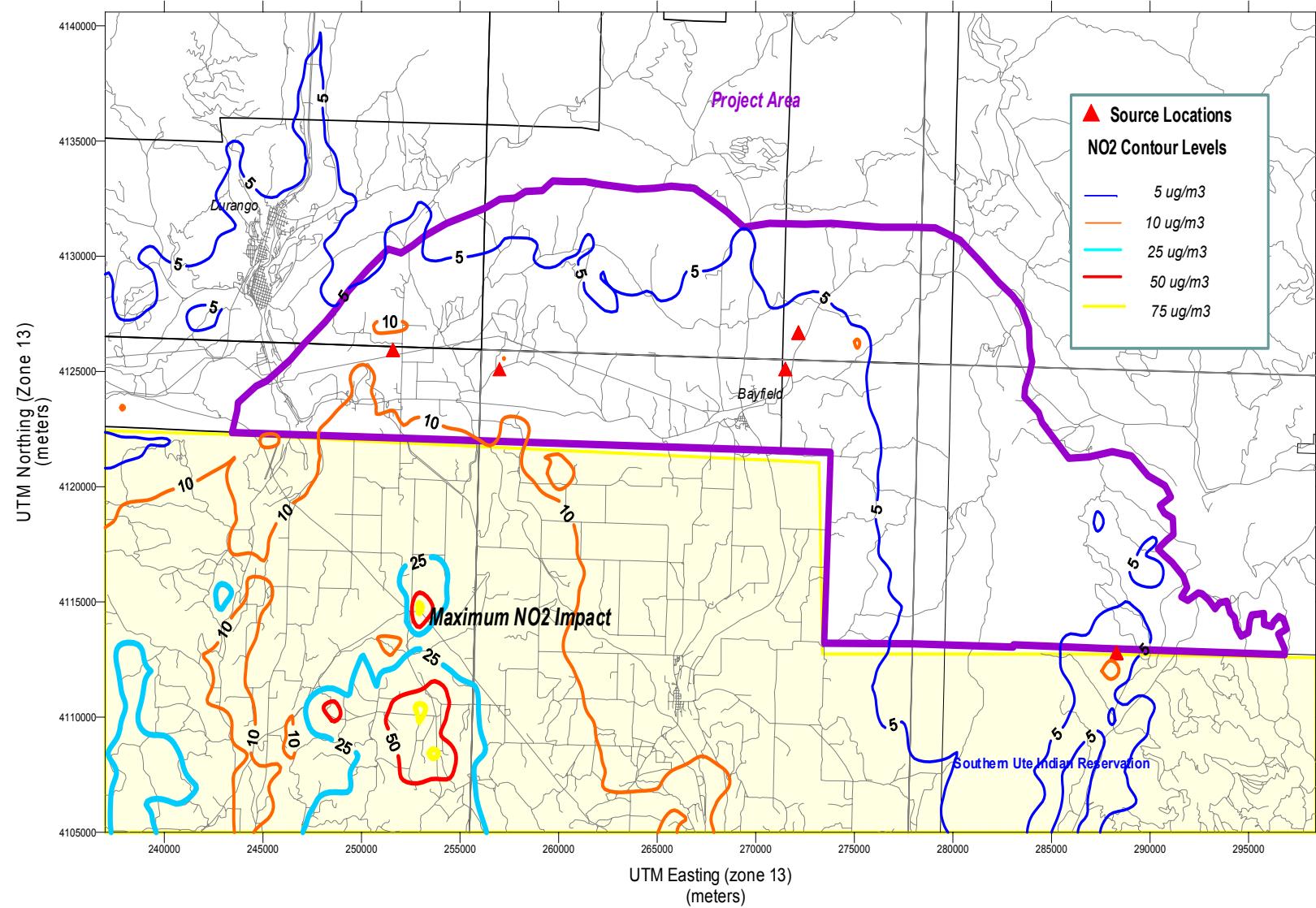


Figure 7-3. Cumulative Annual Average NO₂ Impacts from Alternative 5 (No Action)



7.1.2 PSD Increment Values (Proposed Action and Alternatives)

Near-field modeling was also conducted to compare predicted impacts from the proposed action (and alternatives) directly to PSD Class II increments. Given the lack of detailed engineering data available for this EIS analysis, as well as information regarding which existing sources actually consume the increments, a rigorous PSD analysis is not possible. Further, BLM does not have the regulatory authority to conduct such an analysis. This comparison was made to indicate potential significance only, and is not intended to be a regulatory PSD increment consumption analysis.

The regulatory authority responsible for administrating the PSD program is also responsible for performing a detailed increment analysis; such an analysis would be based on established baseline conditions, permit application data, and existing increment consuming sources, but not sources that are simply undergoing NEPA review. Because this is not a regulatory PSD increment analysis, these results are presented for disclosure purposes only.

Table 7-2 presents maximum predicted NO₂ direct annual impacts for Alternatives 1, 2 and 5. Under Alternatives 1 and 2, the maximum predicted direct annual impacts would be just less than the PSD Class II Increment of 25 $\mu\text{g}/\text{m}^3$, both at 24.8 $\mu\text{g}/\text{m}^3$. This impact was predicted to occur immediately next to the proposed Elmridge 1 compressor station. The maximum impact under Alternative 5 would be 23.6 $\mu\text{g}/\text{m}^3$ which is also less than the applicable PSD Class II Increment.

7.1.3 Incremental Risk from HAPs

As previously stated, the only HAP that would be emitted from the sources associated with the proposed action (and alternatives) is formaldehyde. Maximum cumulative concentrations of formaldehyde associated with the proposed engines (central compressors and small wellhead engines) were used to evaluate incremental health risks. This analysis focused on potential incremental cancer risk to the most likely exposed (MLE) and the maximum exposed individual (MEI). Long-term (annual average) formaldehyde concentrations were adjusted for the expected project lifetime, then multiplied by EPA's formaldehyde unit risk factor, to obtain an estimate of incremental cancer risk. The calculated "cancer risk" reflects the maximum potential incremental risk, but does not represent the total risk to any particular individual.

The incremental cancer risk was based on the maximum predicted annual average formaldehyde concentration, and EPA's unit risk factor of 1.3×10^{-5} (EPA 2003c). The resulting estimated MLE and MEI incremental cancer risks were compared against the cancer risk threshold range of 1 to 100×10^{-6} , (e.g.; 10^{-4} to 10^{-6}). The cancer risk values were also adjusted to account for duration of exposure and time spent at home as detailed below. The EPA MLE criterion assumes that a person would be exposed to the maximum concentration continuously for a period of 70 yr. The criterion allows for an adjustment to reflect the normal years of occupancy at a specific residence.

For the MLE scenario, the exposure duration is assumed to be 9 yr, which corresponds to the mean duration that a family remains at a single residence (EPA 1992). The resulting MLE residency adjustment factor for 9 yr ÷ 70 yr is 0.129. A second daily exposure factor accounts for the percentage of time during any given day that a potentially exposed person is at home. The analysis assumed a maximum "at home" exposure fraction of 0.64. During the remainder of the day, it was

conservatively assumed the same individual would be exposed to 25 percent of the maximum concentration. Therefore, the MLE daily exposure adjustment factor was $[(0.64 \times 1.0)] + [(0.36 \times 0.25)]$, or 0.73. Combining the two adjustment factors for the MLE scenario results in an overall adjustment value of 0.0939 (0.129×0.73).

For the MEI scenario, the exposure duration was assumed to be the life of a typical natural gas well, or 20 yr. Thus, the MEI residency adjustment factor was $20 \text{ yr} \div 70 \text{ yr}$, or 0.286. For the MEI scenario, it was conservatively assumed that a person would remain at home 24 hr per day for the entire 20 yr production period; therefore the daily adjustment factor was 1.0. Combining the two adjustment factors for the MEI scenario results in an overall adjustment value of 0.286 (0.286×1.0).

To calculate the incremental cancer risk for the MLE and MEI scenarios, the maximum annual predicted formaldehyde concentration was first multiplied by EPA's unit risk factor, and then by the appropriate overall adjustment values (Table 7-4). The maximum annual formaldehyde concentration was predicted to be $3.8 \mu\text{g}/\text{m}^3$, at 320-m (nearly 1,050 ft) from a central compressor station for all alternatives. Therefore, the calculated MLE and MEI values became 4.7×10^{-6} and 14.2×10^{-6} , respectively, which are both within the acceptable $1 \text{ to } 100 \times 10^{-6}$ range of risk impacts. Figures 7-4 and 7-5 present risk contours for the MLE and MEI for Alternative 2 (Maximum Development).

Table 7-4. Maximum Predicted Incremental Cancer Risks by Alternative

| Alternative | Maximum conc. ($\mu\text{g}/\text{m}^3$) | UTM Easting (m) | UTM Northing (m) | Unit Risk Factor | MLE exposure factor | MEI exposure factor | Total MLE Risk | Total MEI Risk |
|---------------------|-----------------------------------------------|--------------------|---------------------|-----------------------|---------------------|---------------------|----------------------|-----------------------|
| Proposed Action | 3.8 | 288,400 | 4,112,800 | 1.30×10^{-5} | 0.0939 | 0.286 | 4.7×10^{-6} | 14.2×10^{-6} |
| Maximum Development | 3.8 | 288,400 | 4,112,800 | 1.30×10^{-5} | 0.0939 | 0.286 | 4.7×10^{-6} | 14.2×10^{-6} |
| No Action | 3.8 | 288,400 | 4,112,800 | 1.30×10^{-5} | 0.0939 | 0.286 | 4.7×10^{-6} | 14.2×10^{-6} |

7.2 Far Field Impacts

The far field analysis presents four different combinations of emission source impacts (using CALPUFF) within Mesa Verde National Park and the Weminuche Wilderness PSD Class I Areas. First, direct modeling results are presented for the proposed action and alternative emission sources (Alternatives 1, 2 and 5). Next, these proposed action (and alternative) impacts were combined those from existing New Mexico, Colorado, and Tribal emission sources, as well as other RFS (SUIT EIS) sources. The third analysis included all of the previously mentioned sources, plus other RFS sources identified in the Farmington RMP analysis (including small wellhead engines operating at 9.62 g/hp-hr NOx emissions). The final method was for all of the previous sources, however assuming that the Farmington RMP small wellhead engines would be controlled at a level of 2 g/hp-hr NOx emissions. It should be noted that for this last case, the small engine emissions associated with the Proposed Action (Alternative 1) were assumed to be operating at 10 g/hp-hr NOx emissions.

Figure 7-4. HAP Incremental Risk Analysis for Formaldehyde MLE (Maximum Development)

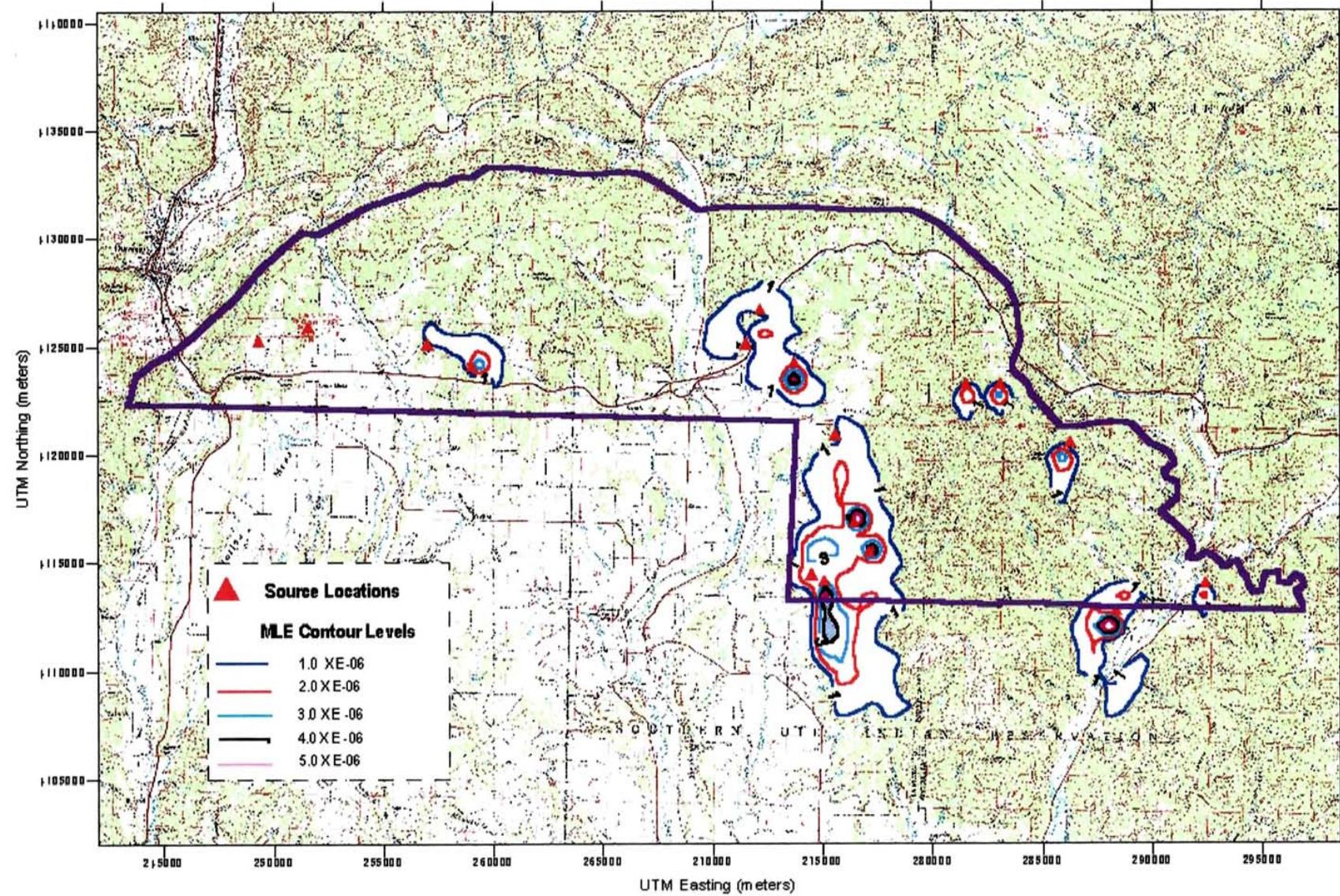
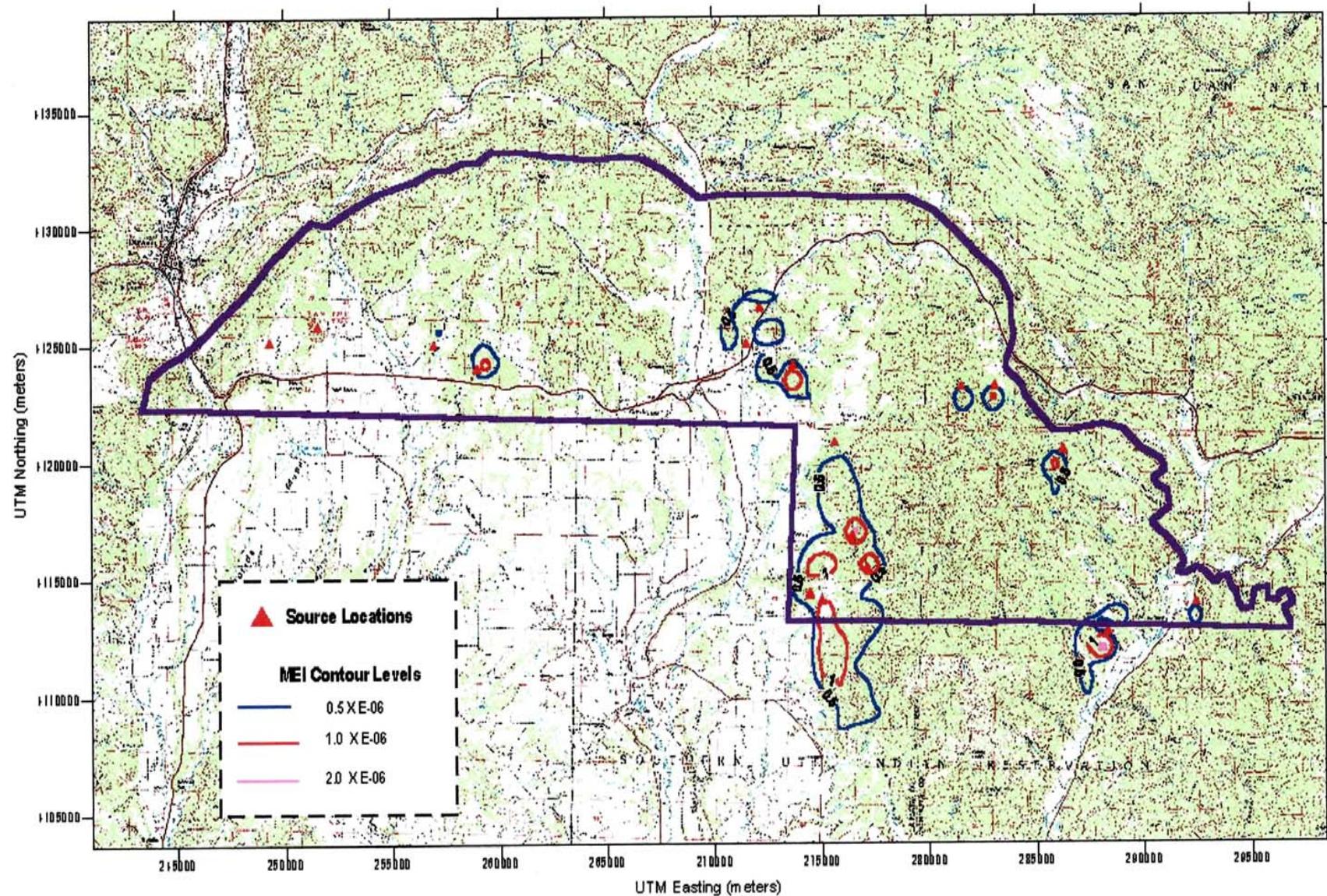


Figure 7-5. HAP Incremental Risk Analysis for Formaldehyde MEI (Maximum Development)



7.2.1 State and NAAQS

A modeling analysis of direct and cumulative air quality impacts was performed to demonstrate the effects of the proposed action (and alternatives) alone, and in conjunction with existing and other RFS, would not result in exceedances of State and NAAQS. Background air pollutant concentrations provided by the State of Colorado for Mesa Verde National Park and the Weminuche Wilderness Area (Table 4-2) were added to the CALPUFF predicted concentrations, and then compared to applicable ambient air quality standards.

Table 7-5 presents a summary of maximum predicted annual average NO₂ concentrations at the Mesa Verde Class I Area under the various emission source combinations. As indicated, all predicted impacts would be well below the applicable annual NO₂ State and NAAQS of 100 µg/m³. The highest predicted direct cumulative NO₂ impacts at Mesa Verde were 0.51 µg/m³ for Alternative 1, 0.57 µg/m³ for Alternative 2 and 0.49 µg/m³ for Alternative 5. When added to an assumed background concentration of 9 µg/m³, total cumulative NO₂ impacts represent nearly 10 percent of the NAAQS. The predicted impacts from the proposed action (and alternatives) sources alone contributed up to 5 percent of the total cumulative predicted impacts.

Table 7-6 presents a summary of maximum predicted annual average NO₂ concentrations at the Weminuche Class I Area under the various emission source combinations. As indicated, all predicted impacts would be well below the applicable annual NO₂ State and NAAQS of 100 µg/m³. The highest predicted direct cumulative NO₂ impacts at Weminuche were 0.27 µg/m³ for Alternative 1, 0.33 µg/m³ for Alternative 2 and 0.21 µg/m³ for Alternative 5. When added to an assumed background concentration of 9 µg/m³, total cumulative NO₂ impacts represent nearly 10 percent of the NAAQS. The predicted impacts from the proposed action (and alternatives) sources alone contributed up to 36 percent of the total cumulative predicted impacts.

7.2.2 PSD Increment Values (Proposed Action and Alternatives)

Far-field modeling was also conducted to compare predicted impacts from the proposed action (and alternatives) directly to PSD Class I increments. Given the lack of detailed engineering data available for this EIS analysis, as well as information regarding which existing sources actually consume the increments, a rigorous PSD analysis is not possible. Further, BLM does not have the regulatory authority to conduct such an analysis. This comparison was made to indicate potential significance only, and is not intended to be a regulatory PSD increment consumption analysis.

The regulatory authority responsible for administrating the PSD program is also responsible for performing a detailed increment analysis; such an analysis would be based on established baseline conditions, permit application data, and existing increment consuming sources, but not sources that are simply undergoing NEPA review. Because this is not a regulatory PSD increment analysis, these results are presented for disclosure purposes only.

As indicated in Tables 7-5 and 7-6, the maximum predicted NO₂ direct annual impacts for Alternatives 1, 2 and 5 were all well below the applicable PSD Class I Increment of 2.5 µg/m³ within both PSD Class I areas.

Table 7-5. Annual Average NO₂ Impact Summary (Mesa Verde)

| Emission Source Group | Maximum Direct Impact ($\mu\text{g}/\text{m}^3$) | UTM Easting (m) | UTM Northing (m) | PSD Class I Increment ($\mu\text{g}/\text{m}^3$) | Percent of PSD Class I Increment | Assumed Background ($\mu\text{g}/\text{m}^3$) | Maximum Total Impact ($\mu\text{g}/\text{m}^3$) | NAAQS ($\mu\text{g}/\text{m}^3$) | Percent of NAAQS |
|---------------------------------------------|----------------------------------------------------|-----------------|------------------|----------------------------------------------------|----------------------------------|-------------------------------------------------|---------------------------------------------------|------------------------------------|------------------|
| Alt 1 (Proposed Action) | 0.02 | 202,555 | 4,123,835 | 2.5 | < 1 | 9 | 9.02 | 100 | 9 |
| Alt 2 (Maximum Development) | 0.03 | 202,555 | 4,123,835 | 2.5 | < 1 | 9 | 9.02 | 100 | 9 |
| Alt 5 (No Action) | 0.00 | 203,775 | 4,125,199 | 2.5 | < 1 | 9 | 9.00 | 100 | 9 |
| | | | | | | | | | |
| Alt 1 + Existing + RFS | 0.25 | 202,555 | 4,123,835 | 2.5 | 10 | 9 | 9.25 | 100 | 9 |
| Alt 2 + Existing + RFS | 0.26 | 202,555 | 4,123,835 | 2.5 | 10 | 9 | 9.26 | 100 | 9 |
| Alt 5 + Existing + RFS | 0.24 | 202,555 | 4,123,835 | 2.5 | 10 | 9 | 9.24 | 100 | 9 |
| | | | | | | | | | |
| Alt 1 + Existing + RFS + FRMP | 0.51 | 202,555 | 4,123,835 | 2.5 | 20 | 9 | 9.51 | 100 | 10 |
| Alt 2 + Existing + RFS + FRMP | 0.57 | 202,555 | 4,123,835 | 2.5 | 21 | 9 | 9.52 | 100 | 10 |
| Alt 5 + Existing + RFS + FRMP | 0.49 | 202,555 | 4,123,835 | 2.5 | 20 | 9 | 9.49 | 100 | 9 |
| | | | | | | | | | |
| Alt 1 + Existing + RFS + FRMP (2.0 g/hp-hr) | 0.37 | 202,555 | 4,123,835 | 2.5 | 15 | 9 | 9.37 | 100 | 9 |
| Alt 2 + Existing + RFS + FRMP (2.0 g/hp-hr) | 0.52 | 202,555 | 4,123,835 | 2.5 | 21 | 9 | 9.52 | 100 | 10 |
| Alt 5 + Existing + RFS + FRMP (2.0 g/hp-hr) | 0.36 | 202,555 | 4,123,835 | 2.5 | 14 | 9 | 9.36 | 100 | 9 |

Table 7-6. Annual Average NO₂ Impact Summary (Weminuche)

| Emission Source Group | Maximum Direct Impact ($\mu\text{g}/\text{m}^3$) | UTM Easting (m) | UTM Northing (m) | PSD Class I Increment ($\mu\text{g}/\text{m}^3$) | Percent of PSD Class I Increment | Assumed Background ($\mu\text{g}/\text{m}^3$) | Maximum Total Impact ($\mu\text{g}/\text{m}^3$) | NAAQS ($\mu\text{g}/\text{m}^3$) | Percent of NAAQS |
|---------------------------------------------|----------------------------------------------------|-----------------|------------------|----------------------------------------------------|----------------------------------|-------------------------------------------------|---------------------------------------------------|------------------------------------|------------------|
| Alt 1 (Proposed Action) | 0.07 | 272,162 | 4,144,211 | 2.5 | 3 | 9 | 9.07 | 100 | 9 |
| Alt 2 (Maximum Development) | 0.12 | 272,162 | 4,144,211 | 2.5 | 5 | 9 | 9.12 | 100 | 9 |
| Alt 5 (No Action) | 0.01 | 272,162 | 4,144,211 | 2.5 | < 1 | 9 | 9.01 | 100 | 9 |
| | | | | | | | | | |
| Alt 1 + Existing + RFS | 0.18 | 272,162 | 4,144,211 | 2.5 | 7 | 9 | 9.18 | 100 | 9 |
| Alt 2 + Existing + RFS | 0.24 | 272,162 | 4,144,211 | 2.5 | 10 | 9 | 9.24 | 100 | 9 |
| Alt 5 + Existing + RFS | 0.12 | 272,162 | 4,144,211 | 2.5 | 5 | 9 | 9.12 | 100 | 9 |
| | | | | | | | | | |
| Alt 1 + Existing + RFS + FRMP | 0.27 | 272,162 | 4,144,211 | 2.5 | 11 | 9 | 9.27 | 100 | 9 |
| Alt 2 + Existing + RFS + FRMP | 0.33 | 272,162 | 4,144,211 | 2.5 | 13 | 9 | 9.33 | 100 | 9 |
| Alt 5 + Existing + RFS + FRMP | 0.21 | 272,162 | 4,144,211 | 2.5 | 8 | 9 | 9.21 | 100 | 9 |
| | | | | | | | | | |
| Alt 1 + Existing + RFS + FRMP (2.0 g/hp-hr) | 0.22 | 272,162 | 4,144,211 | 2.5 | 9 | 9 | 9.22 | 100 | 9 |
| Alt 2 + Existing + RFS + FRMP (2.0 g/hp-hr) | 0.28 | 272,162 | 4,144,211 | 2.5 | 13 | 9 | 9.33 | 100 | 9 |
| Alt 5 + Existing + RFS + FRMP (2.0 g/hp-hr) | 0.16 | 272,162 | 4,144,211 | 2.5 | 7 | 9 | 9.16 | 100 | 9 |

7.2.3 AQRV Impacts

7.2.3.1 Visibility

Tables 7-7 and 7-8 present a summary of the potential cumulative changes in visibility within the Mesa Verde and Weminuche Class I Areas. These tables present the minimum, maximum, and average number of days per year where the reduction in visibility was predicted to exceed a 1.0 dv “just noticeable change” (equivalent to a 10 percent change in extinction). At the request of the USDA-Forest Service, the same information is presented for a 0.5 dv 1/2 of a “just noticeable change” threshold. The maximum predicted single day change in visibility is also presented.

As indicated in Table 7-7, the maximum predicted direct visibility impacts for all alternatives at Mesa Verde are less than 1.0 dv. At Weminuche, up to three days were predicted to exceed 1.0 dv annually under Alternatives 1 and 2 (Table 7-8).

At Mesa Verde (Table 7-7), the maximum cumulative impacts from all sources combined was between 15 and 32 days per year greater than a 1.0 dv “just noticeable change” under Alternative 2 (assuming Farmington RMP small wellhead engines would operate at 9.62 g/hp-hr NO_x emissions). If the Farmington RMP small wellhead engines were limited to 2.0 g/hp-hr NO_x emissions, the maximum cumulative impacts are reduced to between 4 and 16 days greater than a 1.0 dv annually.

At the Weminuche Class I Area (Table 7-8), the maximum cumulative impacts from all sources combined was between 11 and 25 days per year greater than a 1.0 dv “just noticeable change” under Alternative 2 (assuming Farmington RMP small wellhead engines would operate at 9.62 g/hp-hr NO_x emissions). If the Farmington RMP small wellhead engines were limited to 2.0 g/hp-hr NO_x emissions, the maximum cumulative impacts are reduced to between 5 and 17 days greater than a 1.0 dv annually.

7.2.3.2 Atmospheric Deposition

A modeling analysis of total cumulative atmospheric deposition was performed to demonstrate the combined effects of the proposed action (and alternatives) in conjunction with existing and other RFS would not exceed the USDA-Forest Service total nitrogen deposition threshold (Fox, et al 1989) of 3 kg/ha-yr in each Class I area. Since no SO₂ emission sources would be associated with the proposed action (or alternatives), it was assumed that additional sulfur deposition would be negligible. Table 7-9 presents a summary of maximum predicted total annual nitrogen deposition within the Mesa Verde and Weminuche Class I areas. In addition, Figures 7-6 and 7-7 present these modeling results graphically.

The maximum predicted total annual nitrogen deposition within Mesa Verde National Park was 0.22 kg/ha-yr, under the cumulative Maximum Development (Alternative 2) scenario. As indicated in Figure 7-6, the maximum impacts would occur in the southeast corner of Mesa Verde and would decrease towards the northwest.

Table 7-7. Visibility Impact Summary (Mesa Verde)

| Emission Source Group | Maximum Single Day Impact (dv) | Number of Days > 0.5 dv change | | | Number of Days > 1.0 dv change | | |
|---------------------------------------------|--------------------------------|--------------------------------|---------|---------|--------------------------------|---------|---------|
| | | Minimum | Maximum | Average | Minimum | Maximum | Average |
| Alt 1 (Proposed Action) | 0.34 | 0 | 0 | 0 | 0 | 0 | 0 |
| Alt 2 (Maximum Development) | 0.49 | 0 | 0 | 0 | 0 | 0 | 0 |
| Alt 5 (No Action) | 0.12 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | | | | | | |
| Existing + RFS Only | 2.07 | 3 | 18 | 11.2 | 0 | 4 | 1.3 |
| FRMP Only (9.6 g/hp-hr) | 4.59 | 32 | 52 | 40.5 | 7 | 24 | 15.9 |
| FRMP Only (2.0 g/hp-hr) | 2.71 | 6 | 19 | 12.1 | 0 | 5 | 1.5 |
| | | | | | | | |
| Alt 1 + Existing + RFS | 2.31 | 6 | 20 | 12.6 | 0 | 3 | 1.3 |
| Alt 2 + Existing + RFS | 2.44 | 9 | 21 | 14.2 | 0 | 4 | 1.7 |
| Alt 5 + Existing + RFS | 2.13 | 6 | 18 | 10.5 | 0 | 3 | 1.3 |
| | | | | | | | |
| Alt 1 + Existing + RFS + FRMP | 6.25 | 36 | 65 | 52.9 | 14 | 31 | 20.8 |
| Alt 2 + Existing + RFS + FRMP | 6.34 | 37 | 64 | 53.5 | 15 | 32 | 22.2 |
| Alt 5 + Existing + RFS + FRMP | 6.12 | 36 | 61 | 51.5 | 11 | 32 | 20.3 |
| | | | | | | | |
| Alt 1 + Existing + RFS + FRMP (2.0 g/hp-hr) | 3.84 | 23 | 43 | 31.2 | 4 | 11 | 7.5 |
| Alt 2 + Existing + RFS + FRMP (2.0 g/hp-hr) | 3.97 | 24 | 48 | 32.4 | 4 | 16 | 8.2 |
| Alt 5 + Existing + RFS + FRMP (2.0 g/hp-hr) | 3.66 | 21 | 43 | 30.6 | 3 | 13 | 7.0 |

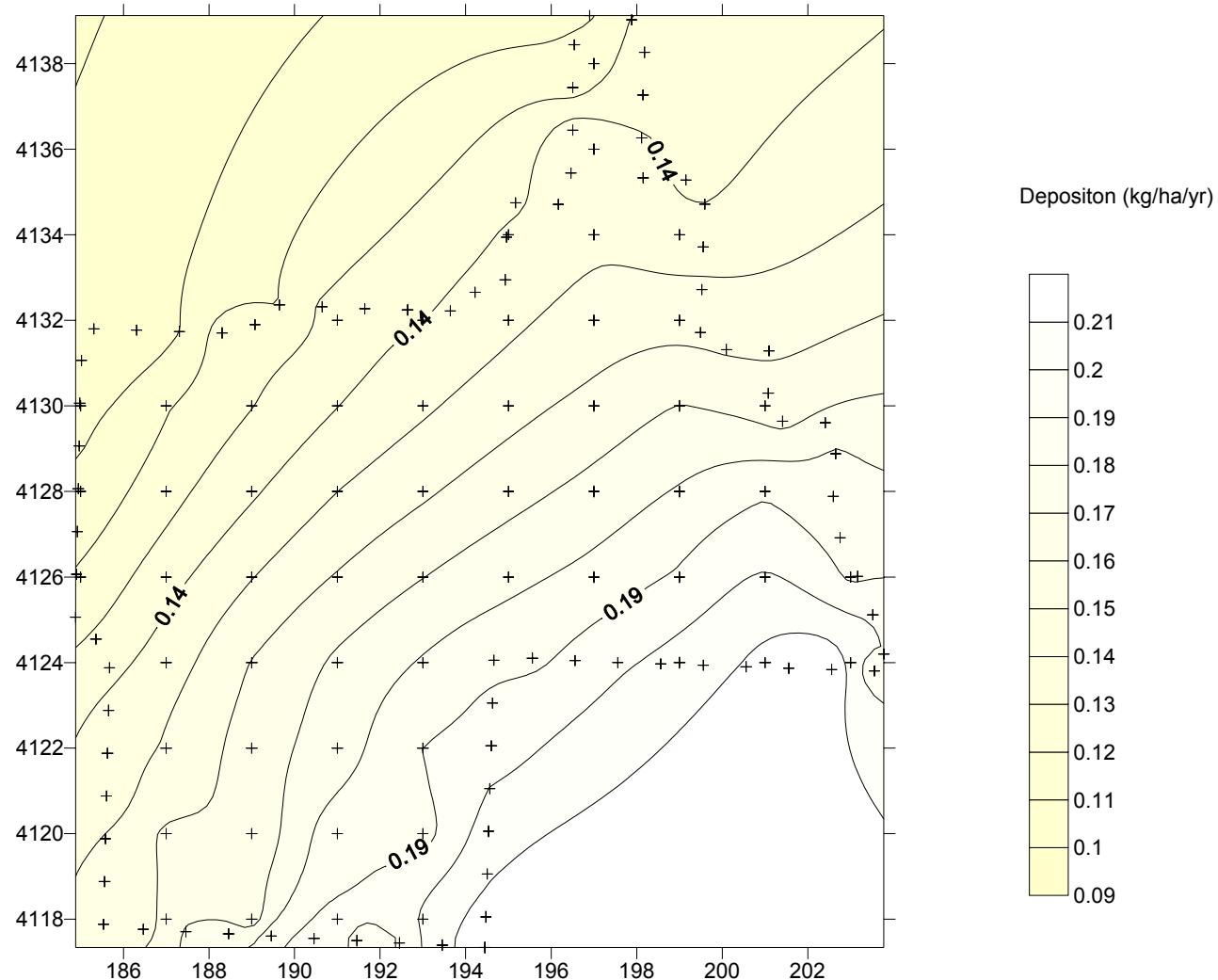
Table 7-8. Visibility Impact Summary (Weminuche)

| Emission Source Group | Maximum Single Day Impact (dv) | Number of Days > 0.5 dv change | | | Number of Days > 1.0 dv change | | |
|---------------------------------------------|--------------------------------|--------------------------------|---------|---------|--------------------------------|---------|---------|
| | | Minimum | Maximum | Average | Minimum | Maximum | Average |
| Alt 1 (Proposed Action) | 1.67 | 2 | 11 | 4.9 | 0 | 3 | 0.9 |
| Alt 2 (Maximum Development) | 1.59 | 1 | 10 | 4.5 | 0 | 3 | 0.5 |
| Alt 5 (No Action) | 0.37 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | | | | | | |
| Existing + RFS Only | 1.67 | 3 | 16 | 7.8 | 0 | 5 | 1.3 |
| FRMP Only (9.6 g/hp-hr) | 3.52 | 10 | 22 | 15.3 | 1 | 12 | 4.3 |
| FRMP Only (2.0 g/hp-hr) | 1.37 | 1 | 8 | 3.5 | 0 | 2 | 0.4 |
| | | | | | | | |
| Alt 1 + Existing + RFS | 2.14 | 1 | 12 | 6.7 | 0 | 3 | 1.1 |
| Alt 2 + Existing + RFS | 2.51 | 12 | 30 | 19.5 | 0 | 12 | 4.7 |
| Alt 5 + Existing + RFS | 1.93 | 3 | 17 | 9.1 | 0 | 6 | 1.6 |
| | | | | | | | |
| Alt 1 + Existing + RFS + FRMP | 4.75 | 25 | 47 | 36.0 | 9 | 21 | 15.0 |
| Alt 2 + Existing + RFS + FRMP | 4.98 | 34 | 53 | 43.5 | 11 | 25 | 18.0 |
| Alt 5 + Existing + RFS + FRMP | 4.93 | 23 | 42 | 32.5 | 5 | 20 | 12.5 |
| | | | | | | | |
| Alt 1 + Existing + RFS + FRMP (2.0 g/hp-hr) | 3.13 | 15 | 35 | 24.3 | 2 | 15 | 7.9 |
| Alt 2 + Existing + RFS + FRMP (2.0 g/hp-hr) | 4.04 | 23 | 43 | 30.0 | 5 | 17 | 10.1 |
| Alt 5 + Existing + RFS + FRMP (2.0 g/hp-hr) | 2.75 | 12 | 27 | 18.8 | 1 | 12 | 5.2 |

Table 7-9. Atmospheric Deposition Impact Summary

| Emission Source Group | Mesa Verde National Park | | | Weminuche Wilderness Area | | |
|---------------------------------------------|-------------------------------|-----------------|------------------|-------------------------------|-----------------|------------------|
| | Maximum Deposition (kg/ha-yr) | UTM Easting (m) | UTM Northing (m) | Maximum Deposition (kg/ha-yr) | UTM Easting (m) | UTM Northing (m) |
| Alt 1 (Proposed Action) | 0.009 | 202.555 | 4123.835 | 0.007 | 272,162 | 4,144,211 |
| Alt 2 (Maximum Development) | 0.013 | 202.555 | 4123.835 | 0.054 | 272,162 | 4,144,211 |
| Alt 5 (No Action) | 0.002 | 203.775 | 4124.199 | 0.006 | 272,162 | 4,144,211 |
| | | | | | | |
| Alt 1 + Existing + RFS | 0.097 | 202.555 | 4123.835 | 0.070 | 271,000 | 4,146,000 |
| Alt 2 + Existing + RFS | 0.101 | | | 0.109 | 271,000 | 4,146,000 |
| Alt 5 + Existing + RFS | 0.091 | 202.555 | 4123.835 | 0.069 | 271,000 | 4,146,000 |
| | | 202.555 | 4123.835 | | | |
| Alt 1 + Existing + RFS + FRMP | 0.216 | 202.555 | 4123.835 | 0.142 | 271,000 | 4,146,000 |
| Alt 2 + Existing + RFS + FRMP | 0.220 | | | 0.181 | 271,000 | 4,146,000 |
| Alt 5 + Existing + RFS + FRMP | 0.210 | 194.451 | 4117.34 | 0.142 | 271,000 | 4,146,000 |
| | | 194.451 | 4117.34 | | | |
| Alt 1 + Existing + RFS + FRMP (2.0 g/hp-hr) | 0.152 | | | 0.102 | 271,000 | 4,146,000 |
| Alt 2 + Existing + RFS + FRMP (2.0 g/hp-hr) | 0.156 | 202.555 | 4123.835 | 0.141 | 271,000 | 4,146,000 |
| Alt 5 + Existing + RFS + FRMP (2.0 g/hp-hr) | 0.146 | 202.555 | 4123.835 | 0.102 | 271,000 | 4,146,000 |

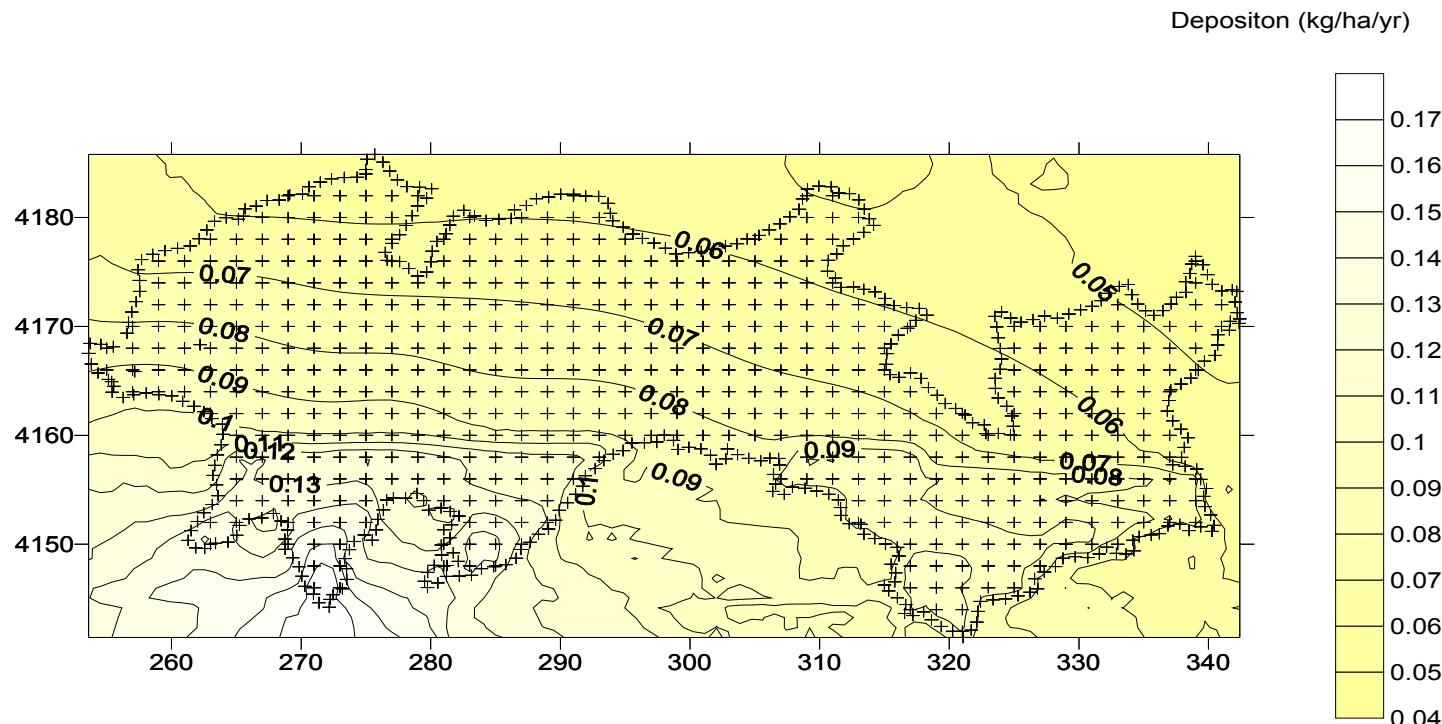
Figure 7-6. Cumulative Mesa Verde Atmospheric Deposition Levels (Maximum Development)



Notes: 1) + Indicates impact modeling receptor locations

2) Emission source groups include Alternative 2 (Maximum Development), Existing Sources, and Other RFS (SUIT EIS and Farmington RMP) Sources

Figure 7-7. Cumulative Weminuche Atmospheric Deposition Levels (Maximum Development)



Notes: 1) + Indicates impact modeling receptor locations

2) Emission source groups include Alternative 2 (Maximum Development), Existing Sources, and Other RFS (SUIT EIS and Farmington RMP) Sources

The maximum predicted total annual nitrogen deposition within the Weminuche Wilderness Area was 0.18 kg/ha-yr, also under the cumulative Maximum Development (Alternative 2) scenario. Figure 7-7 shows the maximum impacts would occur along the southwestern boundary of the Weminuche Class I Area, and would decrease towards the north.

The USDA-Forest Service (2000) screening methodology was used to calculate the potential ANC change at four sensitive lakes, all located within the Weminuche Wilderness Area. No sensitive lakes were identified within Mesa Verde National Park.

Potential changes in ANC at all four lakes (Table 7-10) were below the USDA-Forest Service ten percent change threshold. However, since the background ANC for Upper Grizzly Lake is just under 25 µeq/l (at 24.3 µeq/l), its applicable threshold is a 1.0 µeq/l change. For Upper Grizzly Lake, this corresponds to a 4.1 percent ANC change. Therefore, a “significant, adverse” impact to Upper Grizzly Lake chemistry was predicted to occur for all cumulative scenarios which include potential Farmington RMP emission sources.

Table 7-10. Maximum Predicted Cumulative ANC Changes

| Emission Source Group | Potential Change in ANC (percent) | | | |
|---------------------------------------------|-----------------------------------|---------------------|--------------------|---------------------|
| | Eldorado Lake | Lower Sunlight Lake | Upper Grizzly Lake | Upper Sunlight Lake |
| Alt 1 (Proposed Action) | 0.23 | 0.09 | 0.75 | 0.36 |
| Alt 2 (Maximum Development) | 0.37 | 0.14 | 1.21 | 0.57 |
| Alt 5 (No Action) | 0.08 | 0.03 | 0.26 | 0.12 |
| Alt 1 + Existing + RFS | 1.14 | 0.41 | 3.41 | 1.82 |
| Alt 2 + Existing + RFS | 1.29 | 0.47 | 3.87 | 2.05 |
| Alt 5 + Existing + RFS | 1.00 | 0.35 | 2.92 | 1.55 |
| Alt 1 + Existing + RFS + FRMP | 2.79 | 0.99 | 8.11 | 4.31 |
| Alt 2 + Existing + RFS + FRMP | 2.93 | 1.05 | 8.57 | 4.55 |
| Alt 5 + Existing + RFS + FRMP | 2.64 | 0.93 | 7.62 | 4.04 |
| Alt 1 + Existing + RFS + FRMP (2.0 g/hp-hr) | 1.89 | 0.64 | 5.07 | 2.80 |
| Alt 2 + Existing + RFS + FRMP (2.0 g/hp-hr) | 2.03 | 0.70 | 5.54 | 3.03 |
| Alt 5 + Existing + RFS + FRMP (2.0 g/hp-hr) | 1.74 | 0.59 | 4.58 | 2.53 |

7.3 Construction Impacts

This subsection was originally developed as part of the SUIT Air Quality Analysis (BLM 2000). It is included here for completeness, and is applicable to the proposed action (and alternative) construction impacts.

The SUIT Air Quality analysis performed a detailed impact analysis for the construction phase of development (BLM 2000). No new information was available to revise estimates of these impacts. Therefore, Table 7-11 presents modeling results from the previous study which are directly

applicable to this analysis. These results reflect the reasonable but conservative assumption of four closely spaced well pads developed concurrently.

Table 7-11. Maximum Predicted PM₁₀ and SO₂ Impacts During Construction

| Pollutant | Averaging Period | Maximum Direct Impact ($\mu\text{g}/\text{m}^3$) | Background ($\mu\text{g}/\text{m}^3$) | Maximum Total Impact ⁽¹⁾ ($\mu\text{g}/\text{m}^3$) | NAAQS ($\mu\text{g}/\text{m}^3$) | Percent of NAAQS |
|------------------|------------------|----------------------------------------------------|-----------------------------------------|------------------------------------------------------------------|------------------------------------|---------------------|
| PM ₁₀ | 24-hr | 77 | 50 | 127 | 150 | 85 |
| sulfur dioxide | 3-hr | 645 | 57 | 702 | 1300 | 54 |
| | 3-hr | 645 | 57 | 702 | 700 ⁽²⁾ | >100 ⁽²⁾ |
| | 24-hr | 109 | 23 | 132 | 365 | 36 |

⁽¹⁾ It was conservatively assumed that the maximum modeled predicted concentration would occur concurrently with the maximum measured background concentration.

⁽²⁾ Colorado State Ambient Air Quality Standard

The maximum potential 24 hr PM₁₀ concentrations at least 650 ft (200 m) from a road, and 0.5 miles (805 m) from well emission sources, were predicted to be nearly 127 $\mu\text{g}/\text{m}^3$ (including background), and therefore below the applicable State and NAAQS of 150 $\mu\text{g}/\text{m}^3$. In addition, the predicted PM₁₀ concentrations decrease rapidly away from the construction emission sources. Since these PM₁₀ construction emissions would be temporary, PSD increments are not applicable.

The maximum short-term SO₂ emissions would result from burning diesel fuel (containing trace amounts of sulfur) in drilling rigs and heavy-equipment engines. The maximum modeled concentrations (including representative background) were predicted to be nearly 702 $\mu\text{g}/\text{m}^3$ (3 hr) and 132 $\mu\text{g}/\text{m}^3$ (24 hr). Therefore, predicted short-term (3 hr) SO₂ concentrations were slightly above the restrictive Colorado SO₂ Ambient Air Quality Standard of 700 $\mu\text{g}/\text{m}^3$, but well below the longer-term (24 hr) State and NAAQS of 365 $\mu\text{g}/\text{m}^3$. The 3 hr SO₂ NAAQS (1,300 $\mu\text{g}/\text{m}^3$) is less stringent. Given the reasonable but conservative assumptions used in this modeling analysis, significant impacts are unlikely to actually occur, even when compared to the more restrictive Colorado 3 hr standard. Since these diesel-related SO₂ construction emissions are temporary, PSD increments are not applicable.

8.0 Potential Mitigation Alternatives

Additional analyses were conducted to evaluate the potential visibility benefits of installing small wellhead engines under the Proposed Action (Alternative 1) at a NOx emission rate of 2.0 g/hp-hr. This was in addition to assuming that the Farmington RMP small wellhead engines would also be limited to 2.0 g/hp-hr NOx. A small wellhead engine NOx emission rate of 10 g/hp-hr had been assumed for the proposed action (and alternatives) impact results described in Section 7.0 above. The visibility modeling results for these additional analyses are provided in Tables 8-1 and 8-2.

At the Mesa Verde Class I Area (regardless of the small wellhead engine emission rate), no days were predicted to be greater than 1.0 dv from the Proposed Action (Alternative 1) emission sources alone. Cumulatively, installing 2.0 g/hp-hr small wellhead engines under the Proposed Action (Alternative 1) would reduce the potential exceedances of 1.0 dv by one day per year.

At the Weminuche Class I Area, installing 2.0 g/hp-hr small wellhead engines under the Proposed Action (Alternative 1) would eliminate the potential direct exceedances of 1.0 dv (from a previous maximum of three days per year). Cumulatively, installing 2.0 g/hp-hr small wellhead engines would reduce the maximum annual potential exceedances by three days (from up to 15 days to 12 or less days per year.)

Table 8-1. Proposed Action with Additional Small Wellhead Engine Emission Controls - Visibility Impact Summary (Mesa Verde)

| Emission Source Group | Maximum Single Day Impact (dv) | Number of Days > 0.5 dv change | | | Number of Days > 1.0 dv change | | |
|-----------------------------------------------------------|--------------------------------|--------------------------------|---------|---------|--------------------------------|---------|---------|
| | | Minimum | Maximum | Average | Minimum | Maximum | Average |
| Alt 1 (Proposed Action) (10 g/hp-hr) | 0.34 | 0 | 0 | 0 | 0 | 0 | 0 |
| Alt 1 (Proposed Action) (2.0 g/hp-hr) | 0.19 | 0 | 0 | 0 | 0 | 0 | 0 |
| Alt 1 (10 g/hp-hr) + Existing + RFS + FRMP (2.0 g/hp-hr) | 3.84 | 23 | 43 | 31.2 | 4 | 11 | 7.5 |
| Alt 1 (2.0 g/hp-hr) + Existing + RFS + FRMP (2.0 g/hp-hr) | 3.73 | 20 | 43 | 29.1 | 3 | 10 | 6.5 |

Table 8-2. Proposed Action with Additional Small Wellhead Engine Emission Controls - Visibility Impact Summary (Weminuche)

| Emission Source Group | Maximum Single Day Impact (dv) | Number of Days > 0.5 dv change | | | Number of Days > 1.0 dv change | | |
|-----------------------------------------------------------|--------------------------------|--------------------------------|---------|---------|--------------------------------|---------|---------|
| | | Minimum | Maximum | Average | Minimum | Maximum | Average |
| Alt 1 (Proposed Action) (10 g/hp-hr) | 1.67 | 2 | 11 | 4.9 | 0 | 3 | 0.9 |
| Alt 1 (Proposed Action) (2.0 g/hp-hr) | 0.42 | 0 | 0 | 0 | 0 | 0 | 0 |
| Alt 1 (10 g/hp-hr) + Existing + RFS + FRMP (2.0 g/hp-hr) | 3.13 | 15 | 35 | 24.3 | 2 | 15 | 7.9 |
| Alt 1 (2.0 g/hp-hr) + Existing + RFS + FRMP (2.0 g/hp-hr) | 2.91 | 16 | 30 | 21.7 | 2 | 12 | 6.1 |

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Appendix A – Proposed Action and Alternatives Emission Inventory

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Table A-1. Summary of Proposed Action and Alternatives Central Compressor Stations

| Site | Alternative | | | | |
|---------------|-------------|---|---|---|---|
| | 1 | 2 | 3 | 4 | 5 |
| Bayfield | X | X | X | X | X |
| BP Amoco 1 | X | X | | | |
| BP Amoco 2 | X | X | | | |
| BP Amoco 3 | X | X | X | X | |
| BP Amoco 4 | X | X | X | X | X |
| Cross Timbers | X | X | X | X | X |
| Elmridge 1 | X | X | X | X | X |
| Elmridge 2 | X | X | X | X | |
| Independent 1 | | X | | | |
| Independent 2 | | X | | | |
| Independent 3 | | X | | | |
| Petrox 1 | X | X | X | | |
| Petrox 2 | X | X | X | X | |
| Petrox 3 | X | X | X | | |
| Petrox 4 | X | X | X | | |
| Pure 1 | X | X | | | X |
| Pure 2 | X | X | | | X |

Note: X indicates Central Compressor Station included in Alternative emission inventory.

Table A-2. Summary of Emissions by Alternative

| Proposed Alternative | Central Compression Capacity (hp) | Wellhead Engine Capacity (hp) | Total Capacity (hp) | Compressors | | | Wells | | Dehydrators | | Wellhead Engines | | | Total Emissions | | |
|--------------------------|-----------------------------------|-------------------------------|---------------------|-------------|-----------|-------------|------------|-----------|-------------|-----------|------------------|-----------|-------------|-----------------|-----------|-------------|
| | | | | NOx (t/yr) | CO (t/yr) | HAPs (t/yr) | NOx (t/yr) | CO (t/yr) | NOx (t/yr) | CO (t/yr) | NOx (t/yr) | CO (t/yr) | HAPs (t/yr) | NOx (t/yr) | CO (t/yr) | HAPs (t/yr) |
| 1 Proposed Action | 41,000 | 14,352 | 55,352 | 616 | 821 | 94 | 32 | 27 | 61 | 52 | 731 | 631 | 9.7 | 1,440 | 1,531 | 104 |
| 2 Maximum Development | 46,000 | 25,248 | 71,248 | 688 | 917 | 105 | 57 | 48 | 74 | 63 | 1,267 | 1,095 | 16.7 | 2,087 | 2,122 | 122 |
| 3 No Wells in HD Mtns | 28,640 | 10,416 | 39,056 | 502 | 669 | 77 | 23 | 19 | 44 | 37 | 560 | 483 | 7.4 | 1,128 | 1,209 | 84 |
| 4 Current Management | 30,400 | 9,072 | 39,472 | 435 | 580 | 71 | 21 | 17 | 31 | 26 | 476 | 411 | 6.3 | 963 | 1,036 | 77 |
| 5 No Action | 14,240 | 6,384 | 20,624 | 206 | 275 | 32 | 13 | 11 | 26 | 22 | 342 | 296 | 5.0 | 58 | 604 | 36 |

Table A-3. Summary of Emissions by Site and Source Type

| Alternative 1 | NOx (t/yr) | NOx (%) | CO (t/yr) | CO (%) | HAPs (t/yr) | HAPs (%) |
|----------------------|-------------------|----------------|------------------|---------------|--------------------|-----------------|
| Compressors Engines | 616 | 43 | 821 | 54 | 94 | 91 |
| Separators | 32 | 2 | 27 | 2 | --- | 0 |
| Dehydrators | 61 | 4 | 52 | 3 | --- | 0 |
| Wellhead Engines | 731 | 51 | 631 | 41 | 10 | 9 |
| Total | 1,440 | 100 | 1,531 | 100 | 104 | 100 |
| | | | | | | |
| | | | | | | |
| Alternative 2 | NOx (t/yr) | NOx (%) | CO (t/yr) | CO (%) | HAPs (t/yr) | HAPs (%) |
| Compressors Engines | 688 | 33 | 917 | 44 | 105 | 86 |
| Separators | 57 | 3 | 48 | 2 | --- | 0 |
| Dehydrators | 74 | 4 | 37 | 2 | --- | 0 |
| Wellhead Engines | 1,267 | 61 | 1,095 | 52 | 17 | 14 |
| Total | 2,087 | 100 | 2,097 | 100 | 122 | 100 |
| | | | | | | |
| | | | | | | |
| Alternative 3 | NOx (t/yr) | NOx (%) | CO (t/yr) | CO (%) | HAPs (t/yr) | HAPs (%) |
| Compressors Engines | 502 | 44 | 669 | 55 | 77 | 91 |
| Separators | 23 | 2 | 19 | 2 | --- | 0 |
| Dehydrators | 44 | 4 | 37 | 3 | --- | 0 |
| Wellhead Engines | 560 | 50 | 483 | 40 | 7 | 9 |
| Total | 1,128 | 100 | 1,209 | 100 | 84 | 100 |
| | | | | | | |
| | | | | | | |
| Alternative 4 | NOx (t/yr) | NOx (%) | CO (t/yr) | CO (%) | HAPs (t/yr) | HAPs (%) |
| Compressors Engines | 436 | 45 | 581 | 56 | 71 | 92 |
| Separators | 21 | 2 | 17 | 2 | --- | 0 |
| Dehydrators | 31 | 3 | 26 | 2 | --- | 0 |
| Wellhead Engines | 476 | 49 | 411 | 40 | 6 | 8 |
| Total | 963 | 100 | 1,036 | 100 | 77 | 100 |
| | | | | | | |
| | | | | | | |
| Alternative 5 | NOx (t/yr) | NOx (%) | CO (t/yr) | CO (%) | HAPs (t/yr) | HAPs (%) |
| Compressors Engines | 206 | 35 | 275 | 46 | 32 | 87 |
| Separators | 13 | 2 | 11 | 2 | --- | 0 |
| Dehydrators | 26 | 4 | 22 | 4 | --- | 0 |
| Wellhead Engines | 342 | 58 | 296 | 49 | 5 | 13 |
| Total | 588 | 100 | 604 | 100 | 36 | 100 |

Table A-4. Summary of Emissions by Site – Alternative 1 (Proposed Action)

| Source Group | Total Compressor | | NOx | | | CO | | | Facility Total | |
|---------------|------------------|---------------|--------------|-------------|-------------|--------------|-------------|-------------|----------------|--------------|
| | | | Compressors | Separators | Dehydrators | Compressors | Separators | Dehydrators | NOx | CO |
| | hp | % of total hp | (t/yr) | (t/yr) | (t/yr) | (t/yr) | (t/yr) | (t/yr) | (t/yr) | (t/yr) |
| Bayfield | 2,000 | 4.9 | 29.0 | 1.6 | 4.4 | 38.6 | 1.3 | 3.7 | 34.9 | 43.6 |
| BP Amoco 1 | 4,000 | 9.8 | 57.9 | 3.2 | 4.4 | 77.3 | 2.7 | 3.7 | 65.5 | 83.6 |
| BP Amoco 2 | 3,000 | 7.3 | 43.5 | 2.4 | 4.4 | 57.9 | 2.0 | 3.7 | 50.2 | 63.6 |
| BP Amoco 3 | 3,000 | 7.3 | 43.5 | 2.4 | 4.4 | 57.9 | 2.0 | 3.7 | 50.2 | 63.6 |
| BP Amoco 4 | 4,000 | 9.8 | 57.9 | 3.2 | 4.4 | 77.3 | 2.7 | 3.7 | 65.5 | 83.6 |
| Cross Timbers | 2,500 | 6.1 | 36.2 | 2.0 | 4.4 | 48.3 | 1.7 | 3.7 | 42.6 | 53.6 |
| Elmridge 1 | 5,000 | 12.2 | 72.4 | 4.0 | 4.4 | 96.6 | 3.3 | 3.7 | 80.8 | 103.6 |
| Elmridge 2 | 12,000 | 29.3 | 195.5 | 9.5 | 4.4 | 260.7 | 8.0 | 3.7 | 209.4 | 272.4 |
| Petrox 1 | 620 | 1.5 | 9.0 | 0.5 | 4.4 | 12.0 | 0.4 | 3.7 | 13.9 | 16.1 |
| Petrox 2 | 1,900 | 4.6 | 27.5 | 1.5 | 4.4 | 36.7 | 1.3 | 3.7 | 33.4 | 41.6 |
| Petrox 3 | 620 | 1.5 | 9.0 | 0.5 | 4.4 | 12.0 | 0.4 | 3.7 | 13.9 | 16.1 |
| Petrox 4 | 620 | 1.5 | 9.0 | 0.5 | 4.4 | 12.0 | 0.4 | 3.7 | 13.9 | 16.1 |
| Pure 1 | 1,500 | 3.7 | 21.7 | 1.2 | 4.4 | 29.0 | 1.0 | 3.7 | 27.3 | 33.6 |
| Pure 2 | 240 | 0.6 | 3.5 | 0.2 | 4.4 | 4.6 | 0.2 | 3.7 | 8.0 | 8.5 |
| Total | 41,000 | 100.0 | 615.6 | 32.4 | 61.3 | 820.8 | 27.2 | 51.5 | 709.3 | 899.6 |

Table A-5. Summary of Emissions by Site – Alternative 2 (Maximum Development)

| Source Group | Total Compressor | | NOx | | | CO | | | Facility Total | |
|---------------|------------------|---------------|--------------|-------------|-------------|--------------|-------------|-------------|----------------|---------------|
| | | | Compressors | Separators | Dehydrators | Compressors | Separators | Dehydrators | NOx | CO |
| | hp | % of total hp | (t/yr) | (t/yr) | (t/yr) | (t/yr) | (t/yr) | (t/yr) | (t/yr) | (t/yr) |
| Bayfield | 2,000 | 4.3 | 29.0 | 2.5 | 4.4 | 38.6 | 2.1 | 3.7 | 35.8 | 44.4 |
| BP Amoco 1 | 4,000 | 8.7 | 57.9 | 5.0 | 4.4 | 77.3 | 4.2 | 3.7 | 67.3 | 85.1 |
| BP Amoco 2 | 3,000 | 6.5 | 43.5 | 3.7 | 4.4 | 57.9 | 3.1 | 3.7 | 51.6 | 64.8 |
| BP Amoco 3 | 3,000 | 6.5 | 43.5 | 3.7 | 4.4 | 57.9 | 3.1 | 3.7 | 51.6 | 64.8 |
| BP Amoco 4 | 4,000 | 8.7 | 57.9 | 5.0 | 4.4 | 77.3 | 4.2 | 3.7 | 67.3 | 85.1 |
| Cross Timbers | 2,500 | 5.4 | 36.2 | 3.1 | 4.4 | 48.3 | 2.6 | 3.7 | 43.7 | 54.6 |
| Independent 1 | 1,000 | 2.2 | 14.5 | 1.2 | 4.4 | 19.3 | 1.0 | 3.7 | 20.1 | 24.0 |
| Independent 2 | 2,000 | 4.3 | 29.0 | 2.5 | 4.4 | 38.6 | 2.1 | 3.7 | 35.8 | 44.4 |
| Independent 3 | 2,000 | 4.3 | 29.0 | 2.5 | 4.4 | 38.6 | 2.1 | 3.7 | 35.8 | 44.4 |
| Elmridge 1 | 5,000 | 10.9 | 72.4 | 6.2 | 4.4 | 96.6 | 5.2 | 3.7 | 83.0 | 105.5 |
| Elmridge 2 | 12,000 | 26.1 | 195.5 | 14.9 | 4.4 | 260.7 | 12.5 | 3.7 | 214.8 | 276.9 |
| Petrox 1 | 620 | 1.3 | 9.0 | 0.8 | 4.4 | 12.0 | 0.6 | 3.7 | 14.1 | 16.3 |
| Petrox 2 | 1,900 | 4.1 | 27.5 | 2.4 | 4.4 | 36.7 | 2.0 | 3.7 | 34.3 | 42.4 |
| Petrox 3 | 620 | 1.3 | 9.0 | 0.8 | 4.4 | 12.0 | 0.6 | 3.7 | 14.1 | 16.3 |
| Petrox 4 | 620 | 1.3 | 9.0 | 0.8 | 4.4 | 12.0 | 0.6 | 3.7 | 14.1 | 16.3 |
| Pure 1 | 1,500 | 3.3 | 21.7 | 1.9 | 4.4 | 29.0 | 1.6 | 3.7 | 28.0 | 34.2 |
| Pure 2 | 240 | 0.5 | 3.5 | 0.3 | 4.4 | 4.6 | 0.3 | 3.7 | 8.2 | 8.6 |
| Total | 46,000 | 100.0 | 688.0 | 57.2 | 74.5 | 917.4 | 48.0 | 62.5 | 819.7 | 1027.9 |

Table A-6. Summary of Emissions by Site – Alternative 3 (No Wells in HD Mountains)

| Source Group | Total Compressor | | NOx | | | CO | | | Facility Total | |
|---------------|------------------|---------------|--------------|-------------|-------------|--------------|-------------|-------------|----------------|--------------|
| | | | Compressors | Separators | Dehydrators | Compressors | Separators | Dehydrators | NOx | CO |
| | hp | % of total hp | (t/yr) | (t/yr) | (t/yr) | (t/yr) | (t/yr) | (t/yr) | (t/yr) | (t/yr) |
| Bayfield | 2,000 | 7.1 | 29.0 | 1.6 | 4.4 | 38.6 | 1.4 | 3.7 | 35.0 | 43.7 |
| BP Amoco 3 | 3,000 | 10.7 | 43.5 | 2.5 | 4.4 | 57.9 | 2.1 | 3.7 | 50.3 | 63.7 |
| BP Amoco 4 | 4,000 | 14.2 | 57.9 | 3.3 | 4.4 | 77.3 | 2.8 | 3.7 | 65.6 | 83.7 |
| Cross Timbers | 2,500 | 8.9 | 36.2 | 2.1 | 4.4 | 48.3 | 1.7 | 3.7 | 42.7 | 53.7 |
| Elmridge 1 | 5,000 | 17.8 | 72.4 | 4.1 | 4.4 | 96.6 | 3.5 | 3.7 | 80.9 | 103.7 |
| Elmridge 2 | 12,000 | 42.6 | 195.5 | 9.9 | 4.4 | 260.7 | 8.3 | 3.7 | 209.8 | 272.7 |
| Petrox 1 | 620 | 2.2 | 9.0 | 0.5 | 4.4 | 12.0 | 0.4 | 3.7 | 13.9 | 16.1 |
| Petrox 2 | 1,900 | 6.8 | 27.5 | 1.6 | 4.4 | 36.7 | 1.3 | 3.7 | 33.5 | 41.7 |
| Petrox 3 | 620 | 2.2 | 9.0 | 0.5 | 4.4 | 12.0 | 0.4 | 3.7 | 13.9 | 16.1 |
| Pure 1 | 1,500 | 5.3 | 21.7 | 1.2 | 4.4 | 29.0 | 1.0 | 3.7 | 27.3 | 33.7 |
| Total | 28,140 | 100.0 | 501.8 | 23.2 | 43.8 | 669.0 | 19.5 | 36.8 | 572.9 | 728.8 |

Table A-7. Summary of Emissions by Site – Alternative 4 (Current Development)

| Source Group | Total Compressor | | NOx | | | CO | | | Facility Total | |
|---------------|------------------|---------------|--------------|-------------|-------------|--------------|-------------|-------------|----------------|--------------|
| | | | Compressors | Separators | Dehydrators | Compressors | Separators | Dehydrators | NOx | CO |
| | hp | % of total hp | (t/yr) | (t/yr) | (t/yr) | (t/yr) | (t/yr) | (t/yr) | (t/yr) | (t/yr) |
| Bayfield | 2,000 | 6.6 | 29.0 | 1.4 | 4.4 | 38.6 | 1.1 | 3.7 | 34.7 | 43.4 |
| BP Amoco 3 | 3,000 | 9.9 | 43.5 | 2.0 | 4.4 | 57.9 | 1.7 | 3.7 | 49.9 | 63.3 |
| BP Amoco 4 | 4,000 | 13.2 | 57.9 | 2.7 | 4.4 | 77.3 | 2.3 | 3.7 | 65.0 | 83.2 |
| Cross Timbers | 2,500 | 8.2 | 36.2 | 1.7 | 4.4 | 48.3 | 1.4 | 3.7 | 42.3 | 53.4 |
| Elmridge 1 | 5,000 | 16.4 | 72.4 | 3.4 | 4.4 | 96.6 | 2.8 | 3.7 | 80.2 | 103.1 |
| Elmridge 2 | 12,000 | 39.5 | 195.5 | 8.1 | 4.4 | 260.7 | 6.8 | 3.7 | 208.1 | 271.2 |
| Petrox 2 | 1,900 | 6.3 | 9.0 | 1.3 | 4.4 | 12.0 | 1.1 | 3.7 | 14.6 | 16.7 |
| Total | 30,400 | 100.0 | 443.5 | 20.6 | 30.7 | 591.4 | 17.3 | 25.8 | 494.8 | 634.4 |

Table A-8. Summary of Emissions by Site – Alternative 5 (No Action)

| Source Group | Total Compressor | | NOx | | | CO | | | Facility Total | |
|---------------|------------------|---------------|--------------|-------------|-------------|--------------|-------------|-------------|----------------|--------------|
| | | | Compressors | Separators | Dehydrators | Compressors | Separators | Dehydrators | NOx | CO |
| | hp | % of total hp | (t/yr) | (t/yr) | (t/yr) | (t/yr) | (t/yr) | (t/yr) | (t/yr) | (t/yr) |
| Bayfield | 2,000 | 14.0 | 29.0 | 1.8 | 4.4 | 38.6 | 1.5 | 3.7 | 35.2 | 43.8 |
| BP Amoco 3 | 3,000 | 21.1 | 43.5 | 2.7 | 4.4 | 57.9 | 2.3 | 3.7 | 50.6 | 63.9 |
| Cross Timbers | 2,500 | 17.6 | 36.2 | 2.3 | 4.4 | 48.3 | 1.9 | 3.7 | 42.9 | 53.9 |
| Elmridge 1 | 5,000 | 35.1 | 72.4 | 4.5 | 4.4 | 96.6 | 3.8 | 3.7 | 81.3 | 104.1 |
| Pure 1 | 1,500 | 10.5 | 21.7 | 1.4 | 4.4 | 29.0 | 1.1 | 3.7 | 27.5 | 33.8 |
| Pure 2 | 240 | 1.7 | 3.5 | 0.2 | 4.4 | 4.6 | 0.2 | 3.7 | 8.1 | 8.5 |
| Total | 14,240 | 100.0 | 206.3 | 12.9 | 26.3 | 275.0 | 10.9 | 22.1 | 245.5 | 308.0 |

Table A-9. Potential Central Compressor Emissions and Modeling Assumptions (Bayfield)

| Location | Elevation (ft) | Latitude | Longitude | Jurisdiction |
|------------------|----------------|-------------|---------------|--------------|
| T34N, R7W, Sec 1 | 6,934 | 37° 14' 43" | -107° 34' 34" | Private |

| Unit ID | Source Type | Size ⁽¹⁾ (hp) | UTM | | NOx ⁽²⁾ | | CO ⁽³⁾ | | HAP ⁽⁴⁾ | | Stack Parameters | | | | Building Size | |
|-----------------------------------|---------------------------------|-----------------------------|----------------|-----------------|--------------------|-------------|-------------------|-------------|--------------------|------------|------------------|--------------|-------------------|-----------------|---------------|--------------|
| | | | Easting (m) | Northing (m) | (g/s) | (t/yr) | (g/s) | (t/yr) | (g/s) | (t/yr) | Height (m) | Temp (°K) | Velocity (m/s) | Diameter (m) | Height (m) | Width (m) |
| BAY1 | Natural Gas Engine | 2,000 | 271,500 | 4,125,000 | 0.83 | 29.0 | 1.11 | 38.6 | 0.13 | 4.4 | 7.5 | 644 | 28.6 | 0.46 | 4.9 | 4.9 |
| Compressor Engine Subtotal | | 2,000 | | | 0.83 | 29.0 | 1.11 | 38.6 | 0.13 | 4.4 | | | | | | |
| BAYDEH | Dehydration Unit ⁽⁵⁾ | | 271,500 | 4,125,010 | 0.13 | 4.4 | 0.11 | 3.7 | 0.00 | 0.0 | 3.0 | 533 | 6.4 | 0.20 | 2.0 | 2.0 |
| BAYSEP | Separator ⁽⁵⁾ | | 271,500 | 4,125,020 | 0.07 | 2.5 | 0.06 | 2.1 | 0.00 | 0.0 | 3.0 | 533 | 6.4 | 0.20 | 2.0 | 2.0 |
| Facility Total | | | | | 1.03 | 35.8 | 1.28 | 44.4 | 0.13 | 4.4 | | | | | | |

⁽¹⁾ Assumed unit capacity is based on typical installations

⁽²⁾ Assumed NOx emission rate – 1.50 g/hp-hr

⁽³⁾ Assumed CO emission rate – 2.00 g/hp-hr

⁽⁴⁾ Assumed HAP emission rate – 0.23 g/hp-hr

⁽⁵⁾ Dehydration/separator emissions based on 10 MMBtu/hr heater at each compressor site

Table A-10. Potential Central Compressor Emissions and Modeling Assumptions (BP Amoco 1)

| Location | Elevation (ft) | Latitude | Longitude | Jurisdiction |
|------------------|----------------|-------------|---------------|--------------|
| T34N, R6W, Sec 5 | 7,141 | 37° 14' 16" | -107° 33' 05" | Federal |

| Unit ID | Source Type | Size ⁽¹⁾ (hp) | UTM | | NOx ⁽²⁾ | | CO ⁽³⁾ | | HAP ⁽⁴⁾ | | Stack Parameters | | | | Building Size | |
|-----------------------------------|---------------------------------|-----------------------------|----------------|-----------------|--------------------|-------------|-------------------|-------------|--------------------|------------|------------------|--------------|-------------------|-----------------|---------------|--------------|
| | | | Easting (m) | Northing (m) | (g/s) | (t/yr) | (g/s) | (t/yr) | (g/s) | (t/yr) | Height (m) | Temp (°K) | Velocity (m/s) | Diameter (m) | Height (m) | Width (m) |
| BP1A | Natural Gas Engine | 1,333 | 273,670 | 4,124,111 | 0.56 | 19.3 | 0.74 | 25.8 | 0.09 | 3.0 | 4.6 | 644 | 18.4 | 0.46 | 3.0 | 3.0 |
| BP1B | Natural Gas Engine | 1,333 | 273,670 | 4,124,121 | 0.56 | 19.3 | 0.74 | 25.8 | 0.09 | 3.0 | 4.6 | 644 | 18.4 | 0.46 | 3.0 | 3.0 |
| BPIC | Natural Gas Engine | 1,333 | 273,670 | 4,124,131 | 0.56 | 19.3 | 0.74 | 25.8 | 0.09 | 3.0 | 4.6 | 644 | 18.4 | 0.46 | 3.0 | 3.0 |
| Compressor Engine Subtotal | | 4,000 | | | 1.67 | 57.9 | 2.22 | 77.3 | 0.26 | 8.9 | | | | | | |
| BP1DEH | Dehydration Unit ⁽⁵⁾ | | 273,670 | 4,124,141 | 0.13 | 4.4 | 0.11 | 3.7 | 0.00 | 0.0 | 3.0 | 533 | 6.4 | 0.15 | 2.0 | 2.0 |
| BP1SEP | Separator ⁽⁵⁾ | | 273,670 | 4,124,151 | 0.14 | 5.0 | 0.12 | 4.2 | 0.00 | 0.0 | 3.0 | 533 | 6.4 | 0.15 | 2.0 | 2.0 |
| Facility Total | | | | | 1.94 | 67.3 | 2.45 | 85.1 | 0.26 | 8.9 | | | | | | |

⁽¹⁾ Assumed unit capacity is based on typical installations

⁽²⁾ Assumed NOx emission rate – 1.50 g/hp-hr

⁽³⁾ Assumed CO emission rate – 2.00 g/hp-hr

⁽⁴⁾ Assumed HAP emission rate – 0.23 g/hp-hr

⁽⁵⁾ Dehydration/separator emissions based on 10 MMBtu/hr heater at each compressor site

Table A-11. Potential Central Compressor Emissions and Modeling Assumptions (BP Amoco 2)

| Location | Elevation (ft) | Latitude | Longitude | Jurisdiction |
|---------------------|----------------|-------------|---------------|--------------|
| T34NU, R6W, Sec 32U | 6,799 | 37° 08' 51" | -107° 32' 00" | Federal |

| Unit ID | Source Type | Size ⁽¹⁾ (hp) | UTM | | NOx ⁽²⁾ | | CO ⁽³⁾ | | HAP ⁽⁴⁾ | | Stack Parameters | | | | Building Size | |
|-----------------------------------|---------------------------------|--------------------------|------------|-------------|--------------------|-------------|-------------------|-------------|--------------------|------------|------------------|-----------|----------------|--------------|---------------|-----------|
| | | | Eastng (m) | Northng (m) | (g/s) | (t/yr) | (g/s) | (t/yr) | (g/s) | (t/yr) | Height (m) | Temp (°K) | Velocity (m/s) | Diameter (m) | Height (m) | Width (m) |
| BP2A | Natural Gas Engine | 1,500 | 275,030 | 4,114,050 | 0.63 | 21.7 | 0.83 | 29.0 | 0.10 | 3.3 | 4.6 | 644 | 29.9 | 0.38 | 3.0 | 3.0 |
| BP2B | Natural Gas Engine | 1,500 | 275,030 | 4,114,060 | 0.63 | 21.7 | 0.83 | 29.0 | 0.10 | 3.3 | 4.6 | 644 | 29.9 | 0.38 | 3.0 | 3.0 |
| Compressor Engine Subtotal | | 3,000 | | | 1.25 | 43.5 | 1.67 | 57.9 | 0.19 | 6.7 | | | | | | |
| | | | | | | | | | | | | | | | | |
| BP2DEH | Dehydration Unit ⁽⁵⁾ | | 275,030 | 4,114,070 | 0.13 | 4.4 | 0.11 | 3.7 | 0.00 | 0.0 | 3.0 | 533 | 6.4 | 0.15 | 2.0 | 2.0 |
| BP2SEP | Separator ⁽⁵⁾ | | 275,030 | 4,114,080 | 0.11 | 3.7 | 0.09 | 3.1 | 0.00 | 0.0 | 3.0 | 533 | 6.4 | 0.15 | 2.0 | 2.0 |
| Facility Total | | | | | 1.48 | 51.6 | 1.86 | 64.8 | 0.19 | 6.7 | | | | | | |

⁽¹⁾ Assumed unit capacity is based on typical installations

⁽²⁾ Assumed NOx emission rate – 1.50 g/hp-hr

⁽³⁾ Assumed CO emission rate – 2.00 g/hp-hr

⁽⁴⁾ Assumed HAP emission rate – 0.23 g/hp-hr

⁽⁵⁾ Dehydration/separator emissions based on 10 MMBtu/hr heater at each compressor site

Table A-12. Potential Central Compressor Emissions and Modeling Assumptions (BP Amoco 3)

| Location | Elevation (ft) | Latitude | Longitude | Jurisdiction |
|-------------------|----------------|-------------|---------------|--------------|
| T35N, R6W, Sec 31 | 6,996 | 37° 15' 35" | -107° 34' 09" | Private |

| Unit ID | Source Type | Size ⁽¹⁾ (hp) | UTM | | NOx ⁽²⁾ | | CO ⁽³⁾ | | HAP ⁽⁴⁾ | | Stack Parameters | | | | Building Size | |
|-----------------------------------|---------------------------------|--------------------------|------------|-------------|--------------------|-------------|-------------------|-------------|--------------------|------------|------------------|-----------|----------------|--------------|---------------|-----------|
| | | | Eastng (m) | Northng (m) | (g/s) | (t/yr) | (g/s) | (t/yr) | (g/s) | (t/yr) | Height (m) | Temp (°K) | Velocity (m/s) | Diameter (m) | Height (m) | Width (m) |
| BP3A | Natural Gas Engine | 1,500 | 272,164 | 4,126,575 | 0.63 | 21.7 | 0.83 | 29.0 | 0.10 | 3.3 | 4.6 | 644 | 29.9 | 0.38 | 3.0 | 3.0 |
| BP3B | Natural Gas Engine | 1,500 | 272,164 | 4,126,585 | 0.63 | 21.7 | 0.83 | 29.0 | 0.10 | 3.3 | 4.6 | 644 | 29.9 | 0.38 | 3.0 | 3.0 |
| Compressor Engine Subtotal | | 3,000 | | | 1.25 | 43.5 | 1.67 | 57.9 | 0.19 | 6.7 | | | | | | |
| | | | | | | | | | | | | | | | | |
| BP3DEH | Dehydration Unit ⁽⁵⁾ | | 272,164 | 4,126,595 | 0.13 | 4.4 | 0.11 | 3.7 | 0.00 | 0.0 | 3.0 | 533 | 6.4 | 0.15 | 2.0 | 2.0 |
| BP3SEP | Separator ⁽⁵⁾ | | 272,164 | 4,126,605 | 0.11 | 3.7 | 0.09 | 3.1 | 0.00 | 0.0 | 3.0 | 533 | 6.4 | 0.15 | 2.0 | 2.0 |
| Facility Total | | | | | 1.48 | 51.6 | 1.86 | 64.8 | 0.19 | 6.7 | | | | | | |

⁽¹⁾ Assumed unit capacity is based on typical installations

⁽²⁾ Assumed NOx emission rate – 1.50 g/hp-hr

⁽³⁾ Assumed CO emission rate – 2.00 g/hp-hr

⁽⁴⁾ Assumed HAP emission rate – 0.23 g/hp-hr

⁽⁵⁾ Dehydration/separator emissions based on 10 MMBtu/hr heater at each compressor site

Table A-13. Potential Central Compressor Emissions and Modeling Assumptions (BP Amoco 4)

| Location | Elevation (ft) | Latitude | Longitude | Jurisdiction |
|-------------------|----------------|-------------|---------------|--------------|
| T34N, R8W, Sec 11 | 7,082 | 37° 14' 00" | -107° 43' 00" | Federal |

| Unit ID | Source Type | Size ⁽¹⁾ (hp) | UTM | | NOx ⁽²⁾ | | CO ⁽³⁾ | | HAP ⁽⁴⁾ | | Stack Parameters | | | | Building Size | |
|-----------------------------------|---------------------------------|--------------------------|-------------|--------------|--------------------|-------------|-------------------|-------------|--------------------|------------|------------------|-----------|----------------|--------------|---------------|-----------|
| | | | Eastинг (m) | Northинг (m) | (g/s) | (t/yr) | (g/s) | (t/yr) | (g/s) | (t/yr) | Height (m) | Temp (°K) | Velocity (m/s) | Diameter (m) | Height (m) | Width (m) |
| BP4A | Natural Gas Engine | 1,333 | 259,000 | 4,124,000 | 0.56 | 19.3 | 0.74 | 25.8 | 0.09 | 3.0 | 4.6 | 644 | 18.4 | 0.46 | 3.0 | 3.0 |
| BP4B | Natural Gas Engine | 1,333 | 259,000 | 4,124,010 | 0.56 | 19.3 | 0.74 | 25.8 | 0.09 | 3.0 | 4.6 | 644 | 18.4 | 0.46 | 3.0 | 3.0 |
| BP4C | Natural Gas Engine | 1,333 | 259,000 | 4,124,020 | 0.56 | 19.3 | 0.74 | 25.8 | 0.09 | 3.0 | 4.6 | 644 | 18.4 | 0.46 | 3.0 | 3.0 |
| BP4DEH | | | | | | | | | | | | | | | | |
| BP4SEP | | | | | | | | | | | | | | | | |
| Compressor Engine Subtotal | | 4,000 | | | 1.67 | 57.9 | 2.22 | 77.3 | 0.26 | 8.9 | | | | | | |
| | | | | | | | | | | | | | | | | |
| BP4DEH | Dehydration Unit ⁽⁵⁾ | | 259,000 | 4,124,030 | 0.13 | 4.4 | 0.11 | 3.7 | 0.00 | 0.0 | 3.0 | 533 | 6.4 | 0.15 | 2.0 | 2.0 |
| BP4SEP | Separator ⁽⁵⁾ | | 259,000 | 4,124,040 | 0.14 | 5.0 | 0.12 | 4.2 | 0.00 | 0.0 | 3.0 | 533 | 6.4 | 0.15 | 2.0 | 2.0 |
| Facility Total | | | | | 1.94 | 67.3 | 2.45 | 85.1 | 0.26 | 8.9 | | | | | | |

Table A-14. Potential Central Compressor Emissions and Modeling Assumptions (Cross Timbers)

| Location | Elevation (ft) | Latitude | Longitude | Jurisdiction |
|------------------|----------------|-------------|---------------|--------------|
| T34N, R8W, Sec 9 | 6,934 | 37° 14' 30" | -107° 44' 22" | State |

| Unit ID | Source Type | Size ⁽¹⁾ (hp) | UTM | | NOx ⁽²⁾ | | CO ⁽³⁾ | | HAP ⁽⁴⁾ | | Stack Parameters | | | | Building Size | |
|-----------------------------------|---------------------------------|--------------------------|-------------|--------------|--------------------|-------------|-------------------|-------------|--------------------|------------|------------------|-----------|----------------|--------------|---------------|-----------|
| | | | Eastинг (m) | Northинг (m) | (g/s) | (t/yr) | (g/s) | (t/yr) | (g/s) | (t/yr) | Height (m) | Temp (°K) | Velocity (m/s) | Diameter (m) | Height (m) | Width (m) |
| HUB1 | Natural Gas Engine | 1,250 | 257,000 | 4,125,000 | 0.52 | 18.1 | 0.69 | 24.1 | 0.08 | 2.8 | 4.6 | 644 | 17.3 | 0.46 | 3.0 | 3.0 |
| HUB2 | Natural Gas Engine | 1,250 | 257,000 | 4,125,010 | 0.52 | 18.1 | 0.69 | 24.1 | 0.08 | 2.8 | 4.6 | 644 | 17.3 | 0.46 | 3.0 | 3.0 |
| Compressor Engine Subtotal | | 2,500 | | | 1.04 | 36.2 | 1.39 | 48.3 | 0.16 | 5.6 | | | | | | |
| | | | | | | | | | | | | | | | | |
| HUBDEH | Dehydration Unit ⁽⁵⁾ | | 257,000 | 4,125,020 | 0.13 | 4.4 | 0.11 | 3.7 | 0.00 | 0.0 | 3.0 | 533 | 6.4 | 0.15 | 2.0 | 2.0 |
| HUBSEP | Separator ⁽⁵⁾ | | 257,000 | 4,125,030 | 0.09 | 3.1 | 0.08 | 2.6 | 0.00 | 0.0 | 3.0 | 533 | 6.4 | 0.15 | 2.0 | 2.0 |
| Facility Total | | | | | 1.26 | 43.7 | 1.57 | 54.6 | 0.16 | 5.6 | | | | | | |

⁽¹⁾ Assumed unit capacity is based on typical installations

⁽²⁾ Assumed NOx emission rate – 1.50 g/hp-hr

⁽³⁾ Assumed CO emission rate – 2.00 g/hp-hr

⁽⁴⁾ Assumed HAP emission rate – 0.23 g/hp-hr

⁽⁵⁾ Dehydration/separator emissions based on 10 MMBtu/hr heater at each compressor site

Table A-15. Potential Central Compressor Emissions and Modeling Assumptions (Elmridge 1)

| Location | Elevation (ft) | Latitude | Longitude | Jurisdiction |
|-------------------|----------------|-------------|---------------|--------------|
| T33NU, R5W, Sec 2 | 6,399 | 37° 08' 18" | -107° 23' 00" | Private |

| Unit ID | Source Type | Size ⁽¹⁾ (hp) | UTM | | NOx ⁽²⁾ | | CO ⁽³⁾ | | HAP ⁽⁴⁾ | | Stack Parameters | | | | Building Size | |
|-----------------------------------|---------------------------------|-----------------------------|----------------|-----------------|--------------------|-------------|-------------------|--------------|--------------------|-------------|------------------|--------------|-------------------|-----------------|---------------|--------------|
| | | | Easting (m) | Northing (m) | (g/s) | (t/yr) | (g/s) | (t/yr) | (g/s) | (t/yr) | Height (m) | Temp (°K) | Velocity (m/s) | Diameter (m) | Height (m) | Width (m) |
| ELM1A | Natural Gas Engine | 1,250 | 288,301 | 4,112,688 | 0.52 | 18.1 | 0.69 | 24.1 | 0.08 | 2.8 | 6.6 | 644 | 17.3 | 0.46 | 3.9 | 3.9 |
| ELM1B | Natural Gas Engine | 1,250 | 288,301 | 4,112,698 | 0.52 | 18.1 | 0.69 | 24.1 | 0.08 | 2.8 | 6.6 | 644 | 17.3 | 0.46 | 3.9 | 3.9 |
| ELM1C | Natural Gas Engine | 1,250 | 288,301 | 4,112,708 | 0.52 | 18.1 | 0.69 | 24.1 | 0.08 | 2.8 | 6.6 | 644 | 17.3 | 0.46 | 3.9 | 3.9 |
| ELM1D | Natural Gas Engine | 1,250 | 288,301 | 4,112,718 | 0.52 | 18.1 | 0.69 | 24.1 | 0.08 | 2.8 | 6.6 | 644 | 17.3 | 0.46 | 3.9 | 3.9 |
| Compressor Engine Subtotal | | 5,000 | | | 2.08 | 72.4 | 2.78 | 96.6 | 0.32 | 11.1 | | | | | | |
| | | | | | | | | | | | | | | | | |
| ELM1DEHY | Dehydration Unit ⁽⁵⁾ | | 288,301 | 4,112,728 | 0.126 | 4.4 | 0.11 | 3.7 | 0.00 | 0.0 | 3.5 | 533 | 6.4 | 0.15 | 2.3 | 2.3 |
| ELM1SEP | Separator ⁽⁵⁾ | | 288,301 | 4,112,738 | 0.09 | 6.2 | 0.15 | 5.2 | 0.00 | 0.0 | 3.5 | 533 | 6.4 | 0.15 | 2.3 | 2.3 |
| Facility Total | | | | | 2.30 | 83.0 | 3.03 | 105.5 | 0.32 | 11.1 | | | | | | |

⁽¹⁾ Assumed unit capacity is based on typical installations

⁽²⁾ Assumed NOx emission rate – 1.50 g/hp-hr

⁽³⁾ Assumed CO emission rate – 2.00 g/hp-hr

⁽⁴⁾ Assumed HAP emission rate – 0.23 g/hp-hr

⁽⁵⁾ Dehydration/separator emissions based on 10 MMBtu/hr heater at each compressor site

Table A-16. Potential Central Compressor Emissions and Modeling Assumptions (Elmridge 2)

| Location | Elevation (ft) | Latitude | Longitude | Jurisdiction |
|-------------------|----------------|-------------|---------------|--------------|
| T33NU, R5W, Sec 2 | 6,399 | 37° 08' 59" | -107° 32' 22" | Federal |

| Unit ID | Source Type | Size ⁽¹⁾ (hp) | UTM | | NOx ⁽²⁾ | | CO ⁽³⁾ | | HAP ⁽⁴⁾ | | Stack Parameters | | | | Building Size | |
|-----------------------------------|---------------------------------|-----------------------------|----------------|-----------------|--------------------|--------------|-------------------|--------------|--------------------|-------------|------------------|--------------|-------------------|-----------------|---------------|--------------|
| | | | Easting (m) | Northing (m) | (g/s) | (t/yr) | (g/s) | (t/yr) | (g/s) | (t/yr) | Height (m) | Temp (°K) | Velocity (m/s) | Diameter (m) | Height (m) | Width (m) |
| ELM2A | Natural Gas Engine | 1,500 | 274,470 | 4,114,300 | 0.63 | 21.7 | 0.83 | 29.0 | 0.10 | 3.3 | 9.5 | 644 | 29.2 | 0.38 | 5.9 | 5.9 |
| ELM2B | Natural Gas Engine | 1,500 | 274,470 | 4,114,310 | 0.63 | 21.7 | 0.83 | 29.0 | 0.10 | 3.3 | 9.5 | 644 | 29.2 | 0.38 | 5.9 | 5.9 |
| ELM2C | Natural Gas Engine | 1,500 | 274,470 | 4,114,320 | 0.63 | 21.7 | 0.83 | 29.0 | 0.10 | 3.3 | 9.5 | 644 | 29.2 | 0.38 | 5.9 | 5.9 |
| ELM2D | Natural Gas Engine | 1,500 | 274,470 | 4,114,330 | 0.63 | 21.7 | 0.83 | 29.0 | 0.10 | 3.3 | 9.5 | 644 | 29.2 | 0.38 | 5.9 | 5.9 |
| ELM2E | Natural Gas Engine | 1,500 | 274,470 | 4,114,340 | 0.63 | 21.7 | 0.83 | 29.0 | 0.10 | 3.3 | 9.5 | 644 | 29.2 | 0.38 | 5.9 | 5.9 |
| ELM2F | Natural Gas Engine | 1,500 | 274,470 | 4,114,350 | 0.63 | 21.7 | 0.83 | 29.0 | 0.10 | 3.3 | 9.5 | 644 | 29.2 | 0.38 | 5.9 | 5.9 |
| ELM2G | Natural Gas Engine | 1,500 | 274,470 | 4,114,360 | 0.63 | 21.7 | 0.83 | 29.0 | 0.10 | 3.3 | 9.5 | 644 | 29.2 | 0.38 | 5.9 | 5.9 |
| ELM2H | Natural Gas Engine | 1,500 | 274,470 | 4,114,370 | 0.63 | 21.7 | 0.83 | 29.0 | 0.10 | 3.3 | 9.5 | 644 | 29.2 | 0.38 | 5.9 | 5.9 |
| ELM2I | Natural Gas Engine | 1,500 | 274,470 | 4,114,380 | 0.63 | 21.7 | 0.83 | 29.0 | 0.10 | 3.3 | 9.5 | 644 | 29.2 | 0.38 | 5.9 | 5.9 |
| Compressor Engine Subtotal | | 12,000 | | | 5.63 | 195.5 | 7.50 | 260.7 | 0.86 | 30.0 | | | | | | |
| | | | | | | | | | | | | | | | | |
| ELM2DEHY | Dehydration Unit ⁽⁵⁾ | | 274,470 | 4,114,270 | 0.126 | 4.4 | 0.11 | 3.7 | 0.00 | 0.0 | 3.5 | 533 | 6.4 | 0.15 | 2.0 | 2.0 |
| ELM2SEP | Separator ⁽⁵⁾ | | 274,470 | 4,114,280 | 0.11 | 7.5 | 0.36 | 12.5 | 0.00 | 0.0 | 3.5 | 533 | 6.4 | 0.15 | 2.0 | 2.0 |
| ELM2SEPa | Separator ⁽⁵⁾ | | 274,470 | 4,114,290 | 0.11 | 7.5 | 0.36 | 12.5 | 0.00 | 0.0 | 3.5 | 533 | 6.4 | 0.15 | 2.0 | 2.0 |
| Facility Total | | | | | 5.97 | 214.8 | 8.33 | 289.5 | 0.86 | 30.0 | | | | | | |

⁽¹⁾ Assumed unit capacity is based on typical installations

⁽²⁾ Assumed NOx emission rate – 1.50 g/hp-hr

⁽³⁾ Assumed CO emission rate – 2.00 g/hp-hr

⁽⁴⁾ Assumed HAP emission rate – 0.23 g/hp-hr

⁽⁵⁾ Dehydration/separator emissions based on 10 MMBtu/hr heater at each compressor site

Table A-17. Potential Central Compressor Emissions and Modeling Assumptions (Independent 1)

| Location | Elevation (ft) | Latitude | Longitude | Jurisdiction |
|---------------------|----------------|-------------|---------------|--------------|
| T34NU, R6W, Sec 28U | 7,514 | 37° 09' 38" | -107° 30' 36" | Federal |

| Unit ID | Source Type | Size ⁽¹⁾ (hp) | UTM | | NOx ⁽²⁾ | | CO ⁽³⁾ | | HAP ⁽⁴⁾ | | Stack Parameters | | | | Building Size | |
|-----------------------------------|---------------------------------|--------------------------|-------------|--------------|--------------------|-------------|-------------------|-------------|--------------------|------------|------------------|-----------|----------------|--------------|---------------|-----------|
| | | | Easting (m) | Northing (m) | (g/s) | (t/yr) | (g/s) | (t/yr) | (g/s) | (t/yr) | Height (m) | Temp (°K) | Velocity (m/s) | Diameter (m) | Height (m) | Width (m) |
| IP1 | Natural Gas Engine | 1,000 | 277,120 | 4,115,417 | 0.42 | 14.5 | 0.56 | 19.3 | 0.06 | 2.2 | 3.1 | 644 | 24.8 | 0.30 | 2.0 | 2.0 |
| Compressor Engine Subtotal | | 1,000 | | | 0.42 | 14.5 | 0.56 | 19.3 | 0.06 | 2.2 | | | | | | |
| IP1DEH | Dehydration Unit ⁽⁵⁾ | | 277,120 | 4,115,427 | 0.13 | 4.4 | 0.11 | 3.7 | 0.00 | 0.0 | 3.0 | 533 | 6.4 | 0.15 | 2.0 | 2.0 |
| IP1SEP | Separator ⁽⁵⁾ | | 277,120 | 4,115,437 | 0.04 | 1.2 | 0.03 | 1.0 | 0.00 | 0.0 | 3.0 | 533 | 6.4 | 0.15 | 2.0 | 2.0 |
| Facility Total | | | | | 0.58 | 20.1 | 0.69 | 24.0 | 0.06 | 2.2 | | | | | | |

⁽¹⁾ Assumed unit capacity is based on typical installations

⁽²⁾ Assumed NOx emission rate – 1.50 g/hp-hr

⁽³⁾ Assumed CO emission rate – 2.00 g/hp-hr

⁽⁴⁾ Assumed HAP emission rate – 0.23 g/hp-hr

⁽⁵⁾ Dehydration/separator emissions based on 10 MMBtu/hr heater at each compressor site

Table A-18. Potential Central Compressor Emissions and Modeling Assumptions (Independent 2)

| Location | Elevation (ft) | Latitude | Longitude | Jurisdiction |
|--------------------|----------------|-------------|---------------|--------------|
| T34NU, R6W, Sec 8U | 7,196 | 37° 12' 31" | -107° 31' 43" | Federal |

| Unit ID | Source Type | Size ⁽¹⁾ (hp) | UTM | | NOx ⁽²⁾ | | CO ⁽³⁾ | | HAP ⁽⁴⁾ | | Stack Parameters | | | | Building Size | |
|-----------------------------------|---------------------------------|--------------------------|-------------|--------------|--------------------|-------------|-------------------|-------------|--------------------|------------|------------------|-----------|----------------|--------------|---------------|-----------|
| | | | Easting (m) | Northing (m) | (g/s) | (t/yr) | (g/s) | (t/yr) | (g/s) | (t/yr) | Height (m) | Temp (°K) | Velocity (m/s) | Diameter (m) | Height (m) | Width (m) |
| IP2A | Natural Gas Engine | 2,000 | 275,600 | 4,120,800 | 0.83 | 29.0 | 1.11 | 38.6 | 0.13 | 4.4 | 7.5 | 644 | 25.3 | 0.46 | 4.9 | 4.9 |
| Compressor Engine Subtotal | | 2,000 | | | 0.83 | 29.0 | 1.11 | 38.6 | 0.13 | 4.4 | | | | | | |
| IP2DEH | Dehydration Unit ⁽⁵⁾ | | 275,600 | 4,120,810 | 0.13 | 4.4 | 0.11 | 3.7 | 0.00 | 0.0 | 3.0 | 533 | 6.4 | 0.15 | 2.0 | 2.0 |
| IP2SEP | Separator ⁽⁵⁾ | | 275,600 | 4,120,820 | 0.07 | 2.5 | 0.06 | 2.1 | 0.00 | 0.0 | 3.0 | 533 | 6.4 | 0.15 | 2.0 | 2.0 |
| Facility Total | | | | | 1.03 | 35.8 | 1.28 | 44.4 | 0.13 | 4.4 | | | | | | |

⁽¹⁾ Assumed unit capacity is based on typical installations

⁽²⁾ Assumed NOx emission rate – 1.50 g/hp-hr

⁽³⁾ Assumed CO emission rate – 2.00 g/hp-hr

⁽⁴⁾ Assumed HAP emission rate – 0.23 g/hp-hr

⁽⁵⁾ Dehydration/separator emissions based on 10 MMBtu/hr heater at each compressor site

Table A-19. Potential Central Compressor Emissions and Modeling Assumptions (Independent 3)

| Location | Elevation (ft) | Latitude | Longitude | Jurisdiction |
|--------------------|----------------|-------------|---------------|--------------|
| T34NU R6W, Sec 20U | 7,426 | 37° 10' 21" | -107° 31' 05" | Federal |

| Unit ID | Source Type | Size ⁽¹⁾ (hp) | UTM | | NOx ⁽²⁾ | | CO ⁽³⁾ | | HAP ⁽⁴⁾ | | Stack Parameters | | | | Building Size | |
|-----------------------------------|---------------------------------|--------------------------|-------------|--------------|--------------------|-------------|-------------------|-------------|--------------------|------------|------------------|-----------|----------------|--------------|---------------|-----------|
| | | | Easting (m) | Northing (m) | (g/s) | (t/yr) | (g/s) | (t/yr) | (g/s) | (t/yr) | Height (m) | Temp (°K) | Velocity (m/s) | Diameter (m) | Height (m) | Width (m) |
| IP3A | Natural Gas Engine | 2,000 | 276,435 | 4,116,788 | 0.83 | 29.0 | 1.11 | 38.6 | 0.13 | 4.4 | 7.5 | 644 | 25.3 | 0.46 | 4.9 | 4.9 |
| Compressor Engine Subtotal | | 2,000 | | | 0.83 | 29.0 | 1.11 | 38.6 | 0.13 | 4.4 | | | | | | |
| IP3DEH | Dehydration Unit ⁽⁵⁾ | | 276,435 | 4,116,798 | 0.13 | 4.4 | 0.11 | 3.7 | 0.00 | 0.0 | 3.0 | 533 | 6.4 | 0.15 | 2.0 | 2.0 |
| IP3SEP | Separator ⁽⁵⁾ | | 276,435 | 4,116,778 | 0.07 | 2.5 | 0.06 | 2.1 | 0.00 | 0.0 | 3.0 | 533 | 6.4 | 0.15 | 2.0 | 2.0 |
| Facility Total | | | | | 1.03 | 35.8 | 1.28 | 44.4 | 0.13 | 4.4 | | | | | | |

⁽¹⁾ Assumed unit capacity is based on typical installations

⁽²⁾ Assumed NOx emission rate – 1.50 g/hp-hr

⁽³⁾ Assumed CO emission rate – 2.00 g/hp-hr

⁽⁴⁾ Assumed HAP emission rate – 0.23 g/hp-hr

⁽⁵⁾ Dehydration/separator emissions based on 10 MMBtu/hr heater at each compressor site

Table A-20. Potential Central Compressor Emissions and Modeling Assumptions (Petrox 1)

| Location | Elevation (ft) | Latitude | Longitude | Jurisdiction |
|---------------------|----------------|-------------|---------------|--------------|
| T34NU, R5W, Sec 36U | 6,396 | 37° 09' 01" | -107° 20' 15" | Federal |

| Unit ID | Source Type | Size ⁽¹⁾ (hp) | UTM | | NOx ⁽²⁾ | | CO ⁽³⁾ | | HAP ⁽⁴⁾ | | Stack Parameters | | | | Building Size | |
|-----------------------------------|---------------------------------|--------------------------|-------------|--------------|--------------------|-------------|-------------------|-------------|--------------------|------------|------------------|-----------|----------------|--------------|---------------|-----------|
| | | | Easting (m) | Northing (m) | (g/s) | (t/yr) | (g/s) | (t/yr) | (g/s) | (t/yr) | Height (m) | Temp (°K) | Velocity (m/s) | Diameter (m) | Height (m) | Width (m) |
| PET1 | Natural Gas Engine | 620 | 292,405 | 4,113,912 | 0.26 | 9.0 | 0.34 | 12.0 | 0.04 | 1.4 | 3.1 | 644 | 24.1 | 0.30 | 2.0 | 2.0 |
| Compressor Engine Subtotal | | 620 | | | 0.26 | 9.0 | 0.34 | 12.0 | 0.04 | 1.4 | | | | | | |
| PET1DEH | Dehydration Unit ⁽⁵⁾ | | 292,405 | 4,113,922 | 0.13 | 4.4 | 0.11 | 3.7 | 0.00 | 0.0 | 3.0 | 533 | 6.4 | 0.15 | 2.0 | 2.0 |
| PET1SEP | Separator ⁽⁵⁾ | | 292,405 | 4,113,932 | 0.02 | 0.8 | 0.02 | 0.6 | 0.00 | 0.0 | 3.0 | 533 | 6.4 | 0.15 | 2.0 | 2.0 |
| Facility Total | | | | | 0.41 | 14.1 | 0.47 | 16.3 | 0.04 | 1.4 | | | | | | |

⁽¹⁾ Assumed unit capacity is based on typical installations

⁽²⁾ Assumed NOx emission rate – 1.50 g/hp-hr

⁽³⁾ Assumed CO emission rate – 2.00 g/hp-hr

⁽⁴⁾ Assumed HAP emission rate – 0.23 g/hp-hr

⁽⁵⁾ Dehydration/separator emissions based on 10 MMBtu/hr heater at each compressor site

Table A-21. Potential Central Compressor Emissions and Modeling Assumptions (Petrox 2)

| Location | Elevation (ft) | Latitude | Longitude | Jurisdiction |
|--------------------|----------------|-------------|---------------|--------------|
| T34NU, R5W, Sec 9U | 7,613 | 37° 12' 29" | -107° 24' 35" | Federal |

| Unit ID | Source Type | Size ⁽¹⁾ (hp) | UTM | | NOx ⁽²⁾ | | CO ⁽³⁾ | | HAP ⁽⁴⁾ | | Stack Parameters | | | | Building Size | |
|-----------------------------------|---------------------------------|--------------------------|------------|-------------|--------------------|-------------|-------------------|-------------|--------------------|------------|------------------|-----------|----------------|--------------|---------------|-----------|
| | | | Eastng (m) | Northng (m) | (g/s) | (t/yr) | (g/s) | (t/yr) | (g/s) | (t/yr) | Height (m) | Temp (°K) | Velocity (m/s) | Diameter (m) | Height (m) | Width (m) |
| PET2 | Natural Gas Engine | 1,900 | 286,151 | 4,120,460 | 0.79 | 27.5 | 1.06 | 36.7 | 0.12 | 4.2 | 9.1 | 644 | 26.3 | 0.46 | 4.9 | 4.9 |
| Compressor Engine Subtotal | | 1,900 | | | 0.79 | 27.5 | 1.06 | 36.7 | 0.12 | 4.2 | | | | | | |
| PET2DEH | Dehydration Unit ⁽⁵⁾ | | 286,151 | 4,120,470 | 0.13 | 4.4 | 0.11 | 3.7 | 0.00 | 0.0 | 3.1 | 533 | 6.4 | 0.15 | 2.0 | 2.0 |
| PET2SEP | Separator ⁽⁵⁾ | | 286,151 | 4,120,480 | 0.03 | 1.2 | 0.06 | 2.0 | 0.00 | 0.0 | 3.1 | 533 | 6.4 | 0.15 | 2.0 | 2.0 |
| PET2SEPa | Separator ⁽⁵⁾ | | 286,151 | 4,120,450 | 0.03 | 1.2 | 0.06 | 2.0 | 0.00 | 0.0 | 3.1 | 533 | 6.4 | 0.15 | 2.0 | 2.0 |
| Facility Total | | | | | 0.99 | 34.3 | 1.28 | 44.3 | 0.12 | 4.2 | | | | | | |

⁽¹⁾ Assumed unit capacity is based on typical installations

⁽²⁾ Assumed NOx emission rate – 1.50 g/hp-hr

⁽³⁾ Assumed CO emission rate – 2.00 g/hp-hr

⁽⁴⁾ Assumed HAP emission rate – 0.23 g/hp-hr

⁽⁵⁾ Dehydration/separator emissions based on 10 MMBtu/hr heater at each compressor site

Table A-22. Potential Central Compressor Emissions and Modeling Assumptions (Petrox 3)

| Location | Elevation (ft) | Latitude | Longitude | Jurisdiction |
|------------------|----------------|-------------|---------------|--------------|
| T34N, R5W, Sec 8 | 7,616 | 37° 13' 54" | -107° 26' 42" | |

| Unit ID | Source Type | Size ⁽¹⁾ (hp) | UTM | | NOx ⁽²⁾ | | CO ⁽³⁾ | | HAP ⁽⁴⁾ | | Stack Parameters | | | | Building Size | |
|-----------------------------------|---------------------------------|--------------------------|------------|-------------|--------------------|-------------|-------------------|-------------|--------------------|------------|------------------|-----------|----------------|--------------|---------------|-----------|
| | | | Eastng (m) | Northng (m) | (g/s) | (t/yr) | (g/s) | (t/yr) | (g/s) | (t/yr) | Height (m) | Temp (°K) | Velocity (m/s) | Diameter (m) | Height (m) | Width (m) |
| PET3 | Natural Gas Engine | 620 | 283,100 | 4,123,180 | 0.26 | 9.0 | 0.34 | 12.0 | 0.04 | 1.4 | 3.1 | 644 | 24.1 | 0.30 | 2.0 | 2.0 |
| Compressor Engine Subtotal | | 620 | | | 0.26 | 9.0 | 0.34 | 12.0 | 0.04 | 1.4 | | | | | | |
| PET3DEH | Dehydration Unit ⁽⁵⁾ | | 283,100 | 4,123,190 | 0.13 | 4.4 | 0.11 | 3.7 | 0.00 | 0.0 | 3.0 | 533 | 6.4 | 0.15 | 2.0 | 2.0 |
| PET3SEP | Separator ⁽⁵⁾ | | 283,100 | 4,123,200 | 0.02 | 0.8 | 0.02 | 0.6 | 0.00 | 0.0 | 3.0 | 533 | 6.4 | 0.15 | 2.0 | 2.0 |
| Facility Total | | | | | 0.41 | 14.1 | 0.47 | 16.3 | 0.04 | 1.4 | | | | | | |

⁽¹⁾ Assumed unit capacity is based on typical installations

⁽²⁾ Assumed NOx emission rate – 1.50 g/hp-hr

⁽³⁾ Assumed CO emission rate – 2.00 g/hp-hr

⁽⁴⁾ Assumed HAP emission rate – 0.23 g/hp-hr

⁽⁵⁾ Dehydration/separator emissions based on 10 MMBtu/hr heater at each compressor site

Table A-23. Potential Central Compressor Emissions and Modeling Assumptions (Petrox 4)

| Location | Elevation (ft) | Latitude | Longitude | Jurisdiction |
|------------------|----------------|-------------|---------------|--------------|
| T34N, R5W, Sec 7 | 8,197 | 37° 13' 52" | -107° 27' 47" | |

| Unit ID | Source Type | Size ⁽¹⁾ (hp) | UTM | | NOx ⁽²⁾ | | CO ⁽³⁾ | | HAP ⁽⁴⁾ | | Stack Parameters | | | | Building Size | |
|-----------------------------------|---------------------------------|--------------------------|------------|-------------|--------------------|-------------|-------------------|-------------|--------------------|------------|------------------|-----------|----------------|--------------|---------------|-----------|
| | | | Eastng (m) | Northng (m) | (g/s) | (t/yr) | (g/s) | (t/yr) | (g/s) | (t/yr) | Height (m) | Temp (°K) | Velocity (m/s) | Diameter (m) | Height (m) | Width (m) |
| PET4 | Natural Gas Engine | 620 | 281,500 | 4,123,161 | 0.26 | 9.0 | 0.34 | 12.0 | 0.04 | 1.4 | 3.1 | 644 | 24.1 | 0.30 | 2.0 | 2.0 |
| | | | | | | | | | | | | | | | | |
| Compressor Engine Subtotal | | 620 | | | 0.26 | 9.0 | 0.34 | 12.0 | 0.04 | 1.4 | | | | | | |
| PET4DEH | Dehydration Unit ⁽⁵⁾ | | 281,500 | 4,123,171 | 0.13 | 4.4 | 0.11 | 3.7 | 0.00 | 0.0 | 3.0 | 533 | 6.4 | 0.15 | 2.0 | 2.0 |
| PET4SEP | Separator ⁽⁵⁾ | | 281,500 | 4,123,181 | 0.02 | 0.8 | 0.02 | 0.6 | 0.00 | 0.0 | 3.0 | 533 | 6.4 | 0.15 | 2.0 | 2.0 |
| Facility Total | | | | | 0.41 | 14.1 | 0.47 | 16.3 | 0.04 | 1.4 | | | | | | |

⁽¹⁾ Assumed unit capacity is based on typical installations

⁽²⁾ Assumed NOx emission rate – 1.50 g/hp-hr

⁽³⁾ Assumed CO emission rate – 2.00 g/hp-hr

⁽⁴⁾ Assumed HAP emission rate – 0.23 g/hp-hr

⁽⁵⁾ Dehydration/separator emissions based on 10 MMBtu/hr heater at each compressor site

Table A-24. Potential Central Compressor Emissions and Modeling Assumptions (Pure 1)

| Location | Elevation (ft) | Latitude | Longitude | Jurisdiction |
|---------------------|----------------|-------------|---------------|--------------|
| T34.5N, R9W, Sec 36 | 7,036 | 37° 14' 52" | -107° 48' 02" | State |

| Unit ID | Source Type | Size ⁽¹⁾ (hp) | UTM | | NOx ⁽²⁾ | | CO ⁽³⁾ | | HAP ⁽⁴⁾ | | Stack Parameters | | | | Building Size | |
|-----------------------------------|---------------------------------|--------------------------|------------|-------------|--------------------|-------------|-------------------|-------------|--------------------|------------|------------------|-----------|----------------|--------------|---------------|-----------|
| | | | Eastng (m) | Northng (m) | (g/s) | (t/yr) | (g/s) | (t/yr) | (g/s) | (t/yr) | Height (m) | Temp (°K) | Velocity (m/s) | Diameter (m) | Height (m) | Width (m) |
| PUR1 | Natural Gas Engine | 1,500 | 251,600 | 4,125,830 | 0.63 | 21.7 | 0.83 | 29.0 | 0.10 | 3.3 | 4.6 | 644 | 29.9 | 0.38 | 3.0 | 3.0 |
| Compressor Engine Subtotal | | 1,500 | | | 0.63 | 21.7 | 0.83 | 29.0 | 0.10 | 3.3 | | | | | | |
| PUR1DEH | Dehydration Unit ⁽⁵⁾ | | 251,600 | 4,125,840 | 0.13 | 4.4 | 0.11 | 3.7 | 0.00 | 0.0 | 3.0 | 533 | 6.4 | 0.15 | 2.0 | 2.0 |
| PUR1SEP | Separator ⁽⁵⁾ | | 251,600 | 4,125,850 | 0.05 | 1.9 | 0.05 | 1.6 | 0.00 | 0.0 | 3.0 | 533 | 6.4 | 0.15 | 2.0 | 2.0 |
| Facility Total | | | | | 0.80 | 28.0 | 0.98 | 34.2 | 0.10 | 3.3 | | | | | | |

⁽¹⁾ Assumed unit capacity is based on typical installations

⁽²⁾ Assumed NOx emission rate – 1.50 g/hp-hr

⁽³⁾ Assumed CO emission rate – 2.00 g/hp-hr

⁽⁴⁾ Assumed HAP emission rate – 0.23 g/hp-hr

⁽⁵⁾ Dehydration/separator emissions based on 10 MMBtu/hr heater at each compressor site

Table A-25. Potential Central Compressor Emissions and Modeling Assumptions (Pure 2)

| Location | Elevation (ft) | Latitude | Longitude | Jurisdiction |
|------------------|----------------|-------------|---------------|--------------|
| T34N, R9W, Sec 2 | 6,803 | 37° 14' 28" | -107° 49' 32" | Private |

| Unit ID | Source Type | Size ⁽¹⁾ (hp) | UTM | | NOx ⁽²⁾ | | CO ⁽³⁾ | | HAP ⁽⁴⁾ | | Stack Parameters | | | | Building Size | |
|-----------------------------------|---------------------------------|-----------------------------|----------------|-----------------|--------------------|------------|-------------------|------------|--------------------|------------|------------------|--------------|-------------------|-----------------|---------------|--------------|
| | | | Easting (m) | Northing (m) | (g/s) | (t/yr) | (g/s) | (t/yr) | (g/s) | (t/yr) | Height (m) | Temp (°K) | Velocity (m/s) | Diameter (m) | Height (m) | Width (m) |
| PUR2 | Natural Gas Engine | 240 | 249,350 | 4,125,160 | 0.10 | 3.5 | 0.13 | 4.6 | 0.02 | 0.5 | 3.0 | 583 | 21.5 | 0.18 | 2.0 | 2.0 |
| Compressor Engine Subtotal | | 240 | | | 0.10 | 3.5 | 0.13 | 4.6 | 0.02 | 0.5 | | | | | | |
| PUR2DEH | Dehydration Unit ⁽⁵⁾ | | 249,350 | 4,125,170 | 0.13 | 4.4 | 0.11 | 3.7 | 0.00 | 0.0 | 3.0 | 533 | 6.4 | 0.18 | 2.0 | 2.0 |
| PUR2SEP | Separator ⁽⁵⁾ | | 249,350 | 4,125,180 | 0.01 | 0.3 | 0.01 | 0.3 | 0.00 | 0.0 | 3.0 | 533 | 6.4 | 0.15 | 2.0 | 2.0 |
| Facility Total | | | | | 0.23 | 8.2 | 0.25 | 8.6 | 0.02 | 0.5 | | | | | | |

⁽¹⁾ Assumed unit capacity is based on typical installations

⁽²⁾ Assumed NOx emission rate – 1.50 g/hp-hr

⁽³⁾ Assumed CO emission rate – 2.00 g/hp-hr

⁽⁴⁾ Assumed HAP emission rate – 0.23 g/hp-hr

⁽⁵⁾ Dehydration/separator emissions based on 10 MMBtu/hr heater at each compressor site

Table A-26 Separator Emission Calculations

| Single Well Emission Rate | NOx | CO | HAP |
|----------------------------------|------------|-----------|------------|
| lb/MMscf ⁽¹⁾ | 100 | 84 | 11.3 |
| lb/hr ⁽²⁾ | 0.025 | 0.021 | 0.002825 |
| t/yr ⁽²⁾ | 0.11 | 0.09 | 0.01 |

⁽¹⁾ EPA (AP-42 Section 1.4 emission factors)⁽²⁾ Based on average natural gas heat capacity of 1,000 BTU/scf, and individual separator flame rate of 0.25 MMBtu/hr

| Alternative | Number of wells | NOx (t/yr) | CO (t/yr) | HAP (t/yr) |
|------------------------------|------------------------|-------------------|------------------|-------------------|
| 1 (Proposed Action) | 296 | 32.4 | 27.2 | 3.66 |
| 2 (Maximum Development) | 522 | 57.2 | 48.0 | 6.46 |
| 3 (No Wells in HD Mountains) | 212 | 23.2 | 19.5 | 2.62 |
| 4 (Current Management) | 188 | 20.6 | 17.3 | 2.33 |
| 5 (No Action) | 118 | 12.9 | 10.9 | 1.46 |

Note: Assumes separators operate year-around (8760 hr/yr)

Table A-27 Dehydrator Emission Calculations

| Single Well Emission Rate | NOx | CO | HAP |
|----------------------------------|------------|-----------|------------|
| lb/MMscf ⁽¹⁾ | 100 | 84 | 11.3 |
| lb/hr ⁽²⁾ | 1 | 0.84 | 0.11 |
| t/yr ⁽²⁾ | 4.38 | 3.68 | 0.49 |

Note: Assumes separators operate year-around (8760 hr/yr)

⁽¹⁾ EPA (AP-42 Section 1.4 emission factors)⁽²⁾ Based on average natural gas heat capacity of 1,000 BTU/scf, and individual dehydrator flame rate of 10.0 MMBtu/hr

Table A-28 Small Wellhead Engine Emission Calculations

| Operator / Area | Wells with Wellhead Engines (percent) |
|-----------------|------------------------------------------|
| BP Amoco | 50 |
| Huber | 100 |
| Pure | 50 |
| Eastern Portion | 50 |

| Single Well Emission Rate ⁽¹⁾ | NOx | CO | HAP |
|---------------------------------------------|---------|-------|-------------|
| lb/hp-hr | 0.00441 | 0.019 | 0.000290749 |
| lb/hr | 0.2 | 0.9 | 0.01 |
| t/yr | 0.9 | 4.0 | 0.1 |

⁽¹⁾ Assumes a 48 hp 4 stroke rich burn wellhead engine

| Alternative | Total wells | Huber wells | Non-Huber wells | Wellhead engines |
|------------------------------|-------------|-------------|-----------------|------------------|
| 1 (Proposed Action) | 296 | 17 | 282 | 158 |
| 2 (Maximum Development) | 522 | 22 | 504 | 274 |
| 3 (No Wells in HD Mountains) | 212 | 17 | 200 | 117 |
| 4 (Current Management) | 188 | 17 | 172 | 103 |
| 5 (No Action) | 118 | 15 | 118 | 74 |

| Alternative | Wellhead engines | NOx (t/yr) | CO (t/yr) | HAP (t/yr) |
|------------------------------|------------------|------------|-----------|------------|
| 1 (Proposed Action) | 158 | 731 | 631 | 9.7 |
| 2 (Maximum Development) | 274 | 1,267 | 1,095 | 16.7 |
| 3 (No Wells in HD Mountains) | 117 | 541 | 467 | 7.2 |
| 4 (Current Management) | 103 | 476 | 411 | 6.3 |
| 5 (No Action) | 74 | 342 | 296 | 4.5 |

Table A-29. Small Wellhead Engine Emission Inventory (Alternative 1)

| Source Description | Well Count | Record Number | UTM Easting (m) | UTM Northing (m) | NOx (t/yr) | CO (t/yr) | HAP (t/yr) | Stack Height (m) | Stack Diameter (m) | Stack Velocity (m/s) | Stack Temp (°K) |
|--------------------|------------|---------------|-----------------|------------------|------------|-----------|------------|------------------|--------------------|----------------------|-----------------|
| Huber engine | 1 | 5 | 264640 | 4126938 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 2 | 13 | 258942 | 4123212 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 3 | 207 | 263842 | 4126960 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 4 | 230 | 262712 | 4124660 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 5 | 237 | 261268 | 4123811 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 6 | 249 | 262668 | 4123106 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 7 | 1 | 263008 | 4131981 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 8 | 2 | 259133 | 4129870 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 9 | 176 | 260793 | 4132044 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 10 | 177 | 261302 | 4131252 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 11 | 179 | 258263 | 4130450 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 12 | 185 | 257531 | 4129694 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 13 | 187 | 260723 | 4129603 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 14 | 192 | 253338 | 4128927 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 15 | 193 | 254934 | 4128881 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 16 | 196 | 254120 | 4128349 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 17 | 204 | 254268 | 4127345 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 1 | 3 | 282897 | 4126002 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 2 | 6 | 283641 | 4120431 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 3 | 8 | 285894 | 4121706 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 4 | 10 | 277316 | 4126370 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 5 | 12 | 292360 | 4113882 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 6 | 15 | 261315 | 4125476 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 7 | 17 | 282848 | 4120673 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 8 | 19 | 280281 | 4120962 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 9 | 21 | 280546 | 4117513 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 10 | 23 | 280340 | 4119850 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 11 | 25 | 283587 | 4118322 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 12 | 27 | 280658 | 4118398 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 13 | 29 | 282768 | 4117566 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 14 | 31 | 282573 | 4113463 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 15 | 33 | 282831 | 4116566 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 16 | 35 | 283702 | 4115877 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 17 | 37 | 285237 | 4116837 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 18 | 39 | 282722 | 4115791 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 19 | 41 | 285108 | 4115285 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 20 | 43 | 285941 | 4116597 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 21 | 45 | 276507 | 4115953 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 22 | 47 | 274816 | 4115887 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 23 | 49 | 258263 | 4130450 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 24 | 51 | 288535 | 4117309 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 25 | 53 | 286852 | 4117462 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 26 | 55 | 288428 | 4120088 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 27 | 57 | 287640 | 4120551 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 28 | 59 | 287431 | 4115782 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 29 | 61 | 285349 | 4114280 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 30 | 63 | 286047 | 4117260 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 31 | 65 | 282805 | 4119009 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 32 | 67 | 274000 | 4115243 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 33 | 69 | 280586 | 4119067 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 34 | 71 | 267191 | 4129310 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 35 | 73 | 273532 | 4127582 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 36 | 75 | 269499 | 4129358 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 37 | 77 | 254934 | 4128881 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 38 | 79 | 269384 | 4125140 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 39 | 81 | 276639 | 4124278 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 40 | 83 | 275043 | 4127652 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 41 | 85 | 268570 | 4124608 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 42 | 87 | 271849 | 4124407 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |

Table A-29. Small Wellhead Engine Emission Inventory (Alternative 1) (continued)

| Source Description | Well Count | Record Number | UTM Easting (m) | UTM Northing (m) | NOx (t/yr) | CO (t/yr) | HAP (t/yr) | Stack Height (m) | Stack Diameter (m) | Stack Velocity (m/s) | Stack Temp (°K) |
|--------------------|------------|---------------|-----------------|------------------|------------|-----------|------------|------------------|--------------------|----------------------|-----------------|
| wellhead engine | 43 | 89 | 274977 | 4121880 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 44 | 91 | 270121 | 4122899 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 45 | 93 | 275731 | 4116862 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 46 | 95 | 277106 | 4121823 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 47 | 97 | 274947 | 4120770 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 48 | 99 | 268435 | 4122945 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 49 | 101 | 248207 | 4123526 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 50 | 103 | 266885 | 4124654 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 51 | 105 | 263647 | 4123190 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 52 | 107 | 270186 | 4122009 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 53 | 109 | 289013 | 4115076 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 54 | 111 | 274215 | 4126564 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 55 | 113 | 259681 | 4130410 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 56 | 115 | 281938 | 4119808 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 57 | 117 | 276397 | 4115179 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 58 | 119 | 280969 | 4116725 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 59 | 121 | 255890 | 4128187 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 60 | 123 | 263707 | 4125297 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 61 | 125 | 262712 | 4124660 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 62 | 127 | 252554 | 4123397 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 63 | 129 | 273489 | 4122696 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 64 | 131 | 274843 | 4120217 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 65 | 133 | 264329 | 4122171 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 66 | 135 | 249334 | 4122604 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 67 | 137 | 271870 | 4125184 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 68 | 139 | 257985 | 4123905 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 69 | 141 | 271806 | 4126074 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 70 | 143 | 267833 | 4126849 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 71 | 145 | 262158 | 4123898 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 72 | 147 | 286812 | 4115908 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 73 | 149 | 284366 | 4114083 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 74 | 151 | 281992 | 4115032 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 75 | 153 | 286782 | 4118241 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 76 | 155 | 284120 | 4118309 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 77 | 157 | 282132 | 4120470 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 78 | 159 | 288280 | 4114206 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 79 | 161 | 285790 | 4114158 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 80 | 163 | 282619 | 4115238 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 81 | 165 | 264731 | 4130156 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 82 | 167 | 273402 | 4126031 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 83 | 169 | 273955 | 4113578 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 84 | 171 | 281694 | 4117261 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 85 | 173 | 260723 | 4129603 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 86 | 175 | 271851 | 4127738 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 87 | 180 | 289976 | 4118050 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 88 | 182 | 272626 | 4123608 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 89 | 184 | 281321 | 4123378 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 90 | 188 | 279846 | 4128080 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 91 | 190 | 281249 | 4124046 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 92 | 194 | 285007 | 4121729 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 93 | 197 | 296270 | 4113898 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 94 | 199 | 283718 | 4123427 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 95 | 201 | 285948 | 4120372 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 96 | 203 | 288433 | 4120309 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 97 | 206 | 281439 | 4127927 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 98 | 209 | 282966 | 4121781 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 99 | 211 | 289873 | 4113944 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 100 | 212 | 283386 | 4124324 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 101 | 214 | 285422 | 4120608 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |

Table A-29. Small Wellhead Engine Emission Inventory (Alternative 1) (continued)

| Source Description | Well Count | Record Number | UTM Easting (m) | UTM Northing (m) | NOx (t/yr) | CO (t/yr) | HAP (t/yr) | Stack Height (m) | Stack Diameter (m) | Stack Velocity (m/s) | Stack Temp (°K) |
|--------------------|------------|---------------|-----------------|------------------|------------|-----------|------------|------------------|--------------------|----------------------|-----------------|
| wellhead engine | 43 | 89 | 274977 | 4121880 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 44 | 91 | 270121 | 4122899 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 45 | 93 | 275731 | 4116862 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 46 | 95 | 277106 | 4121823 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 47 | 97 | 274947 | 4120770 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 48 | 99 | 268435 | 4122945 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 49 | 101 | 248207 | 4123526 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 50 | 103 | 266885 | 4124654 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 51 | 105 | 263647 | 4123190 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 52 | 107 | 270186 | 4122009 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 53 | 109 | 289013 | 4115076 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 54 | 111 | 274215 | 4126564 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 55 | 113 | 259681 | 4130410 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 56 | 115 | 281938 | 4119808 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 57 | 117 | 276397 | 4115179 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 58 | 119 | 280969 | 4116725 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 59 | 121 | 255890 | 4128187 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 60 | 123 | 263707 | 4125297 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 61 | 125 | 262712 | 4124660 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 62 | 127 | 252554 | 4123397 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 63 | 129 | 273489 | 4122696 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 64 | 131 | 274843 | 4120217 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 65 | 133 | 264329 | 4122171 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 66 | 135 | 249334 | 4122604 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 67 | 137 | 271870 | 4125184 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 68 | 139 | 257985 | 4123905 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 69 | 141 | 271806 | 4126074 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 70 | 143 | 267833 | 4126849 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 71 | 145 | 262158 | 4123898 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 72 | 147 | 286812 | 4115908 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 73 | 149 | 284366 | 4114083 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 74 | 151 | 281992 | 4115032 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 75 | 153 | 286782 | 4118241 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 76 | 155 | 284120 | 4118309 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 77 | 157 | 282132 | 4120470 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 78 | 159 | 288280 | 4114206 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 79 | 161 | 285790 | 4114158 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 80 | 163 | 282619 | 4115238 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 81 | 165 | 264731 | 4130156 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 82 | 167 | 273402 | 4126031 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 83 | 169 | 273955 | 4113578 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 84 | 171 | 281694 | 4117261 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 85 | 173 | 260723 | 4129603 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 86 | 175 | 271851 | 4127738 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 87 | 180 | 289976 | 4118050 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 88 | 182 | 272626 | 4123608 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 89 | 184 | 281321 | 4123378 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 90 | 188 | 279846 | 4128080 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 91 | 190 | 281249 | 4124046 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 92 | 194 | 285007 | 4121729 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 93 | 197 | 296270 | 4113898 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 94 | 199 | 283718 | 4123427 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 95 | 201 | 285948 | 4120372 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 96 | 203 | 288433 | 4120309 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 97 | 206 | 281439 | 4127927 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 98 | 209 | 282966 | 4121781 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 99 | 211 | 289873 | 4113944 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 100 | 212 | 283386 | 4124324 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 101 | 214 | 285422 | 4120608 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |

Table A-29. Small Wellhead Engine Emission Inventory (Alternative 1) (continued)

| Source Description | Well Count | Record Number | UTM Easting (m) | UTM Northing (m) | NOx (t/yr) | CO (t/yr) | HAP (t/yr) | Stack Height (m) | Stack Diameter (m) | Stack Velocity (m/s) | Stack Temp (°K) |
|------------------------|------------|---------------|-----------------|------------------|------------|------------|-------------|------------------|--------------------|----------------------|-----------------|
| wellhead engine | 102 | 216 | 288435 | 4116867 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 103 | 218 | 295549 | 4113471 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 104 | 220 | 273443 | 4124253 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 105 | 222 | 283412 | 4121880 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 106 | 224 | 290652 | 4116701 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 107 | 226 | 264640 | 4126938 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 108 | 228 | 282056 | 4124358 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 109 | 231 | 277363 | 4128146 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 110 | 233 | 287211 | 4114122 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 111 | 235 | 260454 | 4123279 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 112 | 238 | 296251 | 4113122 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 113 | 240 | 263008 | 4131981 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 114 | 241 | 281705 | 4114262 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 115 | 243 | 260634 | 4126495 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 116 | 245 | 259497 | 4123973 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 117 | 247 | 281627 | 4124924 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 118 | 250 | 282909 | 4123004 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 119 | 252 | 284534 | 4120630 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 120 | 254 | 263091 | 4128647 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 121 | 256 | 289512 | 4117284 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 122 | 258 | 286690 | 4121575 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 123 | 260 | 282009 | 4119140 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 124 | 262 | 285362 | 4118277 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 125 | 264 | 286075 | 4118370 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 126 | 266 | 287451 | 4116559 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 127 | 268 | 283997 | 4113537 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 128 | 269 | 284423 | 4119744 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 129 | 271 | 283606 | 4122542 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 130 | 273 | 274998 | 4125988 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 131 | 275 | 268658 | 4127826 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 132 | 277 | 284323 | 4115860 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 133 | 279 | 276353 | 4116846 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 134 | 281 | 276086 | 4113522 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 135 | 283 | 277161 | 4113826 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 136 | 285 | 285418 | 4113501 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 137 | 287 | 253338 | 4128927 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 138 | 289 | 262961 | 4130317 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 139 | 291 | 262870 | 4127098 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 140 | 293 | 254268 | 4127345 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 141 | 295 | 267216 | 4130197 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Total Emissions | | | | | 727 | 632 | 15.8 | | | | |

Table A-30. Small Wellhead Engine Emission Inventory (Alternative 2)

| Source Description | Well Count | Record Number | UTM Easting (m) | UTM Northing (m) | NOx (t/yr) | CO (t/yr) | HAP (t/yr) | Stack Height (m) | Stack Diameter (m) | Stack Velocity (m/s) | Stack Temp (°K) |
|--------------------|------------|---------------|-----------------|------------------|------------|-----------|------------|------------------|--------------------|----------------------|-----------------|
| Huber engine | 1 | 1 | 263008 | 4131981 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 2 | 2 | 259133 | 4129870 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 3 | 3 | 263091 | 4128647 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 4 | 5 | 264640 | 4126938 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 5 | 6 | 271025 | 4126761 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 6 | 8 | 270212 | 4126228 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 7 | 10 | 266019 | 4125455 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 8 | 12 | 260454 | 4123279 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 9 | 13 | 258942 | 4123212 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 10 | 15 | 284474 | 4121742 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 11 | 17 | 289873 | 4113944 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 12 | 19 | 289820 | 4115389 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 13 | 21 | 290652 | 4116701 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 14 | 23 | 289953 | 4117162 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 15 | 25 | 289190 | 4118625 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 16 | 27 | 289976 | 4118050 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 17 | 29 | 292360 | 4113882 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 18 | 31 | 293869 | 4113846 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 19 | 33 | 293409 | 4113191 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 20 | 35 | 294938 | 4113931 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 21 | 37 | 295549 | 4113471 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 22 | 39 | 296251 | 4113122 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 23 | 41 | 279846 | 4128080 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 24 | 43 | 280629 | 4127505 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 25 | 45 | 281439 | 4127927 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 26 | 47 | 281384 | 4125819 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 27 | 49 | 282276 | 4126018 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 28 | 51 | 274918 | 4122991 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 29 | 53 | 274862 | 4124214 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 30 | 55 | 273443 | 4124253 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 31 | 57 | 272626 | 4123608 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 32 | 59 | 277363 | 4128146 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 33 | 61 | 276595 | 4125945 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 34 | 63 | 280560 | 4124841 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 35 | 65 | 282056 | 4124358 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 36 | 67 | 281321 | 4123378 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 37 | 69 | 282013 | 4122694 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 38 | 71 | 282946 | 4124446 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 39 | 73 | 283718 | 4123427 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 40 | 75 | 282909 | 4123004 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 41 | 77 | 282966 | 4121781 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 42 | 79 | 285118 | 4122614 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 43 | 81 | 285894 | 4121706 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 44 | 83 | 283641 | 4120431 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 45 | 85 | 285422 | 4120608 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 46 | 87 | 285845 | 4119819 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 47 | 89 | 287640 | 4120551 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 48 | 91 | 286911 | 4119793 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 49 | 93 | 288433 | 4120309 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 50 | 95 | 288383 | 4118312 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 51 | 97 | 287676 | 4118441 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 52 | 99 | 286802 | 4119018 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 53 | 101 | 286075 | 4118370 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 54 | 103 | 285382 | 4119054 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 55 | 105 | 286749 | 4116909 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 56 | 107 | 287554 | 4117111 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 57 | 109 | 288435 | 4116867 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 58 | 111 | 284120 | 4118309 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 59 | 113 | 282565 | 4120014 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |

Table A-30. Small Wellhead Engine Emission Inventory (Alternative 2) (continued)

| Source Description | Well Count | Record Number | UTM Easting (m) | UTM Northing (m) | NOx (t/yr) | CO (t/yr) | HAP (t/yr) | Stack Height (m) | Stack Diameter (m) | Stack Velocity (m/s) | Stack Temp (°K) |
|--------------------|------------|---------------|-----------------|------------------|------------|-----------|------------|------------------|--------------------|----------------------|-----------------|
| wellhead engine | 60 | 115 | 282001 | 4118808 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 61 | 117 | 281210 | 4115719 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 62 | 119 | 281705 | 4114262 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 63 | 121 | 283467 | 4113662 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 64 | 123 | 284366 | 4114083 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 65 | 125 | 285349 | 4114280 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 66 | 127 | 286576 | 4113583 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 67 | 129 | 287211 | 4114122 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 68 | 131 | 288299 | 4114983 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 69 | 133 | 287500 | 4115003 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 70 | 135 | 287431 | 4115782 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 71 | 137 | 285039 | 4116065 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 72 | 139 | 285907 | 4115265 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 73 | 141 | 284323 | 4115860 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 74 | 143 | 284011 | 4117534 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 75 | 145 | 285941 | 4116597 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 76 | 147 | 277161 | 4113826 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 77 | 149 | 276086 | 4113522 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 78 | 151 | 275488 | 4114425 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 79 | 153 | 273982 | 4114577 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 80 | 155 | 274798 | 4115221 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 81 | 157 | 274816 | 4115887 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 82 | 159 | 276507 | 4115953 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 83 | 161 | 276353 | 4116846 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 84 | 163 | 260818 | 4132932 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 85 | 165 | 261438 | 4132914 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 86 | 167 | 263119 | 4132755 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 87 | 169 | 264714 | 4132711 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 88 | 171 | 256623 | 4132053 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 89 | 173 | 258219 | 4132006 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 90 | 174 | 259194 | 4131979 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 91 | 175 | 259814 | 4131961 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 92 | 176 | 260793 | 4132044 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 93 | 178 | 264689 | 4131823 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 94 | 180 | 266192 | 4131670 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 95 | 182 | 254920 | 4131436 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 96 | 184 | 256604 | 4131387 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 97 | 186 | 258200 | 4131341 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 98 | 188 | 254388 | 4131451 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 99 | 190 | 264670 | 4131157 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 100 | 192 | 265645 | 4131130 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 101 | 194 | 261302 | 4131252 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 102 | 196 | 267149 | 4130977 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 103 | 198 | 272024 | 4130843 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 104 | 200 | 273619 | 4130800 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 105 | 202 | 272644 | 4130826 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 106 | 204 | 275835 | 4130741 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 107 | 205 | 276811 | 4130714 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 108 | 207 | 277431 | 4130698 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 109 | 209 | 278406 | 4130672 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 110 | 211 | 252675 | 4130502 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 111 | 213 | 254270 | 4130455 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 112 | 214 | 254980 | 4130435 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 113 | 215 | 255958 | 4130517 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 114 | 217 | 258263 | 4130450 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 115 | 218 | 259681 | 4130410 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 116 | 220 | 264731 | 4130156 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 117 | 222 | 267216 | 4130197 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 118 | 224 | 251680 | 4129865 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |

Table A-30. Small Wellhead Engine Emission Inventory (Alternative 2) (continued)

| Source Description | Well Count | Record Number | UTM Easting (m) | UTM Northing (m) | NOx (t/yr) | CO (t/yr) | HAP (t/yr) | Stack Height (m) | Stack Diameter (m) | Stack Velocity (m/s) | Stack Temp (°K) |
|--------------------|------------|---------------|-----------------|------------------|------------|-----------|------------|------------------|--------------------|----------------------|-----------------|
| wellhead engine | 119 | 226 | 252658 | 4129947 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 120 | 228 | 254254 | 4129901 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 121 | 229 | 270404 | 4129999 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 122 | 230 | 254963 | 4129880 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 123 | 232 | 271908 | 4129847 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 124 | 234 | 273504 | 4129804 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 125 | 236 | 275191 | 4129869 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 126 | 237 | 275723 | 4129855 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 127 | 239 | 251148 | 4129881 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 128 | 241 | 257531 | 4129694 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 129 | 242 | 279003 | 4129768 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 130 | 244 | 278379 | 4129673 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 131 | 246 | 255935 | 4129740 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 132 | 248 | 265513 | 4129579 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 133 | 249 | 260723 | 4129603 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 134 | 251 | 269499 | 4129358 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 135 | 253 | 276769 | 4129161 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 136 | 255 | 278986 | 4129103 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 137 | 257 | 279960 | 4129077 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 138 | 259 | 281468 | 4129038 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 139 | 261 | 250143 | 4128911 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 140 | 263 | 251742 | 4128975 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 141 | 265 | 252626 | 4128838 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 142 | 266 | 253338 | 4128927 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 143 | 267 | 254934 | 4128881 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 144 | 268 | 255913 | 4128964 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 145 | 270 | 250038 | 4128359 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 146 | 272 | 269472 | 4128359 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 147 | 274 | 251722 | 4128309 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 148 | 275 | 254120 | 4128349 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 149 | 277 | 278959 | 4128104 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 150 | 279 | 255890 | 4128187 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 151 | 281 | 268658 | 4127826 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 152 | 283 | 271851 | 4127738 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 153 | 285 | 278321 | 4127454 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 154 | 287 | 283023 | 4127443 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 155 | 289 | 249388 | 4127378 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 156 | 291 | 283466 | 4127431 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 157 | 292 | 254268 | 4127345 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 158 | 294 | 259589 | 4127192 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 159 | 296 | 263842 | 4126960 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 160 | 297 | 249371 | 4126823 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 161 | 299 | 269426 | 4126693 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 162 | 301 | 274215 | 4126564 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 163 | 303 | 283089 | 4126552 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 164 | 305 | 283709 | 4126536 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 165 | 307 | 279890 | 4126413 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 166 | 309 | 257438 | 4126476 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 167 | 311 | 262227 | 4126339 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 168 | 313 | 273402 | 4126031 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 169 | 315 | 283695 | 4125982 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 170 | 317 | 278901 | 4125884 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 171 | 319 | 280497 | 4125842 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 172 | 321 | 247833 | 4125870 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 173 | 323 | 251561 | 4125870 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 174 | 325 | 261315 | 4125476 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 175 | 327 | 264505 | 4125275 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 176 | 329 | 269384 | 4125140 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 177 | 331 | 282073 | 4125024 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |

Table A-30. Small Wellhead Engine Emission Inventory (Alternative 2) (continued)

| Source Description | Well Count | Record Number | UTM Easting (m) | UTM Northing (m) | NOx (t/yr) | CO (t/yr) | HAP (t/yr) | Stack Height (m) | Stack Diameter (m) | Stack Velocity (m/s) | Stack Temp (°K) |
|--------------------|------------|---------------|-----------------|------------------|------------|-----------|------------|------------------|--------------------|----------------------|-----------------|
| wellhead engine | 178 | 333 | 258904 | 4124990 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 179 | 335 | 260501 | 4124944 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 180 | 337 | 248253 | 4125080 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 181 | 339 | 246738 | 4124903 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 182 | 341 | 278875 | 4124885 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 183 | 343 | 279850 | 4124860 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 184 | 345 | 266885 | 4124654 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 185 | 347 | 262712 | 4124660 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 186 | 348 | 265462 | 4124583 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 187 | 350 | 246186 | 4124253 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 188 | 352 | 279832 | 4124194 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 189 | 354 | 280454 | 4124178 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 190 | 356 | 250980 | 4124221 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 191 | 358 | 257985 | 4123905 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 192 | 359 | 261268 | 4123811 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 193 | 361 | 264462 | 4123721 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 194 | 363 | 248207 | 4123526 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 195 | 365 | 249892 | 4123476 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 196 | 367 | 277236 | 4123374 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 197 | 369 | 278209 | 4123237 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 198 | 371 | 246688 | 4123238 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 199 | 373 | 280427 | 4123179 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 200 | 375 | 246245 | 4123252 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 201 | 377 | 244644 | 4123189 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 202 | 379 | 268435 | 4122945 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 203 | 380 | 262668 | 4123106 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 204 | 382 | 270121 | 4122899 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 205 | 384 | 244631 | 4122745 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 206 | 386 | 278816 | 4122666 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 207 | 388 | 280413 | 4122625 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 208 | 390 | 273492 | 4122808 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 209 | 392 | 276595 | 4122613 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 210 | 394 | 259452 | 4122420 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 211 | 396 | 269121 | 4122038 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 212 | 398 | 273380 | 4121922 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 213 | 400 | 274977 | 4121880 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 214 | 402 | 281455 | 4121709 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 215 | 404 | 278703 | 4121781 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 216 | 406 | 280390 | 4121736 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 217 | 408 | 274947 | 4120770 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 218 | 410 | 276456 | 4120730 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 219 | 412 | 277432 | 4120704 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 220 | 414 | 279650 | 4120646 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 221 | 416 | 290031 | 4120269 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 222 | 418 | 275817 | 4120080 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 223 | 420 | 277414 | 4120038 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 224 | 422 | 279015 | 4120107 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 225 | 424 | 289132 | 4119848 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 226 | 426 | 290730 | 4119808 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 227 | 428 | 274814 | 4119108 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 228 | 430 | 276415 | 4119176 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 229 | 432 | 277391 | 4119150 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 230 | 434 | 279610 | 4119092 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 231 | 436 | 290705 | 4118809 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 232 | 438 | 275687 | 4118529 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 233 | 440 | 277373 | 4118485 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 234 | 442 | 278971 | 4118443 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 235 | 444 | 274772 | 4117554 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 236 | 446 | 277968 | 4117469 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |

Table A-30. Small Wellhead Engine Emission Inventory (Alternative 2) (continued)

| Source Description | Well Count | Record Number | UTM Easting (m) | UTM Northing (m) | NOx (t/yr) | CO (t/yr) | HAP (t/yr) | Stack Height (m) | Stack Diameter (m) | Stack Velocity (m/s) | Stack Temp (°K) |
|------------------------|------------|---------------|-----------------|------------------|--------------|--------------|-------------|------------------|--------------------|----------------------|-----------------|
| wellhead engine | 237 | 448 | 277258 | 4117488 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 238 | 450 | 283653 | 4117432 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 239 | 452 | 290666 | 4117255 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 240 | 454 | 277240 | 4116822 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 241 | 456 | 278930 | 4116889 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 242 | 458 | 275731 | 4116862 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 243 | 460 | 277217 | 4115934 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 244 | 462 | 279525 | 4115874 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 245 | 464 | 291513 | 4115569 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 246 | 466 | 277910 | 4115250 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 247 | 468 | 279508 | 4115208 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 248 | 470 | 290700 | 4115034 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 249 | 472 | 292117 | 4114888 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 250 | 474 | 279393 | 4114212 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 251 | 476 | 281081 | 4114168 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 252 | 478 | 291563 | 4114013 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 253 | 480 | 279201 | 4113661 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 254 | 482 | 280977 | 4113615 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 255 | 484 | 291547 | 4113347 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 256 | 488 | 281938 | 4119808 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 257 | 490 | 280586 | 4119067 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 258 | 492 | 281880 | 4117589 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 259 | 494 | 280969 | 4116725 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 260 | 496 | 283240 | 4115222 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 261 | 498 | 281639 | 4115152 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 262 | 500 | 284423 | 4119744 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 263 | 501 | 284408 | 4119190 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 264 | 503 | 283587 | 4118322 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 265 | 505 | 280281 | 4120962 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 266 | 507 | 281320 | 4119936 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 267 | 509 | 280658 | 4118398 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 268 | 511 | 280546 | 4117513 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 269 | 513 | 280505 | 4115959 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 270 | 515 | 282831 | 4116566 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 271 | 517 | 282573 | 4113463 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 272 | 519 | 283679 | 4114989 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 273 | 521 | 283636 | 4116767 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 274 | 523 | 282722 | 4115791 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Total Emissions | | | | | 1,260 | 1,096 | 27.4 | | | | |

Table A-31. Small Wellhead Engine Emission Inventory (Alternative 3)

| Source Description | Well Count | Record Number | UTM Easting (m) | UTM Northing (m) | NOx (t/yr) | CO (t/yr) | HAP (t/yr) | Stack Height (m) | Stack Diameter (m) | Stack Velocity (m/s) | Stack Temp (°K) |
|--------------------|------------|---------------|-----------------|------------------|------------|-----------|------------|------------------|--------------------|----------------------|-----------------|
| Huber engine | 1 | 5 | 264640 | 4126938 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 2 | 13 | 258942 | 4123212 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 3 | 148 | 263842 | 4126960 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 4 | 171 | 262712 | 4124660 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 5 | 178 | 261268 | 4123811 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 6 | 190 | 262668 | 4123106 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 7 | 1 | 263008 | 4131981 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 8 | 2 | 259133 | 4129870 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 9 | 117 | 260793 | 4132044 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 10 | 118 | 261302 | 4131252 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 11 | 120 | 258263 | 4130450 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 12 | 126 | 257531 | 4129694 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 13 | 128 | 260723 | 4129603 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 14 | 133 | 253338 | 4128927 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 15 | 134 | 254934 | 4128881 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 16 | 137 | 254120 | 4128349 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 17 | 145 | 254268 | 4127345 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 1 | 3 | 263091 | 4128647 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 2 | 6 | 271025 | 4126761 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 3 | 8 | 270212 | 4126228 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 4 | 10 | 266019 | 4125455 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 5 | 12 | 260454 | 4123279 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 6 | 15 | 284474 | 4121742 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 7 | 17 | 289873 | 4113944 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 8 | 19 | 289820 | 4115389 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 9 | 21 | 290652 | 4116701 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 10 | 23 | 289953 | 4117162 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 11 | 25 | 289190 | 4118625 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 12 | 27 | 289976 | 4118050 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 13 | 29 | 292360 | 4113882 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 14 | 31 | 293869 | 4113846 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 15 | 33 | 293409 | 4113191 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 16 | 35 | 294938 | 4113931 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 17 | 37 | 295549 | 4113471 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 18 | 39 | 296251 | 4113122 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 19 | 41 | 279846 | 4128080 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 20 | 43 | 280629 | 4127505 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 21 | 45 | 281439 | 4127927 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 22 | 47 | 281384 | 4125819 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 23 | 49 | 282276 | 4126018 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 24 | 51 | 274918 | 4122991 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 25 | 53 | 274862 | 4124214 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 26 | 55 | 273443 | 4124253 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 27 | 57 | 272626 | 4123608 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 28 | 59 | 277363 | 4128146 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 29 | 61 | 276595 | 4125945 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 30 | 63 | 280560 | 4124841 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 31 | 65 | 282056 | 4124358 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 32 | 67 | 281321 | 4123378 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 33 | 69 | 282013 | 4122694 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 34 | 71 | 282946 | 4124446 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 35 | 73 | 283718 | 4123427 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 36 | 75 | 282909 | 4123004 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 37 | 77 | 282966 | 4121781 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 38 | 79 | 285118 | 4122614 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 39 | 81 | 285894 | 4121706 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 40 | 83 | 283641 | 4120431 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 41 | 85 | 285422 | 4120608 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 42 | 87 | 285845 | 4119819 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |

Table A-31. Small Wellhead Engine Emission Inventory (Alternative 3) (continued)

| Source Description | Well Count | Record Number | UTM Easting (m) | UTM Northing (m) | NOx (t/yr) | CO (t/yr) | HAP (t/yr) | Stack Height (m) | Stack Diameter (m) | Stack Velocity (m/s) | Stack Temp (°K) |
|--------------------|------------|---------------|-----------------|------------------|------------|-----------|------------|------------------|--------------------|----------------------|-----------------|
| wellhead engine | 43 | 89 | 287640 | 4120551 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 44 | 91 | 286911 | 4119793 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 45 | 93 | 288433 | 4120309 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 46 | 95 | 288383 | 4118312 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 47 | 97 | 287676 | 4118441 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 48 | 99 | 286802 | 4119018 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 49 | 101 | 286075 | 4118370 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 50 | 103 | 285382 | 4119054 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 51 | 105 | 286749 | 4116909 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 52 | 107 | 287554 | 4117111 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 53 | 109 | 288435 | 4116867 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 54 | 111 | 284120 | 4118309 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 55 | 113 | 282565 | 4120014 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 56 | 115 | 282001 | 4118808 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 57 | 119 | 281705 | 4114262 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 58 | 122 | 283997 | 4113537 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 59 | 124 | 285790 | 4114158 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 60 | 127 | 286576 | 4113583 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 61 | 130 | 288280 | 4114206 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 62 | 132 | 288313 | 4115538 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 63 | 136 | 286812 | 4115908 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 64 | 139 | 285907 | 4115265 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 65 | 141 | 284323 | 4115860 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 66 | 143 | 284011 | 4117534 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 67 | 146 | 285418 | 4113501 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 68 | 149 | 276086 | 4113522 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 69 | 151 | 275488 | 4114425 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 70 | 153 | 273982 | 4114577 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 71 | 155 | 274798 | 4115221 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 72 | 157 | 274816 | 4115887 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 73 | 159 | 276507 | 4115953 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 74 | 161 | 276353 | 4116846 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 75 | 163 | 260818 | 4132932 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 76 | 165 | 261438 | 4132914 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 77 | 167 | 263119 | 4132755 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 78 | 169 | 264714 | 4132711 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 79 | 172 | 257598 | 4132025 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 80 | 174 | 259194 | 4131979 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 81 | 176 | 260793 | 4132044 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 82 | 179 | 265661 | 4131685 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 83 | 181 | 267167 | 4131643 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 84 | 183 | 255895 | 4131407 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 85 | 185 | 257491 | 4131361 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 86 | 187 | 267959 | 4131399 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 87 | 189 | 264049 | 4131174 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 88 | 192 | 265645 | 4131130 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 89 | 194 | 261302 | 4131252 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 90 | 196 | 267149 | 4130977 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 91 | 198 | 272024 | 4130843 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 92 | 200 | 273619 | 4130800 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 93 | 202 | 272644 | 4130826 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 94 | 204 | 275835 | 4130741 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 95 | 206 | 279027 | 4130656 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 96 | 208 | 270429 | 4130887 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 97 | 210 | 280001 | 4130630 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 98 | 212 | 253296 | 4130484 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 99 | 214 | 254980 | 4130435 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 100 | 215 | 255958 | 4130517 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 101 | 217 | 258263 | 4130450 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |

Table A-31. Small Wellhead Engine Emission Inventory (Alternative 3) (continued)

| Source Description | Well Count | Record Number | UTM Easting (m) | UTM Northing (m) | NOx (t/yr) | CO (t/yr) | HAP (t/yr) | Stack Height (m) | Stack Diameter (m) | Stack Velocity (m/s) | Stack Temp (°K) |
|------------------------|------------|---------------|-----------------|------------------|------------|------------|-------------|------------------|--------------------|----------------------|-----------------|
| wellhead engine | 102 | 219 | 262961 | 4130317 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 103 | 221 | 266235 | 4130003 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 104 | 223 | 268808 | 4130043 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Total Emissions | | | | | 557 | 484 | 12.1 | | | | |

Table A-32. Small Wellhead Engine Emission Inventory (Alternative 4)

| Source Description | Well Count | Record Number | UTM Easting (m) | UTM Northing (m) | NOx (t/yr) | CO (t/yr) | HAP (t/yr) | Stack Height (m) | Stack Diameter (m) | Stack Velocity (m/s) | Stack Temp (°K) |
|--------------------|------------|---------------|-----------------|------------------|------------|-----------|------------|------------------|--------------------|----------------------|-----------------|
| Huber engine | 1 | 1 | 264640 | 4126938 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 2 | 2 | 258942 | 4123212 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 3 | 5 | 261268 | 4123811 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 4 | 13 | 263842 | 4126960 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 5 | 70 | 262712 | 4124660 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 6 | 76 | 262668 | 4123106 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 7 | 110 | 263008 | 4131981 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 8 | 157 | 259133 | 4129870 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 9 | 158 | 261302 | 4131252 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 10 | 160 | 260723 | 4129603 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 11 | 163 | 260793 | 4132044 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 12 | 164 | 258263 | 4130450 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 13 | 166 | 257531 | 4129694 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 14 | 171 | 253338 | 4128927 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 15 | 173 | 254934 | 4128881 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 16 | 181 | 254120 | 4128349 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 17 | 186 | 254268 | 4127345 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 1 | 3 | 263091 | 4128647 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 2 | 6 | 271025 | 4126761 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 3 | 8 | 270212 | 4126228 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 4 | 10 | 266019 | 4125455 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 5 | 12 | 260454 | 4123279 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 6 | 15 | 285007 | 4121729 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 7 | 17 | 288280 | 4114206 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 8 | 19 | 287197 | 4113567 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 9 | 21 | 283997 | 4113537 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 10 | 23 | 287506 | 4115225 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 11 | 25 | 285904 | 4115154 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 12 | 27 | 284349 | 4116860 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 13 | 29 | 289953 | 4117162 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 14 | 31 | 289176 | 4118070 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 15 | 33 | 286891 | 4119015 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 16 | 35 | 285937 | 4119928 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 17 | 37 | 285422 | 4120608 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 18 | 39 | 286072 | 4118259 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 19 | 41 | 279761 | 4124862 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 20 | 43 | 280163 | 4126629 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 21 | 45 | 279751 | 4127860 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 22 | 47 | 277173 | 4114270 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 23 | 49 | 276086 | 4113522 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 24 | 51 | 273982 | 4114577 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 25 | 53 | 275619 | 4115977 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 26 | 55 | 278045 | 4117023 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 27 | 57 | 277572 | 4119256 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 28 | 59 | 275704 | 4119195 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 29 | 61 | 277346 | 4120817 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 30 | 63 | 278793 | 4121778 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 31 | 65 | 278212 | 4123348 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 32 | 67 | 276442 | 4116843 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 33 | 69 | 289992 | 4118716 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 34 | 72 | 259681 | 4130410 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 35 | 74 | 266235 | 4130003 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 36 | 77 | 269499 | 4129358 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 37 | 79 | 275170 | 4129093 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 38 | 81 | 278338 | 4128120 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 39 | 83 | 275043 | 4127652 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 40 | 85 | 282048 | 4127468 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 41 | 87 | 259589 | 4127192 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 42 | 89 | 269426 | 4126693 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |

Table A-32. Small Wellhead Engine Emission Inventory (Alternative 4) (continued)

| Source Description | Well Count | Record Number | UTM Easting (m) | UTM Northing (m) | NOx (t/yr) | CO (t/yr) | HAP (t/yr) | Stack Height (m) | Stack Diameter (m) | Stack Velocity (m/s) | Stack Temp (°K) |
|------------------------|------------|---------------|-----------------|------------------|------------|------------|-------------|------------------|--------------------|----------------------|-----------------|
| wellhead engine | 43 | 91 | 257438 | 4126476 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 44 | 93 | 271806 | 4126074 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 45 | 95 | 274998 | 4125988 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 46 | 97 | 267787 | 4125184 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 47 | 99 | 271870 | 4125184 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 48 | 101 | 250024 | 4124916 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 49 | 103 | 268570 | 4124608 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 50 | 105 | 282056 | 4124358 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 51 | 107 | 276639 | 4124278 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 52 | 109 | 254173 | 4124127 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 53 | 112 | 275725 | 4123303 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 54 | 114 | 252554 | 4123397 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 55 | 116 | 254151 | 4123350 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 56 | 118 | 263647 | 4123190 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 57 | 120 | 268435 | 4122945 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 58 | 122 | 270121 | 4122899 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 59 | 124 | 283524 | 4122766 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 60 | 126 | 273492 | 4122808 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 61 | 128 | 276595 | 4122613 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 62 | 130 | 269121 | 4122038 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 63 | 132 | 273380 | 4121922 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 64 | 134 | 284474 | 4121742 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 65 | 136 | 277106 | 4121823 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 66 | 138 | 279032 | 4120773 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 67 | 140 | 274134 | 4120236 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 68 | 142 | 274107 | 4119237 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 69 | 144 | 277995 | 4118468 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 70 | 146 | 277258 | 4117488 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 71 | 148 | 288446 | 4117311 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 72 | 150 | 275731 | 4116862 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 73 | 152 | 290649 | 4116590 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 74 | 154 | 279508 | 4115208 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 75 | 156 | 289965 | 4114053 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 76 | 161 | 265513 | 4129579 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 77 | 165 | 255913 | 4128964 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 78 | 168 | 255890 | 4128187 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 79 | 170 | 271851 | 4127738 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 80 | 174 | 262227 | 4126339 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 81 | 176 | 261315 | 4125476 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 82 | 178 | 258904 | 4124990 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 83 | 180 | 248253 | 4125080 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 84 | 183 | 262158 | 4123898 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 85 | 185 | 248207 | 4123526 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 86 | 188 | 264329 | 4122171 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Total Emissions | | | | | 474 | 412 | 10.3 | | | | |

Table A-33. Small Wellhead Engine Emission Inventory (Alternative 5)

| Source Description | Well Count | Record Number | UTM Easting (m) | UTM Northing (m) | NOx (t/yr) | CO (t/yr) | HAP (t/yr) | Stack Height (m) | Stack Diameter (m) | Stack Velocity (m/s) | Stack Temp (°K) |
|--------------------|------------|---------------|-----------------|------------------|------------|-----------|------------|------------------|--------------------|----------------------|-----------------|
| Huber engine | 1 | 207 | 263842 | 4126960 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 2 | 230 | 262712 | 4124660 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 3 | 237 | 261268 | 4123811 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 4 | 249 | 262668 | 4123106 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 5 | hub1 | 264640 | 4126938 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 6 | hub2 | 258942 | 4123212 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 7 | 176 | 260793 | 4132044 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 8 | 177 | 261302 | 4131252 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 9 | 179 | 258263 | 4130450 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 10 | 185 | 257531 | 4129694 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 11 | 187 | 260723 | 4129603 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 12 | 192 | 253338 | 4128927 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 13 | 193 | 254934 | 4128881 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 14 | 196 | 254120 | 4128349 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Huber engine | 15 | 204 | 254268 | 4127345 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 1 | 1 | 290652 | 4116701 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 2 | 3 | 289953 | 4117162 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 3 | 5 | 289190 | 4118625 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 4 | 7 | 289976 | 4118050 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 5 | 9 | 287640 | 4120551 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 6 | 11 | 288428 | 4120088 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 7 | 13 | 287601 | 4118998 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 8 | 15 | 288313 | 4115538 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 9 | 17 | 271025 | 4126761 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 10 | 19 | 270212 | 4126228 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 11 | 21 | 284474 | 4121742 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 12 | 23 | 260793 | 4132044 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 13 | 25 | 262451 | 4131109 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 14 | 27 | 259681 | 4130410 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 15 | 29 | 264731 | 4130156 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 16 | 31 | 267216 | 4130197 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 17 | 33 | 265513 | 4129579 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 18 | 35 | 262407 | 4129555 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 19 | 37 | 267191 | 4129310 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 20 | 39 | 253338 | 4128927 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 21 | 41 | 255913 | 4128964 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 22 | 43 | 254120 | 4128349 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 23 | 45 | 255890 | 4128187 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 24 | 47 | 263956 | 4127845 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 25 | 49 | 275043 | 4127652 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 26 | 51 | 254268 | 4127345 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 27 | 53 | 262870 | 4127098 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 28 | 55 | 267833 | 4126849 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 29 | 57 | 274215 | 4126564 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 30 | 59 | 268616 | 4126272 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 31 | 61 | 271806 | 4126074 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 32 | 63 | 274998 | 4125988 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 33 | 65 | 261315 | 4125476 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 34 | 67 | 264505 | 4125275 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 35 | 69 | 269384 | 4125140 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 36 | 71 | 258904 | 4124990 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 37 | 73 | 250024 | 4124916 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 38 | 75 | 266885 | 4124654 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 39 | 77 | 262712 | 4124660 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 40 | 79 | 271849 | 4124407 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 41 | 81 | 250980 | 4124221 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 42 | 83 | 257985 | 4123905 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 43 | 85 | 262158 | 4123898 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 44 | 87 | 248207 | 4123526 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |

Table A-33. Small Wellhead Engine Emission Inventory (Alternative 5) (continued)

| Source Description | Well Count | Record Number | UTM Easting (m) | UTM Northing (m) | NOx (t/yr) | CO (t/yr) | HAP (t/yr) | Stack Height (m) | Stack Diameter (m) | Stack Velocity (m/s) | Stack Temp (°K) |
|------------------------|------------|---------------|-----------------|------------------|------------|------------|------------|------------------|--------------------|----------------------|-----------------|
| wellhead engine | 45 | 89 | 249892 | 4123476 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 46 | 91 | 277236 | 4123374 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 47 | 93 | 263647 | 4123190 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 48 | 95 | 268435 | 4122945 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 49 | 97 | 269323 | 4122921 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 50 | 99 | 271718 | 4122856 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 51 | 101 | 249334 | 4122604 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 52 | 103 | 252975 | 4122608 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 53 | 105 | 264329 | 4122171 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 54 | 107 | 270186 | 4122009 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 55 | 109 | 274977 | 4121880 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 56 | 111 | 274947 | 4120770 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 57 | 113 | 274843 | 4120217 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 58 | 115 | 274772 | 4117554 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| wellhead engine | 59 | 117 | 275731 | 4116862 | 4.6 | 4.0 | 0.1 | 1.5 | 0.2 | 3.8 | 477 |
| Total Emissions | | | | | 340 | 296 | 7.4 | | | | |

Table A-34. Near Field Modeling Input Values (Alternative 1)

| Source Count | Source Description | Unit ID | UTM | | Emission Rate | | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|--------------------|----------|-------------|--------------|---------------|----------|-----------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | Easting (m) | Northing (m) | NOx (g/s) | CO (g/s) | HAP (g/s) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 1 | Elmridge 1 | ELM1A | 288,301 | 4,112,688 | 0.52 | 0.69 | 0.08 | 6.6 | 644 | 17.3 | 0.46 | 3.9 | 3.9 | 6,399 |
| 2 | Elmridge 1 | ELM1B | 288,301 | 4,112,698 | 0.52 | 0.69 | 0.08 | 6.6 | 644 | 17.3 | 0.46 | 3.9 | 3.9 | 6,399 |
| 3 | Elmridge 1 | ELM1C | 288,301 | 4,112,708 | 0.52 | 0.69 | 0.08 | 6.6 | 644 | 17.3 | 0.46 | 3.9 | 3.9 | 6,399 |
| 4 | Elmridge 1 | ELM1D | 288,301 | 4,112,718 | 0.52 | 0.69 | 0.08 | 6.6 | 644 | 17.3 | 0.46 | 3.9 | 3.9 | 6,399 |
| 5 | Elmridge 1 | ELM1DEHY | 288,301 | 4,112,728 | 0.13 | 0.11 | 0.00 | 3.5 | 533 | 6.4 | 0.15 | 2.3 | 2.3 | 6,399 |
| 6 | Elmridge 1 | ELM1SEP | 288,301 | 4,112,738 | 0.09 | 0.15 | 0.00 | 3.5 | 533 | 6.4 | 0.15 | 2.3 | 2.3 | 6,399 |
| 7 | Elmridge 2 | ELM2A | 274,470 | 4,114,300 | 0.63 | 0.83 | 0.10 | 9.5 | 644 | 29.2 | 0.38 | 5.9 | 5.9 | 6,996 |
| 8 | Elmridge 2 | ELM2B | 274,470 | 4,114,310 | 0.63 | 0.83 | 0.10 | 9.5 | 644 | 29.2 | 0.38 | 5.9 | 5.9 | 6,996 |
| 9 | Elmridge 2 | ELM2C | 274,470 | 4,114,320 | 0.63 | 0.83 | 0.10 | 9.5 | 644 | 29.2 | 0.38 | 5.9 | 5.9 | 6,996 |
| 10 | Elmridge 2 | ELM2D | 274,470 | 4,114,330 | 0.63 | 0.83 | 0.10 | 9.5 | 644 | 29.2 | 0.38 | 5.9 | 5.9 | 6,996 |
| 11 | Elmridge 2 | ELM2E | 274,470 | 4,114,340 | 0.63 | 0.83 | 0.10 | 9.5 | 644 | 29.2 | 0.38 | 5.9 | 5.9 | 6,996 |
| 12 | Elmridge 2 | ELM2F | 274,470 | 4,114,350 | 0.63 | 0.83 | 0.10 | 9.5 | 644 | 29.2 | 0.38 | 5.9 | 5.9 | 6,996 |
| 13 | Elmridge 2 | ELM2G | 274,470 | 4,114,360 | 0.63 | 0.83 | 0.10 | 9.5 | 644 | 29.2 | 0.38 | 5.9 | 5.9 | 6,996 |
| 14 | Elmridge 2 | ELM2H | 274,470 | 4,114,370 | 0.63 | 0.83 | 0.10 | 9.5 | 644 | 29.2 | 0.38 | 5.9 | 5.9 | 6,996 |
| 15 | Elmridge 2 | ELM2I | 274,470 | 4,114,380 | 0.63 | 0.83 | 0.10 | 9.5 | 644 | 29.2 | 0.38 | 5.9 | 5.9 | 6,996 |
| 16 | Elmridge 2 | ELM2DEHY | 274,470 | 4,114,270 | 0.13 | 0.11 | 0.00 | 3.5 | 533 | 6.4 | 0.15 | 2.0 | 2.0 | 6,996 |
| 17 | Elmridge 2 | ELM2SEP | 274,470 | 4,114,280 | 0.11 | 0.36 | 0.00 | 3.5 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 6,996 |
| 18 | Elmridge 2 | ELM2SEPa | 274,470 | 4,114,290 | 0.11 | 0.36 | 0.00 | 3.5 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 6,996 |
| 19 | PETROX 1 | PET1 | 292,405 | 4,113,912 | 0.26 | 0.34 | 0.04 | 3.1 | 644 | 24.1 | 0.3 | 2.0 | 2.0 | 6,396 |
| 20 | PETROX 1 | PET1DEH | 292,405 | 4,113,922 | 0.13 | 0.11 | 0.00 | 3.0 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 6,396 |
| 21 | PETROX 1 | PET1SEP | 292,405 | 4,113,932 | 0.02 | 0.02 | 0.00 | 3.0 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 6,396 |
| 22 | PETROX 2 | PET2 | 286,151 | 4,120,460 | 0.79 | 1.06 | 0.12 | 9.1 | 644 | 26.3 | 0.46 | 4.9 | 4.9 | 7,613 |
| 23 | PETROX 2 | PET2DEH | 286,151 | 4,120,470 | 0.13 | 0.11 | 0.00 | 3.1 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 7,613 |
| 24 | PETROX 2 | PET2SEP | 286,151 | 4,120,480 | 0.03 | 0.06 | 0.00 | 3.1 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 7,613 |
| 25 | PETROX 2 | PET2SEPa | 286,151 | 4,120,450 | 0.03 | 0.06 | 0.00 | 3.1 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 7,613 |
| 26 | BP AMOCO 1 | BP1A | 273,670 | 4,124,111 | 0.56 | 0.74 | 0.09 | 4.6 | 644 | 18.4 | 0.46 | 3.0 | 3.0 | 7,141 |
| 27 | BP AMOCO 1 | BP1B | 273,670 | 4,124,121 | 0.56 | 0.74 | 0.09 | 4.6 | 644 | 18.4 | 0.46 | 3.0 | 3.0 | 7,141 |
| 28 | BP AMOCO 1 | BP1C | 273,670 | 4,124,131 | 0.56 | 0.74 | 0.09 | 4.6 | 644 | 18.4 | 0.46 | 3.0 | 3.0 | 7,141 |
| 29 | BP AMOCO 1 | BP1SEP | 273,670 | 4,124,141 | 0.13 | 0.11 | 0.00 | 3 | 533 | 6.4 | 0.15 | 2.0 | 2.0 | 7,141 |
| 30 | BP AMOCO 1 | BP1DEH | 273,670 | 4,124,151 | 0.14 | 0.12 | 0.00 | 3 | 533 | 6.4 | 0.15 | 2.0 | 2.0 | 7,141 |
| 31 | BP AMOCO 2 | BP2A | 275,030 | 4,114,050 | 0.63 | 0.83 | 0.10 | 4.6 | 644 | 29.9 | 0.38 | 3.0 | 3.0 | 6,799 |
| 32 | BP AMOCO 2 | BP2B | 275,030 | 4,114,060 | 0.63 | 0.83 | 0.10 | 4.6 | 644 | 29.9 | 0.38 | 3.0 | 3.0 | 6,799 |
| 33 | BP AMOCO 2 | BP2SEP | 275,030 | 4,114,070 | 0.13 | 0.11 | 0.00 | 3 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 6,799 |
| 34 | BP AMOCO 2 | BP2DEH | 275,030 | 4,114,080 | 0.11 | 0.09 | 0.00 | 3 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 6,799 |
| 35 | PETROX 3 | PET3 | 283,100 | 4,123,180 | 0.26 | 0.34 | 0.04 | 3.05 | 644 | 24.1 | 0.3 | 2.0 | 2.0 | 7,616 |

Table A-34. Near Field Modeling Input Values (Alternative 1) (continued)

| Source Count | Source Description | Unit ID | UTM | | Emission Rate | | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|--------------------|---------|-------------|--------------|---------------|----------|-----------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | Easting (m) | Northing (m) | NOx (g/s) | CO (g/s) | HAP (g/s) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 36 | PETROX 3 | PET3SEP | 283,100 | 4,123,190 | 0.13 | 0.11 | 0.04 | 3 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 7,616 |
| 37 | PETROX 3 | PET3DEH | 283,100 | 4,123,200 | 0.02 | 0.02 | 0.04 | 3 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 7,616 |
| 38 | PETROX 4 | PET4 | 281,500 | 4,123,161 | 0.26 | 0.34 | 0.04 | 3.05 | 644 | 24.1 | 0.3 | 2.0 | 2.0 | 8,197 |
| 39 | PETROX 4 | PET4SEP | 281,500 | 4,123,171 | 0.13 | 0.11 | 0.00 | 3 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 8,197 |
| 40 | PETROX 4 | PET4DEH | 281,500 | 4,123,181 | 0.02 | 0.02 | 0.00 | 3 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 8,197 |
| 41 | PURE 1 | PUR1 | 251,600 | 4,125,830 | 0.63 | 0.83 | 0.10 | 4.6 | 644 | 29.9 | 0.38 | 3.0 | 3.0 | 7,036 |
| 42 | PURE 1 | PUR1SEP | 251,600 | 4,125,840 | 0.13 | 0.11 | 0.10 | 3 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 7,036 |
| 43 | PURE 1 | PUR1DEH | 251,600 | 4,125,850 | 0.05 | 0.05 | 0.10 | 3 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 7,036 |
| 44 | PURE 2 | PUR2 | 249,350 | 4,125,160 | 0.10 | 0.13 | 0.02 | 3 | 583 | 21.5 | 0.18 | 2.0 | 2.0 | 6,803 |
| 45 | PURE 2 | PUR2SEP | 249,350 | 4,125,170 | 0.13 | 0.11 | 0.00 | 3 | 533 | 6.44 | 0.18 | 2.0 | 2.0 | 6,803 |
| 46 | PURE 2 | PUR2DEH | 249,350 | 4,125,180 | 0.01 | 0.01 | 0.00 | 3 | 533 | 6.44 | 0.15 | 2.0 | 2.0 | 6,803 |
| 47 | BP 3 | BP3A | 272,164 | 4,126,575 | 0.63 | 0.83 | 0.10 | 4.6 | 644 | 29.9 | 0.38 | 3.0 | 3.0 | 6,996 |
| 48 | BP 3 | BP3B | 272,164 | 4,126,585 | 0.63 | 0.83 | 0.10 | 4.6 | 644 | 29.9 | 0.38 | 3.0 | 3.0 | 6,996 |
| 49 | BP 3 | BP3SEP | 272,164 | 4,126,595 | 0.13 | 0.11 | 0.00 | 3 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 6,996 |
| 50 | BP 3 | BP3DEH | 272,164 | 4,126,605 | 0.11 | 0.09 | 0.00 | 3 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 6,996 |
| 51 | BP 4 | BP4A | 259,000 | 4,124,000 | 0.56 | 0.74 | 0.09 | 4.6 | 644 | 18.4 | 0.46 | 3.0 | 3.0 | 7,082 |
| 52 | BP 4 | BP4B | 259,000 | 4,124,010 | 0.56 | 0.74 | 0.09 | 4.6 | 644 | 18.4 | 0.46 | 3.0 | 3.0 | 7,082 |
| 53 | BP 4 | BP4C | 259,000 | 4,124,020 | 0.56 | 0.74 | 0.09 | 4.6 | 644 | 18.4 | 0.46 | 3.0 | 3.0 | 7,082 |
| 54 | BP 4 | BP4SEP | 259,000 | 4,124,030 | 0.13 | 0.11 | 0.00 | 3 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 7,082 |
| 55 | BP 4 | BP4DEH | 259,000 | 4,124,040 | 0.14 | 0.12 | 0.00 | 3 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 7,082 |
| 56 | Cross Timbers | HUB1 | 257,000 | 4,125,000 | 0.52 | 0.69 | 0.08 | 4.6 | 644.0 | 17.3 | 0.5 | 3.0 | 3.0 | 6,934 |
| 57 | Cross Timbers | HUB2 | 257,000 | 4,125,010 | 0.52 | 0.69 | 0.08 | 4.6 | 644.0 | 17.3 | 0.5 | 3.0 | 3.0 | 6,934 |
| 58 | Cross Timbers | HUBSEP | 257,000 | 4,125,020 | 0.13 | 0.11 | 0.00 | 3.0 | 533.0 | 6.4 | 0.2 | 2.0 | 2.0 | 6,934 |
| 59 | Cross Timbers | HUBDEH | 257,000 | 4,125,030 | 0.09 | 0.08 | 0.00 | 3.0 | 533.0 | 6.4 | 0.2 | 2.0 | 2.0 | 6,934 |
| 60 | Bayfield | BAY1 | 271,500 | 4,125,000 | 0.83 | 1.11 | 0.13 | 7.5 | 644.0 | 28.6 | 0.5 | 4.9 | 4.9 | 6,996 |
| 61 | Bayfield | BAYDEH | 271,500 | 4,125,010 | 0.13 | 0.11 | 0.00 | 3.0 | 533.0 | 6.4 | 0.2 | 2.0 | 2.0 | 6,996 |
| 62 | Bayfield | BAYSEP | 271,500 | 4,125,020 | 0.07 | 0.06 | 0.00 | 3.0 | 533.0 | 6.4 | 0.2 | 2.0 | 2.0 | 6,996 |
| 63 | Huber engine | 5 | 264,640 | 4,126,938 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,478 |
| 64 | Huber engine | 13 | 258,942 | 4,123,212 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 6,996 |
| 65 | Huber engine | 207 | 263,842 | 4,126,960 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,744 |
| 66 | Huber engine | 230 | 262,712 | 4,124,660 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,396 |
| 67 | Huber engine | 237 | 261,268 | 4,123,811 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,022 |
| 68 | Huber engine | 249 | 262,668 | 4,123,106 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 6,996 |
| 69 | Huber engine | 1 | 263,008 | 4,131,981 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,970 |
| 70 | Huber engine | 2 | 259,133 | 4,129,870 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,498 |

⁽¹⁾ 0.0017584 g/s HAP emission

Table A-34. Near Field Modeling Input Values (Alternative 1) (continued)

| Source Count | Source Description | Unit ID | UTM | | Emission Rate | | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|--------------------|---------|-------------|--------------|---------------|----------|-----------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | Easting (m) | Northing (m) | NOx (g/s) | CO (g/s) | HAP (g/s) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 71 | Huber engine | 176 | 260,793 | 4,132,044 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,875 |
| 72 | Huber engine | 177 | 261,302 | 4,131,252 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,738 |
| 73 | Huber engine | 179 | 258,263 | 4,130,450 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,574 |
| 74 | Huber engine | 185 | 257,531 | 4,129,694 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,383 |
| 75 | Huber engine | 187 | 260,723 | 4,129,603 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,564 |
| 76 | Huber engine | 192 | 253,338 | 4,128,927 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,272 |
| 77 | Huber engine | 193 | 254,934 | 4,128,881 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,311 |
| 78 | Huber engine | 196 | 254,120 | 4,128,349 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,196 |
| 79 | Huber engine | 204 | 254,268 | 4,127,345 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,052 |
| 80 | wellhead engine | 3 | 282,897 | 4,126,002 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,957 |
| 81 | wellhead engine | 6 | 283,641 | 4,120,431 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 8,797 |
| 82 | wellhead engine | 8 | 285,894 | 4,121,706 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,410 |
| 83 | wellhead engine | 10 | 277,316 | 4,126,370 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,446 |
| 84 | wellhead engine | 12 | 292,360 | 4,113,882 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 6,396 |
| 85 | wellhead engine | 15 | 261,315 | 4,125,476 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,206 |
| 86 | wellhead engine | 17 | 282,848 | 4,120,673 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 8,597 |
| 87 | wellhead engine | 19 | 280,281 | 4,120,962 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 8,102 |
| 88 | wellhead engine | 21 | 280,546 | 4,117,513 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 8,597 |
| 89 | wellhead engine | 23 | 280,340 | 4,119,850 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 8,597 |
| 90 | wellhead engine | 25 | 283,587 | 4,118,322 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 8,085 |
| 91 | wellhead engine | 27 | 280,658 | 4,118,398 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 8,597 |
| 92 | wellhead engine | 29 | 282,768 | 4,117,566 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 8,597 |
| 93 | wellhead engine | 31 | 282,573 | 4,113,463 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,803 |
| 94 | wellhead engine | 33 | 282,831 | 4,116,566 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 8,344 |
| 95 | wellhead engine | 35 | 283,702 | 4,115,877 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,738 |
| 96 | wellhead engine | 37 | 285,237 | 4,116,837 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 8,197 |
| 97 | wellhead engine | 39 | 282,722 | 4,115,791 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 8,029 |
| 98 | wellhead engine | 41 | 285,108 | 4,115,285 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,596 |
| 99 | wellhead engine | 43 | 285,941 | 4,116,597 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,816 |
| 100 | wellhead engine | 45 | 276,507 | 4,115,953 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,895 |
| 101 | wellhead engine | 47 | 274,816 | 4,115,887 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,196 |
| 102 | wellhead engine | 49 | 258,263 | 4,130,450 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,596 |
| 103 | wellhead engine | 51 | 288,535 | 4,117,309 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,196 |
| 104 | wellhead engine | 53 | 286,852 | 4,117,462 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,275 |
| 105 | wellhead engine | 55 | 288,428 | 4,120,088 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,252 |

⁽¹⁾ 0.0017584 g/s HAP emission

Table A-34. Near Field Modeling Input Values (Alternative 1) (continued)

| Source Count | Source Description | Unit ID | UTM | | Emission Rate | | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|--------------------|---------|-------------|--------------|---------------|----------|-----------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | Easting (m) | Northing (m) | NOx (g/s) | CO (g/s) | HAP (g/s) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 106 | wellhead engine | 57 | 287,640 | 4,120,551 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,328 |
| 107 | wellhead engine | 59 | 287,431 | 4,115,782 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,196 |
| 108 | wellhead engine | 61 | 285,349 | 4,114,280 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,537 |
| 109 | wellhead engine | 63 | 286,047 | 4,117,260 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,816 |
| 110 | wellhead engine | 65 | 282,805 | 4,119,009 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 8,797 |
| 111 | wellhead engine | 67 | 274,000 | 4,115,243 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 6,996 |
| 112 | wellhead engine | 69 | 280,586 | 4,119,067 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 8,797 |
| 113 | wellhead engine | 71 | 267,191 | 4,129,310 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,403 |
| 114 | wellhead engine | 73 | 273,532 | 4,127,582 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,206 |
| 115 | wellhead engine | 75 | 269,499 | 4,129,358 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,177 |
| 116 | wellhead engine | 77 | 254,934 | 4,128,881 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,403 |
| 117 | wellhead engine | 79 | 269,384 | 4,125,140 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,045 |
| 118 | wellhead engine | 81 | 276,639 | 4,124,278 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,347 |
| 119 | wellhead engine | 83 | 275,043 | 4,127,652 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,396 |
| 120 | wellhead engine | 85 | 268,570 | 4,124,608 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,045 |
| 121 | wellhead engine | 87 | 271,849 | 4,124,407 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,196 |
| 122 | wellhead engine | 89 | 274,977 | 4,121,880 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,131 |
| 123 | wellhead engine | 91 | 270,121 | 4,122,899 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 6,996 |
| 124 | wellhead engine | 93 | 275,731 | 4,116,862 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,482 |
| 125 | wellhead engine | 95 | 277,106 | 4,121,823 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,350 |
| 126 | wellhead engine | 97 | 274,947 | 4,120,770 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,196 |
| 127 | wellhead engine | 99 | 268,435 | 4,122,945 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 6,996 |
| 128 | wellhead engine | 101 | 248,207 | 4,123,526 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 6,819 |
| 129 | wellhead engine | 103 | 266,885 | 4,124,654 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,396 |
| 130 | wellhead engine | 105 | 263,647 | 4,123,190 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,147 |
| 131 | wellhead engine | 107 | 270,186 | 4,122,009 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 6,954 |
| 132 | wellhead engine | 109 | 289,013 | 4,115,076 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 6,799 |
| 133 | wellhead engine | 111 | 274,215 | 4,126,564 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,196 |
| 134 | wellhead engine | 113 | 259,681 | 4,130,410 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,629 |
| 135 | wellhead engine | 115 | 281,938 | 4,119,808 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 8,797 |
| 136 | wellhead engine | 117 | 276,397 | 4,115,179 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,154 |
| 137 | wellhead engine | 119 | 280,969 | 4,116,725 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 8,597 |
| 138 | wellhead engine | 121 | 255,890 | 4,128,187 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,219 |
| 139 | wellhead engine | 123 | 263,707 | 4,125,297 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,596 |
| 140 | wellhead engine | 125 | 262,712 | 4,124,660 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,544 |

⁽¹⁾ 0.0017584 g/s HAP emission

Table A-34. Near Field Modeling Input Values (Alternative 1) (continued)

| Source Count | Source Description | Unit ID | UTM | | Emission Rate | | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|--------------------|---------|-------------|--------------|---------------|----------|-----------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | Easting (m) | Northing (m) | NOx (g/s) | CO (g/s) | HAP (g/s) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 141 | wellhead engine | 127 | 252,554 | 4,123,397 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 6,960 |
| 142 | wellhead engine | 129 | 273,489 | 4,122,696 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,147 |
| 143 | wellhead engine | 131 | 274,843 | 4,120,217 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,196 |
| 144 | wellhead engine | 133 | 264,329 | 4,122,171 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 6,996 |
| 145 | wellhead engine | 135 | 249,334 | 4,122,604 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 6,796 |
| 146 | wellhead engine | 137 | 271,870 | 4,125,184 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,072 |
| 147 | wellhead engine | 139 | 257,985 | 4,123,905 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,180 |
| 148 | wellhead engine | 141 | 271,806 | 4,126,074 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 6,996 |
| 149 | wellhead engine | 143 | 267,833 | 4,126,849 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,196 |
| 150 | wellhead engine | 145 | 262,158 | 4,123,898 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,337 |
| 151 | wellhead engine | 147 | 286,812 | 4,115,908 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,196 |
| 152 | wellhead engine | 149 | 284,366 | 4,114,083 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 8,016 |
| 153 | wellhead engine | 151 | 281,992 | 4,115,032 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 8,597 |
| 154 | wellhead engine | 153 | 286,782 | 4,118,241 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,413 |
| 155 | wellhead engine | 155 | 284,120 | 4,118,309 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 8,085 |
| 156 | wellhead engine | 157 | 282,132 | 4,120,470 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 8,797 |
| 157 | wellhead engine | 159 | 288,280 | 4,114,206 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 6,737 |
| 158 | wellhead engine | 161 | 285,790 | 4,114,158 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,196 |
| 159 | wellhead engine | 163 | 282,619 | 4,115,238 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 8,252 |
| 160 | wellhead engine | 165 | 264,731 | 4,130,156 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,692 |
| 161 | wellhead engine | 167 | 273,402 | 4,126,031 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,196 |
| 162 | wellhead engine | 169 | 273,955 | 4,113,578 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 6,796 |
| 163 | wellhead engine | 171 | 281,694 | 4,117,261 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 8,597 |
| 164 | wellhead engine | 173 | 260,723 | 4,129,603 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,797 |
| 165 | wellhead engine | 175 | 271,851 | 4,127,738 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,469 |
| 166 | wellhead engine | 180 | 289,976 | 4,118,050 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 6,996 |
| 167 | wellhead engine | 182 | 272,626 | 4,123,608 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,052 |
| 168 | wellhead engine | 184 | 281,321 | 4,123,378 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 8,226 |
| 169 | wellhead engine | 188 | 279,846 | 4,128,080 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,800 |
| 170 | wellhead engine | 190 | 281,249 | 4,124,046 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 8,397 |
| 171 | wellhead engine | 194 | 285,007 | 4,121,729 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,596 |
| 172 | wellhead engine | 197 | 296,270 | 4,113,898 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,196 |
| 173 | wellhead engine | 199 | 283,718 | 4,123,427 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,596 |
| 174 | wellhead engine | 201 | 285,948 | 4,120,372 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,649 |
| 175 | wellhead engine | 203 | 288,433 | 4,120,309 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,311 |

⁽¹⁾ 0.0017584 g/s HAP emission

Table A-34. Near Field Modeling Input Values (Alternative 1) (continued)

| Source Count | Source Description | Unit ID | UTM | | Emission Rate | | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|--------------------|---------|-------------|--------------|---------------|----------|-----------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | Easting (m) | Northing (m) | NOx (g/s) | CO (g/s) | HAP (g/s) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 176 | wellhead engine | 206 | 281,439 | 4,127,927 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,800 |
| 177 | wellhead engine | 209 | 282,966 | 4,121,781 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,997 |
| 178 | wellhead engine | 211 | 289,873 | 4,113,944 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 6,596 |
| 179 | wellhead engine | 212 | 283,386 | 4,124,324 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,764 |
| 180 | wellhead engine | 214 | 285,422 | 4,120,608 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 8,059 |
| 181 | wellhead engine | 216 | 288,435 | 4,116,867 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,196 |
| 182 | wellhead engine | 218 | 295,549 | 4,113,471 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,196 |
| 183 | wellhead engine | 220 | 273,443 | 4,124,253 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,104 |
| 184 | wellhead engine | 222 | 283,412 | 4,121,880 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,997 |
| 185 | wellhead engine | 224 | 290,652 | 4,116,701 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 6,796 |
| 186 | wellhead engine | 226 | 264,640 | 4,126,938 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,596 |
| 187 | wellhead engine | 228 | 282,056 | 4,124,358 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 8,210 |
| 188 | wellhead engine | 231 | 277,363 | 4,128,146 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,396 |
| 189 | wellhead engine | 233 | 287,211 | 4,114,122 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,000 |
| 190 | wellhead engine | 235 | 260,454 | 4,123,279 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,196 |
| 191 | wellhead engine | 238 | 296,251 | 4,113,122 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,196 |
| 192 | wellhead engine | 240 | 263,008 | 4,131,981 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,997 |
| 193 | wellhead engine | 241 | 281,705 | 4,114,262 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 8,397 |
| 194 | wellhead engine | 243 | 260,634 | 4,126,495 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,396 |
| 195 | wellhead engine | 245 | 259,497 | 4,123,973 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,186 |
| 196 | wellhead engine | 247 | 281,627 | 4,124,924 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 8,157 |
| 197 | wellhead engine | 250 | 282,909 | 4,123,004 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,718 |
| 198 | wellhead engine | 252 | 284,534 | 4,120,630 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 8,059 |
| 199 | wellhead engine | 254 | 263,091 | 4,128,647 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,997 |
| 200 | wellhead engine | 256 | 289,512 | 4,117,284 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 6,996 |
| 201 | wellhead engine | 258 | 286,690 | 4,121,575 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,396 |
| 202 | wellhead engine | 260 | 282,009 | 4,119,140 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 8,797 |
| 203 | wellhead engine | 262 | 285,362 | 4,118,277 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 8,397 |
| 204 | wellhead engine | 264 | 286,075 | 4,118,370 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,997 |
| 205 | wellhead engine | 266 | 287,451 | 4,116,559 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,275 |
| 206 | wellhead engine | 268 | 283,997 | 4,113,537 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 8,016 |
| 207 | wellhead engine | 269 | 284,423 | 4,119,744 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 8,797 |
| 208 | wellhead engine | 271 | 283,606 | 4,122,542 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,728 |
| 209 | wellhead engine | 273 | 274,998 | 4,125,988 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,196 |
| 210 | wellhead engine | 275 | 268,658 | 4,127,826 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,127 |

⁽¹⁾ 0.0017584 g/s HAP emission

Table A-34. Near Field Modeling Input Values (Alternative 1) (continued)

| Source Count | Source Description | Unit ID | UTM | | Emission Rate | | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|--------------------|---------|-------------|--------------|---------------|----------|-----------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | Easting (m) | Northing (m) | NOx (g/s) | CO (g/s) | HAP (g/s) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 211 | wellhead engine | 277 | 284,323 | 4,115,860 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,738 |
| 212 | wellhead engine | 279 | 276,353 | 4,116,846 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,482 |
| 213 | wellhead engine | 281 | 276,086 | 4,113,522 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 6,993 |
| 214 | wellhead engine | 283 | 277,161 | 4,113,826 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,544 |
| 215 | wellhead engine | 285 | 285,418 | 4,113,501 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,537 |
| 216 | wellhead engine | 287 | 253,338 | 4,128,927 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,396 |
| 217 | wellhead engine | 289 | 262,961 | 4,130,317 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,800 |
| 218 | wellhead engine | 291 | 262,870 | 4,127,098 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,659 |
| 219 | wellhead engine | 293 | 254,268 | 4,127,345 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,127 |
| 220 | wellhead engine | 295 | 267,216 | 4,130,197 | 0.13 | 0.11 | (1) | 1.524 | 477 | 3.8 | 0.2 | 1.0668 | 1.0668 | 7,521 |

⁽¹⁾ 0.0017584 g/s HAP emission

Table A-35. Near Field Modeling Input Values (Alternative 2)

| Source Count | Source Description | Unit ID | UTM | | Emission Rate | | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|--------------------|----------|-------------|--------------|---------------|----------|-----------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | Easting (m) | Northing (m) | NOx (g/s) | CO (g/s) | HAP (g/s) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 1 | Elmridge 1 | ELM1A | 288,301 | 4,112,688 | 0.521 | 0.694 | 0.08 | 6.60 | 644 | 17.3 | 0.46 | 3.9 | 3.9 | 6,399 |
| 2 | Elmridge 1 | ELM1B | 288,301 | 4,112,698 | 0.521 | 0.694 | 0.08 | 6.60 | 644 | 17.3 | 0.46 | 3.9 | 3.9 | 6,399 |
| 3 | Elmridge 1 | ELM1C | 288,301 | 4,112,708 | 0.521 | 0.694 | 0.08 | 6.60 | 644 | 17.3 | 0.46 | 3.9 | 3.9 | 6,399 |
| 4 | Elmridge 1 | ELM1D | 288,301 | 4,112,718 | 0.521 | 0.694 | 0.08 | 6.60 | 644 | 17.3 | 0.46 | 3.9 | 3.9 | 6,399 |
| 5 | Elmridge 1 | ELM1DEHY | 288,301 | 4,112,728 | 0.126 | 0.106 | 0.00 | 3.50 | 533 | 6.4 | 0.15 | 2.3 | 2.3 | 6,399 |
| 6 | Elmridge 1 | ELM1SEP | 288,301 | 4,112,738 | 0.089 | 0.150 | 0.00 | 3.50 | 533 | 6.4 | 0.15 | 2.3 | 2.3 | 6,399 |
| 7 | Elmridge 2 | ELM2A | 274,470 | 4,114,300 | 0.625 | 0.833 | 0.10 | 9.50 | 644 | 29.2 | 0.38 | 5.9 | 5.9 | 6,996 |
| 8 | Elmridge 2 | ELM2B | 274,470 | 4,114,310 | 0.625 | 0.833 | 0.10 | 9.50 | 644 | 29.2 | 0.38 | 5.9 | 5.9 | 6,996 |
| 9 | Elmridge 2 | ELM2C | 274,470 | 4,114,320 | 0.625 | 0.833 | 0.10 | 9.50 | 644 | 29.2 | 0.38 | 5.9 | 5.9 | 6,996 |
| 10 | Elmridge 2 | ELM2D | 274,470 | 4,114,330 | 0.625 | 0.833 | 0.10 | 9.50 | 644 | 29.2 | 0.38 | 5.9 | 5.9 | 6,996 |
| 11 | Elmridge 2 | ELM2E | 274,470 | 4,114,340 | 0.625 | 0.833 | 0.10 | 9.50 | 644 | 29.2 | 0.38 | 5.9 | 5.9 | 6,996 |
| 12 | Elmridge 2 | ELM2F | 274,470 | 4,114,350 | 0.625 | 0.833 | 0.10 | 9.50 | 644 | 29.2 | 0.38 | 5.9 | 5.9 | 6,996 |
| 13 | Elmridge 2 | ELM2G | 274,470 | 4,114,360 | 0.625 | 0.833 | 0.10 | 9.50 | 644 | 29.2 | 0.38 | 5.9 | 5.9 | 6,996 |
| 14 | Elmridge 2 | ELM2H | 274,470 | 4,114,370 | 0.625 | 0.833 | 0.10 | 9.50 | 644 | 29.2 | 0.38 | 5.9 | 5.9 | 6,996 |
| 15 | Elmridge 2 | ELM2I | 274,470 | 4,114,380 | 0.625 | 0.833 | 0.10 | 9.50 | 644 | 29.2 | 0.38 | 5.9 | 5.9 | 6,996 |
| 16 | Elmridge 2 | ELM2DEHY | 274,470 | 4,114,270 | 0.126 | 0.106 | 0.00 | 3.50 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 6,996 |
| 17 | Elmridge 2 | ELM2SEP | 274,470 | 4,114,280 | 0.110 | 0.360 | 0.00 | 3.50 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 6,996 |
| 18 | Elmridge 2 | ELM2SEPa | 274,470 | 4,114,290 | 0.110 | 0.360 | 0.00 | 3.50 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 6,996 |
| 19 | PETROX 1 | PET1 | 292,405 | 4,113,912 | 0.258 | 0.344 | 0.04 | 3.05 | 644 | 24.1 | 0.3 | 2.0 | 2.0 | 6,396 |
| 20 | PETROX 1 | PET1DEH | 292,405 | 4,113,922 | 0.126 | 0.106 | 0.00 | 3.00 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 6,396 |
| 21 | PETROX 1 | PET1SEP | 292,405 | 4,113,932 | 0.022 | 0.019 | 0.00 | 3.00 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 6,396 |
| 22 | PETROX 2 | PET2 | 286,151 | 4,120,460 | 0.792 | 1.056 | 0.12 | 9.10 | 644 | 26.3 | 0.46 | 4.9 | 4.9 | 7,613 |
| 23 | PETROX 2 | PET2DEH | 286,151 | 4,120,470 | 0.126 | 0.106 | 0.00 | 3.10 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 7,613 |
| 24 | PETROX 2 | PET2SEP | 286,151 | 4,120,480 | 0.034 | 0.057 | 0.00 | 3.10 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 7,613 |
| 25 | PETROX 2 | PET2SEPa | 286,151 | 4,120,450 | 0.034 | 0.057 | 0.00 | 3.10 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 7,613 |
| 25 | BP AMOCO 1 | BP1A | 273,670 | 4,124,111 | 0.556 | 0.741 | 0.09 | 4.60 | 644 | 18.4 | 0.46 | 3.0 | 3.0 | 7,141 |
| 26 | BP AMOCO 1 | BP1B | 273,670 | 4,124,121 | 0.556 | 0.741 | 0.09 | 4.60 | 644 | 18.4 | 0.46 | 3.0 | 3.0 | 7,141 |
| 27 | BP AMOCO 1 | BP1C | 273,670 | 4,124,131 | 0.556 | 0.741 | 0.09 | 4.60 | 644 | 18.4 | 0.46 | 3.0 | 3.0 | 7,141 |
| 28 | BP AMOCO 1 | BP1DEH | 273,670 | 4,124,141 | 0.126 | 0.106 | 0.00 | 3.00 | 533 | 6.4 | 0.15 | 2.0 | 2.0 | 7,141 |
| 29 | BP AMOCO 1 | BP1SEP | 273,670 | 4,124,151 | 0.143 | 0.120 | 0.00 | 3.00 | 533 | 6.4 | 0.15 | 2.0 | 2.0 | 7,141 |
| 30 | BP AMOCO 2 | BP2A | 275,030 | 4,114,050 | 0.625 | 0.833 | 0.10 | 4.60 | 644 | 29.9 | 0.38 | 3.0 | 3.0 | 6,799 |
| 31 | BP AMOCO 2 | BP2B | 275,030 | 4,114,060 | 0.625 | 0.833 | 0.10 | 4.60 | 644 | 29.9 | 0.38 | 3.0 | 3.0 | 6,799 |
| 32 | BP AMOCO 2 | BP2DEH | 275,030 | 4,114,070 | 0.126 | 0.106 | 0.00 | 3.00 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 6,799 |
| 33 | BP AMOCO 2 | BP2SEP | 275,030 | 4,114,080 | 0.107 | 0.090 | 0.00 | 3.00 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 6,799 |
| 34 | PETROX 3 | PET3 | 283,100 | 4,123,180 | 0.258 | 0.344 | 0.04 | 3.05 | 644 | 24.1 | 0.3 | 2.0 | 2.0 | 7,616 |
| 35 | PETROX 3 | PET3DEH | 283,100 | 4,123,190 | 0.126 | 0.106 | 0.00 | 3.00 | 533 | 6.4 | 0.1524 | 2.0 | 2.0 | 7,616 |

Table A-35. Near Field Modeling Input Values (Alternative 2) (continued)

| Source Count | Source Description | Unit ID | UTM | | Emission Rate | | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|--------------------|---------|-------------|--------------|---------------|----------|-----------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | Easting (m) | Northing (m) | NOx (g/s) | CO (g/s) | HAP (g/s) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 36 | PETROX 3 | PET3SEP | 283,100 | 4,123,200 | 0.022 | 0.019 | 0.00 | 3.00 | 533 | 6.4 | 0.1524 | 2.0 | 2.0 | 7,616 |
| 37 | PETROX 4 | PET4 | 281,500 | 4,123,161 | 0.258 | 0.344 | 0.04 | 3.05 | 644 | 24.1 | 0.3 | 2.0 | 2.0 | 8,197 |
| 38 | PETROX 4 | PET4DEH | 281,500 | 4,123,171 | 0.126 | 0.106 | 0.00 | 3.00 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 8,197 |
| 39 | PETROX 4 | PET4SEP | 281,500 | 4,123,181 | 0.022 | 0.019 | 0.00 | 3.00 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 8,197 |
| 40 | PURE 1 | PUR1 | 251,600 | 4,125,830 | 0.625 | 0.833 | 0.10 | 4.60 | 644 | 29.9 | 0.38 | 3.0 | 3.0 | 7,036 |
| 41 | PURE 1 | PUR1DEH | 251,600 | 4,125,840 | 0.126 | 0.106 | 0.00 | 3.00 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 7,036 |
| 42 | PURE 1 | PUR1SEP | 251,600 | 4,125,850 | 0.054 | 0.045 | 0.00 | 3.00 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 7,036 |
| 43 | PURE 2 | PUR2 | 249,350 | 4,125,160 | 0.100 | 0.133 | 0.02 | 3.00 | 583 | 21.5 | 0.18 | 2.0 | 2.0 | 6,803 |
| 44 | PURE 2 | PUR2DEH | 249,350 | 4,125,170 | 0.126 | 0.106 | 0.00 | 3.00 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 6,803 |
| 45 | PURE 2 | PUR2SEP | 249,350 | 4,125,180 | 0.009 | 0.007 | 0.00 | 3.00 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 6,803 |
| 46 | BP 3 | BP3A | 272,164 | 4,126,575 | 0.625 | 0.833 | 0.10 | 4.60 | 644 | 29.9 | 0.38 | 3.0 | 3.0 | 6,996 |
| 47 | BP 3 | BP3B | 272,164 | 4,126,585 | 0.625 | 0.833 | 0.10 | 4.60 | 644 | 29.9 | 0.38 | 3.0 | 3.0 | 6,996 |
| 48 | BP 3 | BP3DEH | 272,164 | 4,126,595 | 0.126 | 0.106 | 0.00 | 3.00 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 6,996 |
| 49 | BP 3 | BP3SEP | 272,164 | 4,126,605 | 0.107 | 0.090 | 0.00 | 3.00 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 6,996 |
| 50 | BP 4 | BP4A | 259,000 | 4,124,000 | 0.556 | 0.741 | 0.09 | 4.60 | 644 | 18.4 | 0.46 | 3.0 | 3.0 | 7082.0 |
| 51 | BP 4 | BP4B | 259,000 | 4,124,010 | 0.556 | 0.741 | 0.09 | 4.60 | 644 | 18.4 | 0.46 | 3.0 | 3.0 | 7082.0 |
| 52 | BP 4 | BP4C | 259,000 | 4,124,020 | 0.556 | 0.741 | 0.09 | 4.60 | 644 | 18.4 | 0.46 | 3.0 | 3.0 | 7082.0 |
| 53 | BP 4 | BP4DEH | 259,000 | 4,124,030 | 0.126 | 0.106 | 0.00 | 3.00 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 7082.0 |
| 54 | BP 4 | BP4SEP | 259,000 | 4,124,040 | 0.143 | 0.120 | 0.00 | 3.00 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 7082.0 |
| 55 | Cross Timbers | HUB1 | 257,000 | 4,125,000 | 0.521 | 0.694 | 0.08 | 4.60 | 644.0 | 17.3 | 0.5 | 3.0 | 3.0 | 6,934 |
| 56 | Cross Timbers | HUB2 | 257,000 | 4,125,010 | 0.521 | 0.694 | 0.08 | 4.60 | 644.0 | 17.3 | 0.5 | 3.0 | 3.0 | 6,934 |
| 57 | Cross Timbers | HUBDEH | 257,000 | 4,125,020 | 0.126 | 0.106 | 0.00 | 3.00 | 533.0 | 6.4 | 0.2 | 2.0 | 2.0 | 6,934 |
| 58 | Cross Timbers | HUBSEP | 257,000 | 4,125,030 | 0.089 | 0.075 | 0.00 | 3.00 | 533.0 | 6.4 | 0.2 | 2.0 | 2.0 | 6,934 |
| 59 | Independent 1 | IP1 | 277,120 | 4,115,417 | 0.417 | 0.556 | 0.06 | 3.05 | 644 | 24.8 | 0.3 | 2.0 | 2.0 | 7,514 |
| 60 | Independent 1 | IP1DEH | 277,120 | 4,115,427 | 0.126 | 0.106 | 0.00 | 3.00 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 7,514 |
| 61 | Independent 1 | IP1SEP | 277,120 | 4,115,437 | 0.036 | 0.030 | 0.00 | 3.00 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 7,514 |
| 62 | Independent 2 | IP2A | 275,600 | 4,120,800 | 0.833 | 1.111 | 0.13 | 7.50 | 644 | 25.3 | 0.46 | 4.9 | 4.9 | 7,196 |
| 63 | Independent 2 | IP2DEH | 275,600 | 4,120,810 | 0.126 | 0.106 | 0.00 | 3.00 | 533 | 6.4 | 0.15 | 2.0 | 2.0 | 7,196 |
| 64 | Independent 2 | IP2SEP | 275,600 | 4,120,820 | 0.071 | 0.060 | 0.00 | 3.00 | 533 | 6.4 | 0.15 | 2.0 | 2.0 | 7,196 |
| 65 | Independent 3 | IP3A | 276,435 | 4,116,788 | 0.833 | 1.111 | 0.13 | 7.50 | 644 | 25.3 | 0.46 | 4.9 | 4.9 | 7,426 |
| 66 | Independent 3 | IP3DEH | 276,435 | 4,116,778 | 0.126 | 0.106 | 0.00 | 3.00 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 7,426 |
| 67 | Independent 3 | IP3SEP | 276,435 | 4,116,778 | 0.071 | 0.060 | 0.00 | 3.00 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 7,426 |
| 68 | Bayfield | BAY1 | 271,500 | 4,125,000 | 0.833 | 1.111 | 0.13 | 7.50 | 644 | 28.6 | 0.5 | 4.9 | 4.9 | 6,996 |
| 69 | Bayfield | BAYDEH | 271,500 | 4,125,010 | 0.126 | 0.106 | 0.00 | 3.00 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 6,996 |
| 70 | Bayfield | BAYSEP | 271,500 | 4,125,020 | 0.071 | 0.060 | 0.00 | 3.00 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 6,996 |

Table A-35. Near Field Modeling Input Values (Alternative 2) (continued)

| Source Count | Source Description | Unit ID | UTM | | Emission Rate | | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|--------------------|---------|-------------|--------------|---------------|----------|-----------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | Easting (m) | Northing (m) | NOx (g/s) | CO (g/s) | HAP (g/s) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 71 | Huber engine | 5 | 263,008 | 4,131,981 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,970 |
| 72 | Huber engine | 13 | 259,133 | 4,129,870 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,498 |
| 73 | Huber engine | 296 | 263,091 | 4,128,647 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,797 |
| 74 | Huber engine | 347 | 264,640 | 4,126,938 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,478 |
| 75 | Huber engine | 359 | 271,025 | 4,126,761 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,196 |
| 76 | Huber engine | 380 | 270,212 | 4,126,228 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,291 |
| 77 | Huber engine | 1 | 266,019 | 4,125,455 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,377 |
| 78 | Huber engine | 2 | 260,454 | 4,123,279 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,157 |
| 79 | Huber engine | 174 | 258,942 | 4,123,212 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6,996 |
| 80 | Huber engine | 175 | 284,474 | 4,121,742 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,544 |
| 81 | Huber engine | 176 | 289,873 | 4,113,944 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6,586 |
| 82 | Huber engine | 213 | 289,820 | 4,115,389 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6,796 |
| 83 | Huber engine | 214 | 290,652 | 4,116,701 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6,609 |
| 84 | Huber engine | 217 | 289,953 | 4,117,162 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6,796 |
| 85 | Huber engine | 228 | 289,190 | 4,118,625 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6,996 |
| 86 | Huber engine | 230 | 289,976 | 4,118,050 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6,396 |
| 87 | Huber engine | 241 | 292,360 | 4,113,882 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6,396 |
| 88 | Huber engine | 249 | 293,869 | 4,113,846 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6,996 |
| 89 | Huber engine | 266 | 293,409 | 4,113,191 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6,862 |
| 90 | Huber engine | 267 | 294,938 | 4,113,931 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6,790 |
| 91 | Huber engine | 275 | 295,549 | 4,113,471 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6,790 |
| 92 | Huber engine | 292 | 296,251 | 4,113,122 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,528 |
| 93 | wellhead engine | 3 | 279,846 | 4,128,080 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,800 |
| 94 | wellhead engine | 6 | 280,629 | 4,127,505 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,800 |
| 95 | wellhead engine | 8 | 281,439 | 4,127,927 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,800 |
| 96 | wellhead engine | 10 | 281,384 | 4,125,819 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,397 |
| 97 | wellhead engine | 12 | 282,276 | 4,126,018 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,256 |
| 98 | wellhead engine | 15 | 274,918 | 4,122,991 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,196 |
| 99 | wellhead engine | 17 | 274,862 | 4,124,214 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,196 |
| 100 | wellhead engine | 19 | 273,443 | 4,124,253 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,104 |
| 101 | wellhead engine | 21 | 272,626 | 4,123,608 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,052 |
| 102 | wellhead engine | 23 | 277,363 | 4,128,146 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,396 |
| 103 | wellhead engine | 25 | 276,595 | 4,125,945 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,446 |
| 104 | wellhead engine | 27 | 280,560 | 4,124,841 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,728 |
| 105 | wellhead engine | 29 | 282,056 | 4,124,358 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,210 |

Table A-35. Near Field Modeling Input Values (Alternative 2) (continued)

| Source Count | Source Description | Unit ID | UTM | | Emission Rate | | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|--------------------|---------|-------------|--------------|---------------|----------|-----------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | Easting (m) | Northing (m) | NOx (g/s) | CO (g/s) | HAP (g/s) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 106 | wellhead engine | 31 | 281,321 | 4,123,378 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,226 |
| 107 | wellhead engine | 33 | 282,013 | 4,122,694 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,125 |
| 108 | wellhead engine | 35 | 282,946 | 4,124,446 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,764 |
| 109 | wellhead engine | 37 | 283,718 | 4,123,427 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,596 |
| 110 | wellhead engine | 39 | 282,909 | 4,123,004 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,718 |
| 111 | wellhead engine | 41 | 282,966 | 4,121,781 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,997 |
| 112 | wellhead engine | 43 | 285,118 | 4,122,614 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,596 |
| 113 | wellhead engine | 45 | 285,894 | 4,121,706 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,410 |
| 114 | wellhead engine | 47 | 283,641 | 4,120,431 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,797 |
| 115 | wellhead engine | 49 | 285,422 | 4,120,608 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,059 |
| 116 | wellhead engine | 51 | 285,845 | 4,119,819 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,354 |
| 117 | wellhead engine | 53 | 287,640 | 4,120,551 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,328 |
| 118 | wellhead engine | 55 | 286,911 | 4,119,793 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,580 |
| 119 | wellhead engine | 57 | 288,433 | 4,120,309 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,311 |
| 120 | wellhead engine | 59 | 288,383 | 4,118,312 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,209 |
| 121 | wellhead engine | 61 | 287,676 | 4,118,441 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,209 |
| 122 | wellhead engine | 63 | 286,802 | 4,119,018 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,436 |
| 123 | wellhead engine | 65 | 286,075 | 4,118,370 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,997 |
| 124 | wellhead engine | 67 | 285,382 | 4,119,054 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,640 |
| 125 | wellhead engine | 69 | 286,749 | 4,116,909 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,275 |
| 126 | wellhead engine | 71 | 287,554 | 4,117,111 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,196 |
| 127 | wellhead engine | 73 | 288,435 | 4,116,867 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,196 |
| 128 | wellhead engine | 75 | 284,120 | 4,118,309 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,085 |
| 129 | wellhead engine | 77 | 282,565 | 4,120,014 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,597 |
| 130 | wellhead engine | 79 | 282,001 | 4,118,808 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,797 |
| 131 | wellhead engine | 81 | 281,210 | 4,115,719 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,584 |
| 132 | wellhead engine | 83 | 281,705 | 4,114,262 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,397 |
| 133 | wellhead engine | 85 | 283,467 | 4,113,662 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,075 |
| 134 | wellhead engine | 87 | 284,366 | 4,114,083 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,016 |
| 135 | wellhead engine | 89 | 285,349 | 4,114,280 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,537 |
| 136 | wellhead engine | 91 | 286,576 | 4,113,583 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,000 |
| 137 | wellhead engine | 93 | 287,211 | 4,114,122 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,000 |
| 138 | wellhead engine | 95 | 288,299 | 4,114,983 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6,911 |
| 139 | wellhead engine | 97 | 287,500 | 4,115,003 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6,911 |
| 140 | wellhead engine | 99 | 287,431 | 4,115,782 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,196 |

Table A-35. Near Field Modeling Input Values (Alternative 2) (continued)

| Source Count | Source Description | Unit ID | UTM | | Emission Rate | | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|--------------------|---------|-------------|--------------|---------------|----------|-----------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | Easting (m) | Northing (m) | NOx (g/s) | CO (g/s) | HAP (g/s) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 141 | wellhead engine | 101 | 285,039 | 4,116,065 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,797 |
| 142 | wellhead engine | 103 | 285,907 | 4,115,265 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,196 |
| 143 | wellhead engine | 105 | 284,323 | 4,115,860 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,738 |
| 144 | wellhead engine | 107 | 284,011 | 4,117,534 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,085 |
| 145 | wellhead engine | 109 | 285,941 | 4,116,597 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,816 |
| 146 | wellhead engine | 111 | 277,161 | 4,113,826 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,544 |
| 147 | wellhead engine | 113 | 276,086 | 4,113,522 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6,993 |
| 148 | wellhead engine | 115 | 275,488 | 4,114,425 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6,875 |
| 149 | wellhead engine | 117 | 273,982 | 4,114,577 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6,996 |
| 150 | wellhead engine | 119 | 274,798 | 4,115,221 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6,996 |
| 151 | wellhead engine | 121 | 274,816 | 4,115,887 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,196 |
| 152 | wellhead engine | 123 | 276,507 | 4,115,953 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,895 |
| 153 | wellhead engine | 125 | 276,353 | 4,116,846 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,482 |
| 154 | wellhead engine | 127 | 260,818 | 4,132,932 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,164 |
| 155 | wellhead engine | 129 | 261,438 | 4,132,914 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,164 |
| 156 | wellhead engine | 131 | 263,119 | 4,132,755 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,941 |
| 157 | wellhead engine | 133 | 264,714 | 4,132,711 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,997 |
| 158 | wellhead engine | 135 | 256,623 | 4,132,053 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,079 |
| 159 | wellhead engine | 137 | 258,219 | 4,132,006 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,062 |
| 160 | wellhead engine | 139 | 259,194 | 4,131,979 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,770 |
| 161 | wellhead engine | 141 | 259,814 | 4,131,961 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,797 |
| 162 | wellhead engine | 143 | 260,793 | 4,132,044 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,875 |
| 163 | wellhead engine | 145 | 264,689 | 4,131,823 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,777 |
| 164 | wellhead engine | 147 | 266,192 | 4,131,670 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,997 |
| 165 | wellhead engine | 149 | 254,920 | 4,131,436 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,997 |
| 166 | wellhead engine | 151 | 256,604 | 4,131,387 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,600 |
| 167 | wellhead engine | 153 | 258,200 | 4,131,341 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,596 |
| 168 | wellhead engine | 155 | 254,388 | 4,131,451 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,997 |
| 169 | wellhead engine | 157 | 264,670 | 4,131,157 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,626 |
| 170 | wellhead engine | 159 | 265,645 | 4,131,130 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,596 |
| 171 | wellhead engine | 161 | 261,302 | 4,131,252 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,964 |
| 172 | wellhead engine | 163 | 267,149 | 4,130,977 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,583 |
| 173 | wellhead engine | 165 | 272,024 | 4,130,843 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,997 |
| 174 | wellhead engine | 167 | 273,619 | 4,130,800 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,997 |
| 175 | wellhead engine | 169 | 272,644 | 4,130,826 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,997 |

Table A-35. Near Field Modeling Input Values (Alternative 2) (continued)

| Source Count | Source Description | Unit ID | UTM | | Emission Rate | | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|--------------------|---------|-------------|--------------|---------------|----------|-----------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | Easting (m) | Northing (m) | NOx (g/s) | CO (g/s) | HAP (g/s) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 176 | wellhead engine | 171 | 275,835 | 4,130,741 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,029 |
| 177 | wellhead engine | 173 | 276,811 | 4,130,714 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,902 |
| 178 | wellhead engine | 178 | 277,431 | 4,130,698 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,902 |
| 179 | wellhead engine | 180 | 278,406 | 4,130,672 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,783 |
| 180 | wellhead engine | 182 | 252,675 | 4,130,502 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,544 |
| 181 | wellhead engine | 184 | 254,270 | 4,130,455 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,997 |
| 182 | wellhead engine | 186 | 254,980 | 4,130,435 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,826 |
| 183 | wellhead engine | 188 | 255,958 | 4,130,517 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,997 |
| 184 | wellhead engine | 190 | 258,263 | 4,130,450 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,574 |
| 185 | wellhead engine | 192 | 259,681 | 4,130,410 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,629 |
| 186 | wellhead engine | 194 | 264,731 | 4,130,156 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,692 |
| 187 | wellhead engine | 196 | 267,216 | 4,130,197 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,521 |
| 188 | wellhead engine | 198 | 251,680 | 4,129,865 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,314 |
| 189 | wellhead engine | 200 | 252,658 | 4,129,947 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,715 |
| 190 | wellhead engine | 202 | 254,254 | 4,129,901 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,439 |
| 191 | wellhead engine | 204 | 270,404 | 4,129,999 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,593 |
| 192 | wellhead engine | 205 | 254,963 | 4,129,880 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,492 |
| 193 | wellhead engine | 207 | 271,908 | 4,129,847 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,797 |
| 194 | wellhead engine | 209 | 273,504 | 4,129,804 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,505 |
| 195 | wellhead engine | 211 | 275,191 | 4,129,869 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,387 |
| 196 | wellhead engine | 215 | 275,723 | 4,129,855 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,400 |
| 197 | wellhead engine | 218 | 251,148 | 4,129,881 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,997 |
| 198 | wellhead engine | 220 | 257,531 | 4,129,694 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,383 |
| 199 | wellhead engine | 222 | 279,003 | 4,129,768 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,649 |
| 200 | wellhead engine | 224 | 278,379 | 4,129,673 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,482 |
| 201 | wellhead engine | 226 | 255,935 | 4,129,740 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,636 |
| 202 | wellhead engine | 229 | 265,513 | 4,129,579 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,797 |
| 203 | wellhead engine | 232 | 260,723 | 4,129,603 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,564 |
| 204 | wellhead engine | 234 | 269,499 | 4,129,358 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,177 |
| 205 | wellhead engine | 236 | 276,769 | 4,129,161 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,396 |
| 206 | wellhead engine | 237 | 278,986 | 4,129,103 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,449 |
| 207 | wellhead engine | 239 | 279,960 | 4,129,077 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,593 |
| 208 | wellhead engine | 242 | 281,468 | 4,129,038 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,780 |
| 209 | wellhead engine | 244 | 250,143 | 4,128,911 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,187 |
| 210 | wellhead engine | 246 | 251,742 | 4,128,975 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,229 |

Table A-35. Near Field Modeling Input Values (Alternative 2) (continued)

| Source Count | Source Description | Unit ID | UTM | | Emission Rate | | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|--------------------|---------|-------------|--------------|---------------|----------|-----------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | Easting (m) | Northing (m) | NOx (g/s) | CO (g/s) | HAP (g/s) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 211 | wellhead engine | 248 | 252,626 | 4,128,838 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,396 |
| 212 | wellhead engine | 251 | 253,338 | 4,128,927 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,272 |
| 213 | wellhead engine | 253 | 254,934 | 4,128,881 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,311 |
| 214 | wellhead engine | 255 | 255,913 | 4,128,964 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,400 |
| 215 | wellhead engine | 257 | 250,038 | 4,128,359 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,416 |
| 216 | wellhead engine | 259 | 269,472 | 4,128,359 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,127 |
| 217 | wellhead engine | 261 | 251,722 | 4,128,309 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,170 |
| 218 | wellhead engine | 263 | 254,120 | 4,128,349 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,196 |
| 219 | wellhead engine | 265 | 278,959 | 4,128,104 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,600 |
| 220 | wellhead engine | 268 | 255,890 | 4,128,187 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,219 |
| 221 | wellhead engine | 270 | 268,658 | 4,127,826 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,127 |
| 222 | wellhead engine | 272 | 271,851 | 4,127,738 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,469 |
| 223 | wellhead engine | 274 | 278,321 | 4,127,454 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,701 |
| 224 | wellhead engine | 277 | 283,023 | 4,127,443 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,128 |
| 225 | wellhead engine | 279 | 249,388 | 4,127,378 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,396 |
| 226 | wellhead engine | 281 | 283,466 | 4,127,431 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,128 |
| 227 | wellhead engine | 283 | 254,268 | 4,127,345 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,052 |
| 228 | wellhead engine | 285 | 259,589 | 4,127,192 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,446 |
| 229 | wellhead engine | 287 | 263,842 | 4,126,960 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,744 |
| 230 | wellhead engine | 289 | 249,371 | 4,126,823 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,396 |
| 231 | wellhead engine | 291 | 269,426 | 4,126,693 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,154 |
| 232 | wellhead engine | 294 | 274,215 | 4,126,564 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,196 |
| 233 | wellhead engine | 297 | 283,089 | 4,126,552 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,128 |
| 234 | wellhead engine | 299 | 283,709 | 4,126,536 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,197 |
| 235 | wellhead engine | 301 | 279,890 | 4,126,413 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,230 |
| 236 | wellhead engine | 303 | 257,438 | 4,126,476 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,091 |
| 237 | wellhead engine | 305 | 262,227 | 4,126,339 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,396 |
| 238 | wellhead engine | 307 | 273,402 | 4,126,031 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,196 |
| 239 | wellhead engine | 309 | 283,695 | 4,125,982 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,026 |
| 240 | wellhead engine | 311 | 278,901 | 4,125,884 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,197 |
| 241 | wellhead engine | 313 | 280,497 | 4,125,842 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,230 |
| 242 | wellhead engine | 315 | 247,833 | 4,125,870 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,275 |
| 243 | wellhead engine | 317 | 251,561 | 4,125,870 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,045 |
| 244 | wellhead engine | 319 | 261,315 | 4,125,476 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,206 |
| 245 | wellhead engine | 321 | 264,505 | 4,125,275 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,239 |

Table A-35. Near Field Modeling Input Values (Alternative 2) (continued)

| Source Count | Source Description | Unit ID | UTM | | Emission Rate | | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|--------------------|---------|-------------|--------------|---------------|----------|-----------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | Easting (m) | Northing (m) | NOx (g/s) | CO (g/s) | HAP (g/s) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 246 | wellhead engine | 323 | 269,384 | 4,125,140 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,045 |
| 247 | wellhead engine | 325 | 282,073 | 4,125,024 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,157 |
| 248 | wellhead engine | 327 | 258,904 | 4,124,990 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,196 |
| 249 | wellhead engine | 329 | 260,501 | 4,124,944 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,206 |
| 250 | wellhead engine | 331 | 248,253 | 4,125,080 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6,996 |
| 251 | wellhead engine | 333 | 246,738 | 4,124,903 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6,996 |
| 252 | wellhead engine | 335 | 278,875 | 4,124,885 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,256 |
| 253 | wellhead engine | 337 | 279,850 | 4,124,860 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,459 |
| 254 | wellhead engine | 339 | 266,885 | 4,124,654 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,396 |
| 255 | wellhead engine | 341 | 262,712 | 4,124,660 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,396 |
| 256 | wellhead engine | 343 | 265,462 | 4,124,583 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,239 |
| 257 | wellhead engine | 345 | 246,186 | 4,124,253 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6,796 |
| 258 | wellhead engine | 348 | 279,832 | 4,124,194 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,426 |
| 259 | wellhead engine | 350 | 280,454 | 4,124,178 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,426 |
| 260 | wellhead engine | 352 | 250,980 | 4,124,221 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6,996 |
| 261 | wellhead engine | 354 | 257,985 | 4,123,905 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,180 |
| 262 | wellhead engine | 356 | 261,268 | 4,123,811 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,022 |
| 263 | wellhead engine | 358 | 264,462 | 4,123,721 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,311 |
| 264 | wellhead engine | 361 | 248,207 | 4,123,526 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6,819 |
| 265 | wellhead engine | 363 | 249,892 | 4,123,476 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6,796 |
| 266 | wellhead engine | 365 | 277,236 | 4,123,374 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,380 |
| 267 | wellhead engine | 367 | 278,209 | 4,123,237 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,672 |
| 268 | wellhead engine | 369 | 246,688 | 4,123,238 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6,783 |
| 269 | wellhead engine | 371 | 280,427 | 4,123,179 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,138 |
| 270 | wellhead engine | 373 | 246,245 | 4,123,252 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6,754 |
| 271 | wellhead engine | 375 | 244,644 | 4,123,189 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,082 |
| 272 | wellhead engine | 377 | 268,435 | 4,122,945 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6,996 |
| 273 | wellhead engine | 379 | 262,668 | 4,123,106 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6,996 |
| 274 | wellhead engine | 382 | 270,121 | 4,122,899 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6,996 |
| 275 | wellhead engine | 384 | 244,631 | 4,122,745 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,082 |
| 276 | wellhead engine | 386 | 278,816 | 4,122,666 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,931 |
| 277 | wellhead engine | 388 | 280,413 | 4,122,625 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,970 |
| 278 | wellhead engine | 390 | 273,492 | 4,122,808 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,147 |
| 279 | wellhead engine | 392 | 276,595 | 4,122,613 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,380 |
| 280 | wellhead engine | 394 | 259,452 | 4,122,420 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6,996 |

Table A-35. Near Field Modeling Input Values (Alternative 2) (continued)

| Source Count | Source Description | Unit ID | UTM | | Emission Rate | | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|--------------------|---------|-------------|--------------|---------------|----------|-----------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | Easting (m) | Northing (m) | NOx (g/s) | CO (g/s) | HAP (g/s) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 281 | wellhead engine | 396 | 269,121 | 4,122,038 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6,944 |
| 282 | wellhead engine | 398 | 273,380 | 4,121,922 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6,996 |
| 283 | wellhead engine | 400 | 274,977 | 4,121,880 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,131 |
| 284 | wellhead engine | 402 | 281,455 | 4,121,709 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,502 |
| 285 | wellhead engine | 404 | 278,703 | 4,121,781 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,685 |
| 286 | wellhead engine | 406 | 280,390 | 4,121,736 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,397 |
| 287 | wellhead engine | 408 | 274,947 | 4,120,770 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,196 |
| 288 | wellhead engine | 410 | 276,456 | 4,120,730 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,377 |
| 289 | wellhead engine | 412 | 277,432 | 4,120,704 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,669 |
| 290 | wellhead engine | 414 | 279,650 | 4,120,646 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,102 |
| 291 | wellhead engine | 416 | 290,031 | 4,120,269 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,396 |
| 292 | wellhead engine | 418 | 275,817 | 4,120,080 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,406 |
| 293 | wellhead engine | 420 | 277,414 | 4,120,038 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,600 |
| 294 | wellhead engine | 422 | 279,015 | 4,120,107 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,469 |
| 295 | wellhead engine | 424 | 289,132 | 4,119,848 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,396 |
| 296 | wellhead engine | 426 | 290,730 | 4,119,808 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,396 |
| 297 | wellhead engine | 428 | 274,814 | 4,119,108 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,196 |
| 298 | wellhead engine | 430 | 276,415 | 4,119,176 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,442 |
| 299 | wellhead engine | 432 | 277,391 | 4,119,150 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,754 |
| 300 | wellhead engine | 434 | 279,610 | 4,119,092 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,744 |
| 301 | wellhead engine | 436 | 290,705 | 4,118,809 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,341 |
| 302 | wellhead engine | 438 | 275,687 | 4,118,529 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,442 |
| 303 | wellhead engine | 440 | 277,373 | 4,118,485 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,305 |
| 304 | wellhead engine | 442 | 278,971 | 4,118,443 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,597 |
| 305 | wellhead engine | 444 | 274,772 | 4,117,554 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,196 |
| 306 | wellhead engine | 446 | 277,968 | 4,117,469 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,295 |
| 307 | wellhead engine | 448 | 277,258 | 4,117,488 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,082 |
| 308 | wellhead engine | 450 | 283,653 | 4,117,432 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,997 |
| 309 | wellhead engine | 452 | 290,666 | 4,117,255 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6,796 |
| 310 | wellhead engine | 454 | 277,240 | 4,116,822 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,082 |
| 311 | wellhead engine | 456 | 278,930 | 4,116,889 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,456 |
| 312 | wellhead engine | 458 | 275,731 | 4,116,862 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,482 |
| 313 | wellhead engine | 460 | 277,217 | 4,115,934 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,895 |
| 314 | wellhead engine | 462 | 279,525 | 4,115,874 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,266 |
| 315 | wellhead engine | 464 | 291,513 | 4,115,569 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6,599 |

Table A-35. Near Field Modeling Input Values (Alternative 2) (continued)

| Source Count | Source Description | Unit ID | UTM | | Emission Rate | | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|--------------------|---------|-------------|--------------|---------------|----------|-----------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | Easting (m) | Northing (m) | NOx (g/s) | CO (g/s) | HAP (g/s) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 316 | wellhead engine | 466 | 277,910 | 4,115,250 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,997 |
| 317 | wellhead engine | 468 | 279,508 | 4,115,208 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,039 |
| 318 | wellhead engine | 470 | 290,700 | 4,115,034 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6,504 |
| 319 | wellhead engine | 472 | 292,117 | 4,114,888 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6,596 |
| 320 | wellhead engine | 474 | 279,393 | 4,114,212 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,764 |
| 321 | wellhead engine | 476 | 281,081 | 4,114,168 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,397 |
| 322 | wellhead engine | 478 | 291,563 | 4,114,013 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6,396 |
| 323 | wellhead engine | 480 | 279,201 | 4,113,661 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,764 |
| 324 | wellhead engine | 482 | 280,977 | 4,113,615 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,397 |
| 325 | wellhead engine | 484 | 291,547 | 4,113,347 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6,393 |
| 326 | wellhead engine | 488 | 281,938 | 4,119,808 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,797 |
| 327 | wellhead engine | 490 | 280,586 | 4,119,067 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,797 |
| 328 | wellhead engine | 492 | 281,880 | 4,117,589 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,797 |
| 329 | wellhead engine | 494 | 280,969 | 4,116,725 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,597 |
| 330 | wellhead engine | 496 | 283,240 | 4,115,222 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,252 |
| 331 | wellhead engine | 498 | 281,639 | 4,115,152 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,597 |
| 332 | wellhead engine | 500 | 284,423 | 4,119,744 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,797 |
| 333 | wellhead engine | 501 | 284,408 | 4,119,190 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,797 |
| 334 | wellhead engine | 503 | 283,587 | 4,118,322 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,085 |
| 335 | wellhead engine | 505 | 280,281 | 4,120,962 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,102 |
| 336 | wellhead engine | 507 | 281,320 | 4,119,936 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,728 |
| 337 | wellhead engine | 509 | 280,658 | 4,118,398 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,597 |
| 338 | wellhead engine | 511 | 280,546 | 4,117,513 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,597 |
| 339 | wellhead engine | 513 | 280,505 | 4,115,959 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,584 |
| 340 | wellhead engine | 515 | 282,831 | 4,116,566 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,344 |
| 341 | wellhead engine | 517 | 282,573 | 4,113,463 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,803 |
| 342 | wellhead engine | 519 | 283,679 | 4,114,989 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,167 |
| 343 | wellhead engine | 521 | 283,636 | 4,116,767 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7,997 |
| 344 | wellhead engine | 523 | 282,722 | 4,115,791 | 0.133 | 0.115 | 0.002 | 1.52 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 8,029 |

Table A-36. Near Field Modeling Input Values (Alternative 5)

| Source Count | Source Description | Unit ID | UTM | | Emission Rate | | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|--------------------|----------|-------------|--------------|---------------|----------|-----------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | Easting (m) | Northing (m) | NOx (g/s) | CO (g/s) | HAP (g/s) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 1 | Elmridge 1 | ELM1A | 288,301 | 4,112,688 | 0.52 | 0.69 | 0.08 | 6.6 | 644 | 17.3 | 0.5 | 3.9 | 3.9 | 6399 |
| 2 | Elmridge 1 | ELM1B | 288,301 | 4,112,698 | 0.52 | 0.69 | 0.08 | 6.6 | 644 | 17.3 | 0.5 | 3.9 | 3.9 | 6399 |
| 3 | Elmridge 1 | ELM1C | 288,301 | 4,112,708 | 0.52 | 0.69 | 0.08 | 6.6 | 644 | 17.3 | 0.5 | 3.9 | 3.9 | 6399 |
| 4 | Elmridge 1 | ELM1D | 288,301 | 4,112,718 | 0.52 | 0.69 | 0.08 | 6.6 | 644 | 17.3 | 0.5 | 3.9 | 3.9 | 6399 |
| 5 | Elmridge 1 | ELM1DEHY | 288,301 | 4,112,728 | 0.13 | 0.11 | 0.00 | 3.5 | 533 | 6.4 | 0.2 | 2.3 | 2.3 | 6399 |
| 6 | Elmridge 1 | ELM1SEP | 288,301 | 4,112,738 | 0.09 | 0.15 | 0.00 | 3.5 | 533 | 6.4 | 0.2 | 2.3 | 2.3 | 6399 |
| 7 | PURE 1 | PUR1 | 251,600 | 4,125,830 | 0.63 | 0.83 | 0.10 | 4.6 | 644 | 29.9 | 0.4 | 3.0 | 3.0 | 7036 |
| 8 | PURE 1 | PUR1SEP | 251,600 | 4,125,840 | 0.13 | 0.11 | 0.00 | 3.0 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 7036 |
| 9 | PURE 1 | PUR1DEH | 251,600 | 4,125,850 | 0.05 | 0.05 | 0.00 | 3.0 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 7036 |
| 10 | PURE 2 | PUR2 | 249,350 | 4,125,160 | 0.10 | 0.13 | 0.02 | 3.0 | 583 | 21.5 | 0.2 | 2.0 | 2.0 | 6803 |
| 11 | PURE 2 | PUR2SEP | 249,350 | 4,125,170 | 0.13 | 0.11 | 0.00 | 3.0 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 6803 |
| 12 | PURE 2 | PUR2DEH | 249,350 | 4,125,180 | 0.01 | 0.01 | 0.00 | 3.0 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 6803 |
| 13 | BP 3 | BP3A | 272,164 | 4,126,575 | 0.63 | 0.83 | 0.10 | 29.9 | 644 | 29.9 | 0.4 | 3.0 | 3.0 | 6996 |
| 14 | BP 3 | BP3B | 272,164 | 4,126,585 | 0.6 | 0.83 | 0.1 | 29.9 | 644 | 29.9 | 0.4 | 3.0 | 3.0 | 6996 |
| 15 | BP 3 | BP3SEP | 272,164 | 4,126,595 | 0.1 | 0.11 | 0.0 | 6.4 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 6996 |
| 16 | BP 3 | BP3DEH | 272,164 | 4,126,605 | 0.1 | 0.09 | 0.0 | 6.4 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 6996 |
| 17 | Cross Timbers | HUB1 | 257,000 | 4,125,000 | 0.5 | 0.69 | 0.1 | 4.6 | 644 | 17.3 | 0.5 | 3.0 | 3.0 | 6934 |
| 18 | Cross Timbers | HUB2 | 257,000 | 4,125,010 | 0.5 | 0.69 | 0.1 | 4.6 | 644 | 17.3 | 0.5 | 3.0 | 3.0 | 6934 |
| 19 | Cross Timbers | HUBDEH | 257,000 | 4,125,020 | 0.1 | 0.11 | 0.0 | 3.0 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 6934 |
| 20 | Cross Timbers | HUBSEP | 257,000 | 4,125,030 | 0.1 | 0.08 | 0.0 | 3.0 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 6934 |
| 21 | Bayfield | BAY1 | 271,500 | 4,125,000 | 0.8 | 1.1 | 0.1 | 7.5 | 644 | 28.6 | 0.5 | 4.9 | 4.9 | 6996 |
| 22 | Bayfield | BAYDEH | 271,500 | 4,125,010 | 0.1 | 0.1 | 0.0 | 3.0 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 6996 |
| 23 | Bayfield | BAYSEP | 271,500 | 4,125,020 | 0.1 | 0.1 | 0.0 | 3.0 | 533 | 6.4 | 0.2 | 2.0 | 2.0 | 6996 |
| 24 | Huber engine | 207 | 263,842 | 4,126,960 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.20 | 1.1 | 1.1 | 7744 |
| 25 | Huber engine | 230 | 262,712 | 4,124,660 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7396 |
| 26 | Huber engine | 237 | 261,268 | 4,123,811 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7022 |
| 27 | Huber engine | 249 | 262,668 | 4,123,106 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6996 |
| 28 | Huber engine | hub1 | 264,640 | 4,126,938 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7478 |
| 29 | Huber engine | hub2 | 258,942 | 4,123,212 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6996 |
| 30 | Huber engine | 176 | 260,793 | 4,132,044 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7875 |
| 31 | Huber engine | 177 | 261,302 | 4,131,252 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7738 |
| 32 | Huber engine | 179 | 258,263 | 4,130,450 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7574 |
| 33 | Huber engine | 185 | 257,531 | 4,129,694 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7383 |
| 34 | Huber engine | 187 | 260,723 | 4,129,603 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7564 |
| 35 | Huber engine | 192 | 253,338 | 4,128,927 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7272 |

Table A-36. Near Field Modeling Input Values (Alternative 5) (continued)

| Source Count | Source Description | Unit ID | UTM | | Emission Rate | | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|--------------------|---------|-------------|--------------|---------------|----------|-----------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | Easting (m) | Northing (m) | NOx (g/s) | CO (g/s) | HAP (g/s) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 36 | Huber engine | 193 | 254,934 | 4,128,881 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7311 |
| 37 | Huber engine | 196 | 254,120 | 4,128,349 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7196 |
| 38 | Huber engine | 204 | 254,268 | 4,127,345 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7052 |
| 39 | wellhead engine | 1 | 290,652 | 4,116,701 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6796 |
| 40 | wellhead engine | 3 | 289,953 | 4,117,162 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6996 |
| 41 | wellhead engine | 5 | 289,190 | 4,118,625 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7045 |
| 42 | wellhead engine | 7 | 289,976 | 4,118,050 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6996 |
| 43 | wellhead engine | 9 | 287,640 | 4,120,551 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7328 |
| 44 | wellhead engine | 11 | 288,428 | 4,120,088 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7252 |
| 45 | wellhead engine | 13 | 287,601 | 4,118,998 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7249 |
| 46 | wellhead engine | 15 | 288,313 | 4,115,538 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7196 |
| 47 | wellhead engine | 17 | 271,025 | 4,126,761 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7196 |
| 48 | wellhead engine | 19 | 270,212 | 4,126,228 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7291 |
| 49 | wellhead engine | 21 | 284,474 | 4,121,742 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7997 |
| 50 | wellhead engine | 23 | 260,793 | 4,132,044 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7997 |
| 51 | wellhead engine | 25 | 262,451 | 4,131,109 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7823 |
| 52 | wellhead engine | 27 | 259,681 | 4,130,410 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7629 |
| 53 | wellhead engine | 29 | 264,731 | 4,130,156 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7692 |
| 54 | wellhead engine | 31 | 267,216 | 4,130,197 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7521 |
| 55 | wellhead engine | 33 | 265,513 | 4,129,579 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7797 |
| 56 | wellhead engine | 35 | 262,407 | 4,129,555 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7797 |
| 57 | wellhead engine | 37 | 267,191 | 4,129,310 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7403 |
| 58 | wellhead engine | 39 | 253,338 | 4,128,927 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7396 |
| 59 | wellhead engine | 41 | 255,913 | 4,128,964 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7400 |
| 60 | wellhead engine | 43 | 254,120 | 4,128,349 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7200 |
| 61 | wellhead engine | 45 | 255,890 | 4,128,187 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7219 |
| 62 | wellhead engine | 47 | 263,956 | 4,127,845 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7797 |
| 63 | wellhead engine | 49 | 275,043 | 4,127,652 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7396 |
| 64 | wellhead engine | 51 | 254,268 | 4,127,345 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7127 |
| 65 | wellhead engine | 53 | 262,870 | 4,127,098 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7659 |
| 66 | wellhead engine | 55 | 267,833 | 4,126,849 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7196 |
| 67 | wellhead engine | 57 | 274,215 | 4,126,564 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7196 |
| 68 | wellhead engine | 59 | 268,616 | 4,126,272 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7059 |
| 69 | wellhead engine | 61 | 271,806 | 4,126,074 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6996 |
| 70 | wellhead engine | 63 | 274,998 | 4,125,988 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7196 |

Table A-36. Near Field Modeling Input Values (Alternative 5) (continued)

| Source Count | Source Description | Unit ID | UTM | | Emission Rate | | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|--------------------|---------|-------------|--------------|---------------|----------|-----------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | Easting (m) | Northing (m) | NOx (g/s) | CO (g/s) | HAP (g/s) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 71 | wellhead engine | 65 | 261,315 | 4,125,476 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7206 |
| 72 | wellhead engine | 67 | 264,505 | 4,125,275 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7239 |
| 73 | wellhead engine | 69 | 269,384 | 4,125,140 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7045 |
| 74 | wellhead engine | 71 | 258,904 | 4,124,990 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7196 |
| 75 | wellhead engine | 73 | 250,024 | 4,124,916 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6796 |
| 76 | wellhead engine | 75 | 266,885 | 4,124,654 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7396 |
| 77 | wellhead engine | 77 | 262,712 | 4,124,660 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7544 |
| 78 | wellhead engine | 79 | 271,849 | 4,124,407 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7196 |
| 79 | wellhead engine | 81 | 250,980 | 4,124,221 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6996 |
| 80 | wellhead engine | 83 | 257,985 | 4,123,905 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7180 |
| 81 | wellhead engine | 85 | 262,158 | 4,123,898 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7337 |
| 82 | wellhead engine | 87 | 248,207 | 4,123,526 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6819 |
| 83 | wellhead engine | 89 | 249,892 | 4,123,476 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6796 |
| 84 | wellhead engine | 91 | 277,236 | 4,123,374 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7380 |
| 85 | wellhead engine | 93 | 263,647 | 4,123,190 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7147 |
| 86 | wellhead engine | 95 | 268,435 | 4,122,945 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6996 |
| 87 | wellhead engine | 97 | 269,323 | 4,122,921 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6977 |
| 88 | wellhead engine | 99 | 271,718 | 4,122,856 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7039 |
| 89 | wellhead engine | 101 | 249,334 | 4,122,604 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6796 |
| 90 | wellhead engine | 103 | 252,975 | 4,122,608 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6960 |
| 91 | wellhead engine | 105 | 264,329 | 4,122,171 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6996 |
| 92 | wellhead engine | 107 | 270,186 | 4,122,009 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 6954 |
| 93 | wellhead engine | 109 | 274,977 | 4,121,880 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7131 |
| 94 | wellhead engine | 111 | 274,947 | 4,120,770 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7196 |
| 95 | wellhead engine | 113 | 274,843 | 4,120,217 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7196 |
| 96 | wellhead engine | 115 | 274,772 | 4,117,554 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7196 |
| 97 | wellhead engine | 117 | 275,731 | 4,116,862 | 0.13 | 0.11 | 0.002 | 1.5 | 477 | 3.8 | 0.2 | 1.1 | 1.1 | 7482 |

Table A-37. Far Field Modeling Input Values (Alternative 1)

| Source Count | Source Description | Unit ID | NOx Emission Rate (g/s) | UTM | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|--------------------|----------|-------------------------|-------------|--------------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | | Easting (m) | Northing (m) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 1 | Elmridge 1 | ELM1A | 0.52 | 288,301 | 4,112,688 | 6.6 | 0.46 | 17.3 | 644 | 3.9 | 3.9 | 6,399 |
| 2 | Elmridge 1 | ELM1B | 0.52 | 288,301 | 4,112,698 | 6.6 | 0.46 | 17.3 | 644 | 3.9 | 3.9 | 6,399 |
| 3 | Elmridge 1 | ELM1C | 0.52 | 288,301 | 4,112,708 | 6.6 | 0.46 | 17.3 | 644 | 3.9 | 3.9 | 6,399 |
| 4 | Elmridge 1 | ELM1D | 0.52 | 288,301 | 4,112,718 | 6.6 | 0.46 | 17.3 | 644 | 3.9 | 3.9 | 6,399 |
| 5 | Elmridge 1 | ELM1DEHY | 0.13 | 288,301 | 4,112,728 | 3.5 | 0.15 | 6.4 | 533 | 2.3 | 2.3 | 6,399 |
| 6 | Elmridge 1 | ELM1SEP | 0.09 | 288,301 | 4,112,738 | 3.5 | 0.15 | 6.4 | 533 | 2.3 | 2.3 | 6,399 |
| 7 | Elmridge 2 | ELM2A | 0.63 | 274,470 | 4,114,300 | 9.5 | 0.38 | 29.2 | 644 | 5.9 | 5.9 | 6,996 |
| 8 | Elmridge 2 | ELM2B | 0.63 | 274,470 | 4,114,310 | 9.5 | 0.38 | 29.2 | 644 | 5.9 | 5.9 | 6,996 |
| 9 | Elmridge 2 | ELM2C | 0.63 | 274,470 | 4,114,320 | 9.5 | 0.38 | 29.2 | 644 | 5.9 | 5.9 | 6,996 |
| 10 | Elmridge 2 | ELM2D | 0.63 | 274,470 | 4,114,330 | 9.5 | 0.38 | 29.2 | 644 | 5.9 | 5.9 | 6,996 |
| 11 | Elmridge 2 | ELM2E | 0.63 | 274,470 | 4,114,340 | 9.5 | 0.38 | 29.2 | 644 | 5.9 | 5.9 | 6,996 |
| 12 | Elmridge 2 | ELM2F | 0.63 | 274,470 | 4,114,350 | 9.5 | 0.38 | 29.2 | 644 | 5.9 | 5.9 | 6,996 |
| 13 | Elmridge 2 | ELM2G | 0.63 | 274,470 | 4,114,360 | 9.5 | 0.38 | 29.2 | 644 | 5.9 | 5.9 | 6,996 |
| 14 | Elmridge 2 | ELM2H | 0.63 | 274,470 | 4,114,370 | 9.5 | 0.38 | 29.2 | 644 | 5.9 | 5.9 | 6,996 |
| 15 | Elmridge 2 | ELM2I | 0.63 | 274,470 | 4,114,380 | 9.5 | 0.38 | 29.2 | 644 | 5.9 | 5.9 | 6,996 |
| 16 | Elmridge 2 | ELM2DEHY | 0.13 | 274,470 | 4,114,270 | 3.5 | 0.15 | 6.4 | 533 | 2.0 | 2.0 | 6,996 |
| 17 | Elmridge 2 | ELM2SEP | 0.11 | 274,470 | 4,114,280 | 3.5 | 0.15 | 6.4 | 533 | 2.0 | 2.0 | 6,996 |
| 18 | Elmridge 2 | ELM2SEPa | 0.11 | 274,470 | 4,114,290 | 3.5 | 0.15 | 6.4 | 533 | 2.0 | 2.0 | 6,996 |
| 19 | PETROX 1 | PET1 | 0.26 | 292,405 | 4,113,912 | 3.1 | 0.30 | 24.1 | 644 | 2.0 | 2.0 | 6,396 |
| 20 | PETROX 1 | PET1DEH | 0.13 | 292,405 | 4,113,922 | 3.0 | 0.15 | 6.4 | 533 | 2.0 | 2.0 | 6,396 |
| 21 | PETROX 1 | PET1SEP | 0.02 | 292,405 | 4,113,932 | 3.0 | 0.15 | 6.4 | 533 | 2.0 | 2.0 | 6,396 |
| 22 | PETROX 2 | PET2 | 0.79 | 286,151 | 4,120,460 | 9.1 | 0.46 | 26.3 | 644 | 4.9 | 4.9 | 7,613 |
| 23 | PETROX 2 | PET2DEH | 0.13 | 286,151 | 4,120,470 | 3.1 | 0.15 | 6.4 | 533 | 2.0 | 2.0 | 7,613 |
| 24 | PETROX 2 | PET2SEP | 0.03 | 286,151 | 4,120,480 | 3.1 | 0.15 | 6.4 | 533 | 2.0 | 2.0 | 7,613 |
| 25 | PETROX 2 | PET2SEPa | 0.03 | 286,151 | 4,120,450 | 3.1 | 0.15 | 6.4 | 533 | 2.0 | 2.0 | 7,613 |
| 26 | BP AMOCO 1 | BP1A | 0.56 | 273,670 | 4,124,111 | 4.6 | 0.46 | 18.4 | 644 | 3.0 | 3.0 | 7,141 |
| 27 | BP AMOCO 1 | BP1B | 0.56 | 273,670 | 4,124,121 | 4.6 | 0.46 | 18.4 | 644 | 3.0 | 3.0 | 7,141 |
| 28 | BP AMOCO 1 | BP1C | 0.56 | 273,670 | 4,124,131 | 4.6 | 0.46 | 18.4 | 644 | 3.0 | 3.0 | 7,141 |
| 29 | BP AMOCO 1 | BP1SEP | 0.13 | 273,670 | 4,124,141 | 3 | 0.15 | 6.4 | 533 | 2.0 | 2.0 | 7,141 |
| 30 | BP AMOCO 1 | BP1DEH | 0.14 | 273,670 | 4,124,151 | 3 | 0.15 | 6.4 | 533 | 2.0 | 2.0 | 7,141 |
| 31 | BP AMOCO 2 | BP2A | 0.63 | 275,030 | 4,114,050 | 4.6 | 0.38 | 29.9 | 644 | 3.0 | 3.0 | 6,799 |
| 32 | BP AMOCO 2 | BP2B | 0.63 | 275,030 | 4,114,060 | 4.6 | 0.38 | 29.9 | 644 | 3.0 | 3.0 | 6,799 |
| 33 | BP AMOCO 2 | BP2SEP | 0.13 | 275,030 | 4,114,070 | 3 | 0.15 | 6.4 | 533 | 2.0 | 2.0 | 6,799 |
| 34 | BP AMOCO 2 | BP2DEH | 0.11 | 275,030 | 4,114,080 | 3 | 0.15 | 6.4 | 533 | 2.0 | 2.0 | 6,799 |
| 35 | PETROX 3 | PET3 | 0.26 | 283,100 | 4,123,180 | 3.05 | 0.30 | 24.1 | 644 | 2.0 | 2.0 | 7,616 |

Table A-37. Far Field Modeling Input Values (Alternative 1) (continued)

| Source Count | Source Description | Unit ID | NOx Emission Rate (g/s) | UTM | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|--------------------|---------|-------------------------|-------------|--------------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | | Easting (m) | Northing (m) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 36 | PETROX 3 | PET3SEP | 0.13 | 283,100 | 4,123,190 | 3 | 0.15 | 6.4 | 533 | 2.0 | 2.0 | 7,616 |
| 37 | PETROX 3 | PET3DEH | 0.02 | 283,100 | 4,123,200 | 3 | 0.15 | 6.4 | 533 | 2.0 | 2.0 | 7,616 |
| 38 | PETROX 4 | PET4 | 0.26 | 281,500 | 4,123,161 | 3.05 | 0.30 | 24.1 | 644 | 2.0 | 2.0 | 8,197 |
| 39 | PETROX 4 | PET4SEP | 0.13 | 281,500 | 4,123,171 | 3 | 0.15 | 6.4 | 533 | 2.0 | 2.0 | 8,197 |
| 40 | PETROX 4 | PET4DEH | 0.02 | 281,500 | 4,123,181 | 3 | 0.15 | 6.4 | 533 | 2.0 | 2.0 | 8,197 |
| 41 | PURE 1 | PUR1 | 0.63 | 251,600 | 4,125,830 | 4.6 | 0.38 | 29.9 | 644 | 3.0 | 3.0 | 7,036 |
| 42 | PURE 1 | PUR1SEP | 0.13 | 251,600 | 4,125,840 | 3 | 0.15 | 6.4 | 533 | 2.0 | 2.0 | 7,036 |
| 43 | PURE 1 | PUR1DEH | 0.05 | 251,600 | 4,125,850 | 3 | 0.15 | 6.4 | 533 | 2.0 | 2.0 | 7,036 |
| 44 | PURE 2 | PUR2 | 0.10 | 249,350 | 4,125,160 | 3 | 0.18 | 21.5 | 583 | 2.0 | 2.0 | 6,803 |
| 45 | PURE 2 | PUR2SEP | 0.13 | 249,350 | 4,125,170 | 3 | 0.18 | 6.44 | 533 | 2.0 | 2.0 | 6,803 |
| 46 | PURE 2 | PUR2DEH | 0.01 | 249,350 | 4,125,180 | 3 | 0.15 | 6.44 | 533 | 2.0 | 2.0 | 6,803 |
| 47 | BP 3 | BP3A | 0.63 | 272,164 | 4,126,575 | 4.6 | 0.38 | 29.9 | 644 | 3.0 | 3.0 | 6,996 |
| 48 | BP 3 | BP3B | 0.63 | 272,164 | 4,126,585 | 4.6 | 0.38 | 29.9 | 644 | 3.0 | 3.0 | 6,996 |
| 49 | BP 3 | BP3SEP | 0.13 | 272,164 | 4,126,595 | 3 | 0.15 | 6.4 | 533 | 2.0 | 2.0 | 6,996 |
| 50 | BP 3 | BP3DEH | 0.11 | 272,164 | 4,126,605 | 3 | 0.15 | 6.4 | 533 | 2.0 | 2.0 | 6,996 |
| 51 | BP 4 | BP4A | 0.56 | 259,000 | 4,124,000 | 4.6 | 0.46 | 18.4 | 644 | 3.0 | 3.0 | 7,082 |
| 52 | BP 4 | BP4B | 0.56 | 259,000 | 4,124,010 | 4.6 | 0.46 | 18.4 | 644 | 3.0 | 3.0 | 7,082 |
| 53 | BP 4 | BP4C | 0.56 | 259,000 | 4,124,020 | 4.6 | 0.46 | 18.4 | 644 | 3.0 | 3.0 | 7,082 |
| 54 | BP 4 | BP4SEP | 0.13 | 259,000 | 4,124,030 | 3 | 0.15 | 6.4 | 533 | 2.0 | 2.0 | 7,082 |
| 55 | BP 4 | BP4DEH | 0.14 | 259,000 | 4,124,040 | 3 | 0.15 | 6.4 | 533 | 2.0 | 2.0 | 7,082 |
| 56 | Cross Timbers | HUB1 | 0.52 | 257,000 | 4,125,000 | 4.6 | 0.46 | 17.3 | 644.0 | 3.0 | 3.0 | 6,934 |
| 57 | Cross Timbers | HUB2 | 0.52 | 257,000 | 4,125,010 | 4.6 | 0.46 | 17.3 | 644.0 | 3.0 | 3.0 | 6,934 |
| 58 | Cross Timbers | HUBSEP | 0.13 | 257,000 | 4,125,020 | 3.0 | 0.15 | 6.4 | 533.0 | 2.0 | 2.0 | 6,934 |
| 59 | Cross Timbers | HUBDEH | 0.09 | 257,000 | 4,125,030 | 3.0 | 0.15 | 6.4 | 533.0 | 2.0 | 2.0 | 6,934 |
| 60 | Bayfield | BAY1 | 0.83 | 271,500 | 4,125,000 | 7.5 | 0.46 | 28.6 | 644.0 | 4.9 | 4.9 | 6,996 |
| 61 | Bayfield | BAYDEH | 0.13 | 271,500 | 4,125,010 | 3.0 | 0.20 | 6.4 | 533.0 | 2.0 | 2.0 | 6,996 |
| 62 | Bayfield | BAYSEP | 0.07 | 271,500 | 4,125,020 | 3.0 | 0.20 | 6.4 | 533.0 | 2.0 | 2.0 | 6,996 |
| 63 | wellhead engine | 101 | 1.06 | 248,207 | 4,123,526 | 1.524 | 0.20 | 3.8 | 477 | 1.0668 | 1.0668 | 6,767 |
| 64 | Huber engine | 193 | 1.06 | 254,934 | 4,128,881 | 1.524 | 0.20 | 3.8 | 477 | 1.0668 | 1.0668 | 7,311 |
| 65 | Huber engine | 2 | 1.06 | 259,133 | 4,129,870 | 1.524 | 0.20 | 3.8 | 477 | 1.0668 | 1.0668 | 7,282 |
| 66 | Huber engine | 237 | 1.06 | 261,268 | 4,123,811 | 1.524 | 0.20 | 3.8 | 477 | 1.0668 | 1.0668 | 7,022 |
| 67 | wellhead engine | 289 | 1.06 | 262,961 | 4,130,317 | 1.524 | 0.20 | 3.8 | 477 | 1.0668 | 1.0668 | 7,800 |
| 68 | Huber engine | 5 | 1.06 | 264,640 | 4,126,938 | 1.524 | 0.20 | 3.8 | 477 | 1.0668 | 1.0668 | 7,478 |
| 69 | wellhead engine | 85 | 1.06 | 268,570 | 4,124,608 | 1.524 | 0.20 | 3.8 | 477 | 1.0668 | 1.0668 | 7,045 |
| 70 | wellhead engine | 175 | 1.06 | 271,851 | 4,127,738 | 1.524 | 0.20 | 3.8 | 477 | 1.0668 | 1.0668 | 7,106 |

Table A-37. Far Field Modeling Input Values (Alternative 1) (continued)

| Source Count | Source Description | Unit ID | NOx Emission Rate (g/s) | UTM | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|--------------------|---------|-------------------------|-------------|--------------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | | Easting (m) | Northing (m) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 71 | wellhead engine | 67 | 1.06 | 274,000 | 4,115,243 | 1.524 | 0.20 | 3.8 | 477 | 1.0668 | 1.0668 | 6,996 |
| 72 | wellhead engine | 93 | 1.06 | 275,731 | 4,116,862 | 1.524 | 0.20 | 3.8 | 477 | 1.0668 | 1.0668 | 7,118 |
| 73 | wellhead engine | 10 | 1.06 | 277,316 | 4,126,370 | 1.524 | 0.20 | 3.8 | 477 | 1.0668 | 1.0668 | 7,446 |
| 74 | wellhead engine | 119 | 1.06 | 280,969 | 4,116,725 | 1.524 | 0.20 | 3.8 | 477 | 1.0668 | 1.0668 | 8,407 |
| 75 | wellhead engine | 151 | 1.06 | 281,992 | 4,115,032 | 1.524 | 0.20 | 3.8 | 477 | 1.0668 | 1.0668 | 8,597 |
| 76 | wellhead engine | 65 | 1.06 | 282,805 | 4,119,009 | 1.524 | 0.20 | 3.8 | 477 | 1.0668 | 1.0668 | 8,797 |
| 77 | wellhead engine | 25 | 1.06 | 283,587 | 4,118,322 | 1.524 | 0.20 | 3.8 | 477 | 1.0668 | 1.0668 | 8,085 |
| 78 | wellhead engine | 149 | 1.06 | 284,366 | 4,114,083 | 1.524 | 0.20 | 3.8 | 477 | 1.0668 | 1.0668 | 7,514 |
| 79 | wellhead engine | 285 | 1.06 | 285,418 | 4,113,501 | 1.524 | 0.20 | 3.8 | 477 | 1.0668 | 1.0668 | 8,016 |
| 80 | wellhead engine | 258 | 1.06 | 286,690 | 4,121,575 | 1.524 | 0.20 | 3.8 | 477 | 1.0668 | 1.0668 | 7,396 |
| 81 | wellhead engine | 159 | 1.06 | 288,280 | 4,114,206 | 1.524 | 0.20 | 3.8 | 477 | 1.0668 | 1.0668 | 7,193 |
| 82 | wellhead engine | 180 | 0.80 | 289,976 | 4,118,050 | 1.524 | 0.20 | 3.8 | 477 | 1.0668 | 1.0668 | 6,996 |

Table A-38. Far Field Modeling Input Values (Alternative 2)

| Source Count | Source Description | Unit ID | NOx Emission Rate (g/s) | UTM | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|--------------------|----------|-------------------------|-------------|--------------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | | Easting (m) | Northing (m) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 1 | Elmridge 1 | ELM1A | 0.521 | 288,301 | 4,112,688 | 6.60 | 0.5 | 17.3 | 644 | 3.9 | 3.9 | 6,399 |
| 2 | Elmridge 1 | ELM1B | 0.521 | 288,301 | 4,112,698 | 6.60 | 0.5 | 17.3 | 644 | 3.9 | 3.9 | 6,399 |
| 3 | Elmridge 1 | ELM1C | 0.521 | 288,301 | 4,112,708 | 6.60 | 0.5 | 17.3 | 644 | 3.9 | 3.9 | 6,399 |
| 4 | Elmridge 1 | ELM1D | 0.521 | 288,301 | 4,112,718 | 6.60 | 0.5 | 17.3 | 644 | 3.9 | 3.9 | 6,399 |
| 5 | Elmridge 1 | ELM1DEHY | 0.126 | 288,301 | 4,112,728 | 3.50 | 0.2 | 6.4 | 533 | 2.3 | 2.3 | 6,399 |
| 6 | Elmridge 1 | ELM1SEP | 0.089 | 288,301 | 4,112,738 | 3.50 | 0.2 | 6.4 | 533 | 2.3 | 2.3 | 6,399 |
| 7 | Elmridge 2 | ELM2A | 0.625 | 274,470 | 4,114,300 | 9.50 | 0.4 | 29.2 | 644 | 5.9 | 5.9 | 6,996 |
| 8 | Elmridge 2 | ELM2B | 0.625 | 274,470 | 4,114,310 | 9.50 | 0.4 | 29.2 | 644 | 5.9 | 5.9 | 6,996 |
| 9 | Elmridge 2 | ELM2C | 0.625 | 274,470 | 4,114,320 | 9.50 | 0.4 | 29.2 | 644 | 5.9 | 5.9 | 6,996 |
| 10 | Elmridge 2 | ELM2D | 0.625 | 274,470 | 4,114,330 | 9.50 | 0.4 | 29.2 | 644 | 5.9 | 5.9 | 6,996 |
| 11 | Elmridge 2 | ELM2E | 0.625 | 274,470 | 4,114,340 | 9.50 | 0.4 | 29.2 | 644 | 5.9 | 5.9 | 6,996 |
| 12 | Elmridge 2 | ELM2F | 0.625 | 274,470 | 4,114,350 | 9.50 | 0.4 | 29.2 | 644 | 5.9 | 5.9 | 6,996 |
| 13 | Elmridge 2 | ELM2G | 0.625 | 274,470 | 4,114,360 | 9.50 | 0.4 | 29.2 | 644 | 5.9 | 5.9 | 6,996 |
| 14 | Elmridge 2 | ELM2H | 0.625 | 274,470 | 4,114,370 | 9.50 | 0.4 | 29.2 | 644 | 5.9 | 5.9 | 6,996 |
| 15 | Elmridge 2 | ELM2I | 0.625 | 274,470 | 4,114,380 | 9.50 | 0.4 | 29.2 | 644 | 5.9 | 5.9 | 6,996 |
| 16 | Elmridge 2 | ELM2DEHY | 0.126 | 274,470 | 4,114,270 | 3.50 | 0.2 | 6.4 | 533 | 2.0 | 2.0 | 6,996 |
| 17 | Elmridge 2 | ELM2SEP | 0.110 | 274,470 | 4,114,280 | 3.50 | 0.2 | 6.4 | 533 | 2.0 | 2.0 | 6,996 |
| 18 | Elmridge 2 | ELM2SEPa | 0.110 | 274,470 | 4,114,290 | 3.50 | 0.2 | 6.4 | 533 | 2.0 | 2.0 | 6,996 |
| 19 | PETROX 1 | PET1 | 0.258 | 292,405 | 4,113,912 | 3.05 | 0.3 | 24.1 | 644 | 2.0 | 2.0 | 6,396 |
| 20 | PETROX 1 | PET1DEH | 0.126 | 292,405 | 4,113,922 | 3.00 | 0.2 | 6.4 | 533 | 2.0 | 2.0 | 6,396 |
| 21 | PETROX 1 | PET1SEP | 0.022 | 292,405 | 4,113,932 | 3.00 | 0.2 | 6.4 | 533 | 2.0 | 2.0 | 6,396 |
| 22 | PETROX 2 | PET2 | 0.792 | 286,151 | 4,120,460 | 9.10 | 0.5 | 26.3 | 644 | 4.9 | 4.9 | 7,613 |
| 23 | PETROX 2 | PET2DEH | 0.126 | 286,151 | 4,120,470 | 3.10 | 0.2 | 6.4 | 533 | 2.0 | 2.0 | 7,613 |
| 24 | PETROX 2 | PET2SEP | 0.034 | 286,151 | 4,120,480 | 3.10 | 0.2 | 6.4 | 533 | 2.0 | 2.0 | 7,613 |
| 25 | PETROX 2 | PET2SEPa | 0.034 | 286,151 | 4,120,450 | 3.10 | 0.2 | 6.4 | 533 | 2.0 | 2.0 | 7,613 |
| 26 | BP AMOCO 1 | BP1A | 0.556 | 273,670 | 4,124,111 | 4.60 | 0.5 | 18.4 | 644 | 3.0 | 3.0 | 7,141 |
| 27 | BP AMOCO 1 | BP1B | 0.556 | 273,670 | 4,124,121 | 4.60 | 0.5 | 18.4 | 644 | 3.0 | 3.0 | 7,141 |
| 28 | BP AMOCO 1 | BP1C | 0.556 | 273,670 | 4,124,131 | 4.60 | 0.5 | 18.4 | 644 | 3.0 | 3.0 | 7,141 |
| 29 | BP AMOCO 1 | BP1DEH | 0.126 | 273,670 | 4,124,141 | 3.00 | 0.2 | 6.4 | 533 | 2.0 | 2.0 | 7,141 |
| 30 | BP AMOCO 1 | BP1SEP | 0.143 | 273,670 | 4,124,151 | 3.00 | 0.2 | 6.4 | 533 | 2.0 | 2.0 | 7,141 |
| 31 | BP AMOCO 2 | BP2A | 0.625 | 275,030 | 4,114,050 | 4.60 | 0.4 | 29.9 | 644 | 3.0 | 3.0 | 6,799 |
| 32 | BP AMOCO 2 | BP2B | 0.625 | 275,030 | 4,114,060 | 4.60 | 0.4 | 29.9 | 644 | 3.0 | 3.0 | 6,799 |
| 33 | BP AMOCO 2 | BP2DEH | 0.126 | 275,030 | 4,114,070 | 3.00 | 0.2 | 6.4 | 533 | 2.0 | 2.0 | 6,799 |
| 34 | BP AMOCO 2 | BP2SEP | 0.107 | 275,030 | 4,114,080 | 3.00 | 0.2 | 6.4 | 533 | 2.0 | 2.0 | 6,799 |
| 35 | PETROX 3 | PET3 | 0.258 | 283,100 | 4,123,180 | 3.05 | 0.3 | 24.1 | 644 | 2.0 | 2.0 | 7,616 |

Table A-38. Far Field Modeling Input Values (Alternative 2) (continued)

| Source Count | Source Description | Unit ID | NOx Emission Rate (g/s) | UTM | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|--------------------|---------|-------------------------|-------------|--------------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | | Easting (m) | Northing (m) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 36 | PETROX 3 | PET3DEH | 0.126 | 283,100 | 4,123,190 | 3.00 | 0.2 | 6.4 | 533 | 2.0 | 2.0 | 7,616 |
| 37 | PETROX 3 | PET3SEP | 0.022 | 283,100 | 4,123,200 | 3.00 | 0.2 | 6.4 | 533 | 2.0 | 2.0 | 7,616 |
| 38 | PETROX 4 | PET4 | 0.258 | 281,500 | 4,123,161 | 3.05 | 0.3 | 24.1 | 644 | 2.0 | 2.0 | 8,197 |
| 39 | PETROX 4 | PET4DEH | 0.126 | 281,500 | 4,123,171 | 3.00 | 0.2 | 6.4 | 533 | 2.0 | 2.0 | 8,197 |
| 40 | PETROX 4 | PET4SEP | 0.022 | 281,500 | 4,123,181 | 3.00 | 0.2 | 6.4 | 533 | 2.0 | 2.0 | 8,197 |
| 41 | PURE 1 | PUR1 | 0.625 | 251,600 | 4,125,830 | 4.60 | 0.4 | 29.9 | 644 | 3.0 | 3.0 | 7,036 |
| 42 | PURE 1 | PUR1DEH | 0.126 | 251,600 | 4,125,840 | 3.00 | 0.2 | 6.4 | 533 | 2.0 | 2.0 | 7,036 |
| 43 | PURE 1 | PUR1SEP | 0.054 | 251,600 | 4,125,850 | 3.00 | 0.2 | 6.4 | 533 | 2.0 | 2.0 | 7,036 |
| 44 | PURE 2 | PUR2 | 0.100 | 249,350 | 4,125,160 | 3.00 | 0.2 | 21.5 | 583 | 2.0 | 2.0 | 6,803 |
| 45 | PURE 2 | PUR2DEH | 0.126 | 249,350 | 4,125,170 | 3.00 | 0.2 | 6.4 | 533 | 2.0 | 2.0 | 6,803 |
| 46 | PURE 2 | PUR2SEP | 0.009 | 249,350 | 4,125,180 | 3.00 | 0.2 | 6.4 | 533 | 2.0 | 2.0 | 6,803 |
| 47 | BP 3 | BP3A | 0.625 | 272,164 | 4,126,575 | 4.60 | 0.4 | 29.9 | 644 | 3.0 | 3.0 | 6,996 |
| 48 | BP 3 | BP3B | 0.625 | 272,164 | 4,126,585 | 4.60 | 0.4 | 29.9 | 644 | 3.0 | 3.0 | 6,996 |
| 49 | BP 3 | BP3DEH | 0.126 | 272,164 | 4,126,595 | 3.00 | 0.2 | 6.4 | 533 | 2.0 | 2.0 | 6,996 |
| 50 | BP 3 | BP3SEP | 0.107 | 272,164 | 4,126,605 | 3.00 | 0.2 | 6.4 | 533 | 2.0 | 2.0 | 6,996 |
| 51 | BP 4 | BP4A | 0.556 | 259,000 | 4,124,000 | 4.60 | 0.5 | 18.4 | 644 | 3.0 | 3.0 | 7,082 |
| 52 | BP 4 | BP4B | 0.556 | 259,000 | 4,124,010 | 4.60 | 0.5 | 18.4 | 644 | 3.0 | 3.0 | 7,082 |
| 53 | BP 4 | BP4C | 0.556 | 259,000 | 4,124,020 | 4.60 | 0.5 | 18.4 | 644 | 3.0 | 3.0 | 7,082 |
| 54 | BP 4 | BP4DEH | 0.126 | 259,000 | 4,124,030 | 3.00 | 0.2 | 6.4 | 533 | 2.0 | 2.0 | 7,082 |
| 55 | BP 4 | BP4SEP | 0.143 | 259,000 | 4,124,040 | 3.00 | 0.2 | 6.4 | 533 | 2.0 | 2.0 | 7,082 |
| 56 | Cross Timbers | HUB1 | 0.521 | 257,000 | 4,125,000 | 4.60 | 0.5 | 17.3 | 644.0 | 3.0 | 3.0 | 6,934 |
| 57 | Cross Timbers | HUB2 | 0.521 | 257,000 | 4,125,010 | 4.60 | 0.5 | 17.3 | 644.0 | 3.0 | 3.0 | 6,934 |
| 58 | Cross Timbers | HUBDEH | 0.126 | 257,000 | 4,125,020 | 3.00 | 0.2 | 6.4 | 533.0 | 2.0 | 2.0 | 6,934 |
| 59 | Cross Timbers | HUBSEP | 0.089 | 257,000 | 4,125,030 | 3.00 | 0.2 | 6.4 | 533.0 | 2.0 | 2.0 | 6,934 |
| 60 | Independent 1 | IP1 | 0.417 | 277,120 | 4,115,417 | 3.05 | 0.3 | 24.8 | 644 | 2.0 | 2.0 | 7,514 |
| 61 | Independent 1 | IP1DEH | 0.126 | 277,120 | 4,115,427 | 3.00 | 0.2 | 6.4 | 533 | 2.0 | 2.0 | 7,514 |
| 62 | Independent 1 | IP1SEP | 0.036 | 277,120 | 4,115,437 | 3.00 | 0.2 | 6.4 | 533 | 2.0 | 2.0 | 7,514 |
| 63 | Independent 2 | IP2A | 0.833 | 275,600 | 4,120,800 | 7.50 | 0.5 | 25.3 | 644 | 4.9 | 4.9 | 7,196 |
| 64 | Independent 2 | IP2DEH | 0.126 | 275,600 | 4,120,810 | 3.00 | 0.2 | 6.4 | 533 | 2.0 | 2.0 | 7,196 |
| 65 | Independent 2 | IP2SEP | 0.071 | 275,600 | 4,120,820 | 3.00 | 0.2 | 6.4 | 533 | 2.0 | 2.0 | 7,196 |
| 66 | Independent 3 | IP3A | 0.833 | 276,435 | 4,116,788 | 7.50 | 0.5 | 25.3 | 644 | 4.9 | 4.9 | 7,426 |
| 67 | Independent 3 | IP3DEH | 0.126 | 276,435 | 4,116,778 | 3.00 | 0.2 | 6.4 | 533 | 2.0 | 2.0 | 7,426 |
| 68 | Independent 3 | IP3SEP | 0.071 | 276,435 | 4,116,778 | 3.00 | 0.2 | 6.4 | 533 | 2.0 | 2.0 | 7,426 |
| 69 | Bayfield | BAY1 | 0.833 | 271,500 | 4,125,000 | 7.50 | 0.5 | 28.6 | 644 | 4.9 | 4.9 | 6,996 |
| 70 | Bayfield | BAYDEH | 0.126 | 271,500 | 4,125,010 | 3.00 | 0.2 | 6.4 | 533 | 2.0 | 2.0 | 6,996 |

Table A-38. Far Field Modeling Input Values (Alternative 2) (continued)

| Source Count | Source Description | Unit ID | NOx Emission Rate (g/s) | UTM | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|--------------------|---------|-------------------------|-------------|--------------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | | Easting (m) | Northing (m) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 71 | Bayfield | BAYSEP | 0.071 | 271,500 | 4,125,020 | 3.00 | 0.2 | 6.4 | 533 | 2.0 | 2.0 | 6,996 |
| 72 | wellhead engine | 384 | 1.064 | 244,631 | 4,122,745 | 1.52 | 0.2 | 3.8 | 477 | 1.1 | 1.1 | 6,816 |
| 73 | wellhead engine | 337 | 1.064 | 248,253 | 4,125,080 | 1.52 | 0.2 | 3.8 | 477 | 1.1 | 1.1 | 6,901 |
| 74 | wellhead engine | 323 | 1.064 | 251,561 | 4,125,870 | 1.52 | 0.2 | 3.8 | 477 | 1.1 | 1.1 | 7,039 |
| 75 | Huber engine | 275 | 1.064 | 254,120 | 4,128,349 | 1.52 | 0.2 | 3.8 | 477 | 1.1 | 1.1 | 7,196 |
| 76 | Huber engine | 214 | 1.064 | 254,980 | 4,130,435 | 1.52 | 0.2 | 3.8 | 477 | 1.1 | 1.1 | 7,826 |
| 77 | Huber engine | 241 | 1.064 | 257,531 | 4,129,694 | 1.52 | 0.2 | 3.8 | 477 | 1.1 | 1.1 | 7,383 |
| 78 | Huber engine | 174 | 1.064 | 259,194 | 4,131,979 | 1.52 | 0.2 | 3.8 | 477 | 1.1 | 1.1 | 7,770 |
| 79 | Huber engine | 176 | 1.064 | 260,793 | 4,132,044 | 1.52 | 0.2 | 3.8 | 477 | 1.1 | 1.1 | 7,875 |
| 80 | Huber engine | 347 | 1.064 | 262,712 | 4,124,660 | 1.52 | 0.2 | 3.8 | 477 | 1.1 | 1.1 | 7,396 |
| 81 | wellhead engine | 190 | 1.064 | 264,670 | 4,131,157 | 1.52 | 0.2 | 3.8 | 477 | 1.1 | 1.1 | 7,596 |
| 82 | wellhead engine | 180 | 1.064 | 266,192 | 4,131,670 | 1.52 | 0.2 | 3.8 | 477 | 1.1 | 1.1 | 7,419 |
| 83 | wellhead engine | 299 | 1.064 | 269,426 | 4,126,693 | 1.52 | 0.2 | 3.8 | 477 | 1.1 | 1.1 | 7,052 |
| 84 | wellhead engine | 232 | 1.064 | 271,908 | 4,129,847 | 1.52 | 0.2 | 3.8 | 477 | 1.1 | 1.1 | 7,478 |
| 85 | wellhead engine | 234 | 1.064 | 273,504 | 4,129,804 | 1.52 | 0.2 | 3.8 | 477 | 1.1 | 1.1 | 7,341 |
| 86 | wellhead engine | 53 | 1.064 | 274,862 | 4,124,214 | 1.52 | 0.2 | 3.8 | 477 | 1.1 | 1.1 | 7,124 |
| 87 | wellhead engine | 458 | 1.064 | 275,731 | 4,116,862 | 1.52 | 0.2 | 3.8 | 477 | 1.1 | 1.1 | 7,118 |
| 88 | wellhead engine | 392 | 1.064 | 276,595 | 4,122,613 | 1.52 | 0.2 | 3.8 | 477 | 1.1 | 1.1 | 7,180 |
| 89 | wellhead engine | 448 | 1.064 | 277,258 | 4,117,488 | 1.52 | 0.2 | 3.8 | 477 | 1.1 | 1.1 | 8,062 |
| 90 | wellhead engine | 446 | 1.064 | 277,968 | 4,117,469 | 1.52 | 0.2 | 3.8 | 477 | 1.1 | 1.1 | 8,256 |
| 91 | wellhead engine | 317 | 1.064 | 278,901 | 4,125,884 | 1.52 | 0.2 | 3.8 | 477 | 1.1 | 1.1 | 7,865 |
| 92 | wellhead engine | 474 | 1.064 | 279,393 | 4,114,212 | 1.52 | 0.2 | 3.8 | 477 | 1.1 | 1.1 | 7,396 |
| 93 | wellhead engine | 307 | 1.064 | 279,890 | 4,126,413 | 1.52 | 0.2 | 3.8 | 477 | 1.1 | 1.1 | 7,793 |
| 94 | wellhead engine | 513 | 1.064 | 280,505 | 4,115,959 | 1.52 | 0.2 | 3.8 | 477 | 1.1 | 1.1 | 8,197 |
| 95 | wellhead engine | 476 | 1.064 | 281,081 | 4,114,168 | 1.52 | 0.2 | 3.8 | 477 | 1.1 | 1.1 | 8,102 |
| 96 | wellhead engine | 498 | 1.064 | 281,639 | 4,115,152 | 1.52 | 0.2 | 3.8 | 477 | 1.1 | 1.1 | 8,597 |
| 97 | wellhead engine | 49 | 1.064 | 282,276 | 4,126,018 | 1.52 | 0.2 | 3.8 | 477 | 1.1 | 1.1 | 7,839 |
| 98 | wellhead engine | 287 | 1.064 | 283,023 | 4,127,443 | 1.52 | 0.2 | 3.8 | 477 | 1.1 | 1.1 | 7,938 |
| 99 | wellhead engine | 450 | 1.064 | 283,653 | 4,117,432 | 1.52 | 0.2 | 3.8 | 477 | 1.1 | 1.1 | 7,593 |
| 100 | wellhead engine | 123 | 1.064 | 284,366 | 4,114,083 | 1.52 | 0.2 | 3.8 | 477 | 1.1 | 1.1 | 7,514 |
| 101 | wellhead engine | 85 | 1.064 | 285,422 | 4,120,608 | 1.52 | 0.2 | 3.8 | 477 | 1.1 | 1.1 | 7,682 |
| 102 | wellhead engine | 99 | 1.064 | 286,802 | 4,119,018 | 1.52 | 0.2 | 3.8 | 477 | 1.1 | 1.1 | 7,396 |
| 103 | wellhead engine | 131 | 1.064 | 288,299 | 4,114,983 | 1.52 | 0.2 | 3.8 | 477 | 1.1 | 1.1 | 6,780 |
| 104 | wellhead engine | 23 | 1.064 | 289,953 | 4,117,162 | 1.52 | 0.2 | 3.8 | 477 | 1.1 | 1.1 | 6,796 |
| 105 | wellhead engine | 464 | 0.665 | 291,513 | 4,115,569 | 1.52 | 0.2 | 3.8 | 477 | 1.1 | 1.1 | 6,399 |
| 106 | wellhead engine | 29 | 0.665 | 292,360 | 4,113,882 | 1.52 | 0.2 | 3.8 | 477 | 1.1 | 1.1 | 6,396 |

Table A-39. Far Field Modeling Input Values (Alternative 5)

| Source Count | Source Description | Unit ID | NOx Emission Rate (g/s) | UTM | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|--------------------|----------|-------------------------|-------------|--------------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | | Easting (m) | Northing (m) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 1 | Elmridge 1 | ELM1A | 0.52 | 288,301 | 4,112,688 | 6.6 | 0.5 | 17.3 | 644 | 3.9 | 3.9 | 6,399 |
| 2 | Elmridge 1 | ELM1B | 0.52 | 288,301 | 4,112,698 | 6.6 | 0.5 | 17.3 | 644 | 3.9 | 3.9 | 6,399 |
| 3 | Elmridge 1 | ELM1C | 0.52 | 288,301 | 4,112,708 | 6.6 | 0.5 | 17.3 | 644 | 3.9 | 3.9 | 6,399 |
| 4 | Elmridge 1 | ELM1D | 0.52 | 288,301 | 4,112,718 | 6.6 | 0.5 | 17.3 | 644 | 3.9 | 3.9 | 6,399 |
| 5 | Elmridge 1 | ELM1DEHY | 0.13 | 288,301 | 4,112,728 | 3.5 | 0.2 | 6.4 | 533 | 2.3 | 2.3 | 6,399 |
| 6 | Elmridge 1 | ELM1SEP | 0.09 | 288,301 | 4,112,738 | 3.5 | 0.2 | 6.4 | 533 | 2.3 | 2.3 | 6,399 |
| 7 | PURE 1 | PUR1 | 0.63 | 251,600 | 4,125,830 | 4.6 | 0.4 | 29.9 | 644 | 3.0 | 3.0 | 7,036 |
| 8 | PURE 1 | PUR1DEH | 0.13 | 251,600 | 4,125,840 | 3 | 0.2 | 6.4 | 533 | 2.0 | 2.0 | 7,036 |
| 9 | PURE 1 | PUR1SEP | 0.05 | 251,600 | 4,125,850 | 3 | 0.2 | 6.4 | 533 | 2.0 | 2.0 | 7,036 |
| 10 | PURE 2 | PUR2 | 0.10 | 249,350 | 4,125,160 | 3 | 0.2 | 21.5 | 583 | 2.0 | 2.0 | 6,803 |
| 11 | PURE 2 | PUR2DEH | 0.13 | 249,350 | 4,125,170 | 3 | 0.2 | 6.4 | 533 | 2.0 | 2.0 | 6,803 |
| 12 | PURE 2 | PUR2SEP | 0.01 | 249,350 | 4,125,180 | 3 | 0.2 | 6.4 | 533 | 2.0 | 2.0 | 6,803 |
| 13 | BP 3 | BP3A | 0.63 | 272,164 | 4,126,575 | 4.6 | 0.4 | 29.9 | 644.0 | 3.0 | 3.0 | 6,996 |
| 14 | BP 3 | BP3B | 0.6 | 272,164 | 4,126,585 | 4.6 | 0.4 | 29.9 | 644.0 | 3.0 | 3.0 | 6,996 |
| 15 | BP 3 | BP3DEH | 0.1 | 272,164 | 4,126,595 | 3 | 0.2 | 6.4 | 533.0 | 2.0 | 2.0 | 6,996 |
| 16 | BP 3 | BP3SEP | 0.1 | 272,164 | 4,126,605 | 3 | 0.2 | 6.4 | 533.0 | 2.0 | 2.0 | 6,996 |
| 17 | Cross Timbers | HUB1 | 0.5 | 257,000 | 4,125,000 | 4.6 | 0.5 | 17.3 | 644 | 3.0 | 3.0 | 6,934 |
| 18 | Cross Timbers | HUB2 | 0.5 | 257,000 | 4,125,010 | 4.6 | 0.5 | 17.3 | 644 | 3.0 | 3.0 | 6,934 |
| 19 | Cross Timbers | HUBDEH | 0.1 | 257,000 | 4,125,020 | 3.0 | 0.2 | 6.4 | 533 | 2.0 | 2.0 | 6,934 |
| 20 | Cross Timbers | HUBSEP | 0.1 | 257,000 | 4,125,030 | 3.0 | 0.2 | 6.4 | 533 | 2.0 | 2.0 | 6,934 |
| 21 | Bayfield | BAY1 | 0.8 | 271,500 | 4,125,000 | 7.5 | 0.5 | 28.6 | 644.0 | 4.9 | 4.9 | 6,996.0 |
| 22 | Bayfield | BAYDEH | 0.1 | 271,500 | 4,125,010 | 3 | 0.2 | 6.4 | 533.0 | 2.0 | 2.0 | 6,996.0 |
| 23 | Bayfield | BAYSEP | 0.1 | 271,500 | 4,125,020 | 3 | 0.2 | 6.4 | 533.0 | 2.0 | 2.0 | 6,996.0 |
| 24 | wellhead engine | 87 | 1.06 | 248,207 | 4,123,526 | 1.5 | 0.2 | 3.8 | 477 | 1.1 | 1.1 | 7,183 |
| 25 | Huber engine | 196 | 1.06 | 254,120 | 4,128,349 | 1.5 | 0.2 | 3.8 | 477 | 1.1 | 1.1 | 7,196 |
| 26 | wellhead engine | 83 | 1.06 | 257,985 | 4,123,905 | 1.5 | 0.2 | 3.8 | 477 | 1.1 | 1.1 | 7,196 |
| 27 | Huber engine | 237 | 1.06 | 261,268 | 4,123,811 | 1.5 | 0.2 | 3.8 | 477 | 1.1 | 1.1 | 7,022 |
| 28 | wellhead engine | 77 | 1.06 | 262,712 | 4,124,660 | 1.5 | 0.2 | 3.8 | 477 | 1.1 | 1.1 | 7,239 |
| 29 | wellhead engine | 29 | 1.06 | 264,731 | 4,130,156 | 1.5 | 0.2 | 3.8 | 477 | 1.1 | 1.1 | 7,797 |
| 30 | wellhead engine | 97 | 1.06 | 269,323 | 4,122,921 | 1.5 | 0.2 | 3.8 | 477 | 1.1 | 1.1 | 6,996 |
| 31 | wellhead engine | 57 | 1.06 | 274,215 | 4,126,564 | 1.5 | 0.2 | 3.8 | 477 | 1.1 | 1.1 | 7,091 |
| 32 | wellhead engine | 91 | 1.06 | 277,236 | 4,123,374 | 1.5 | 0.2 | 3.8 | 477 | 1.1 | 1.1 | 6,934 |
| 33 | wellhead engine | 7 | 0.27 | 289,976 | 4,118,050 | 1.5 | 0.2 | 3.8 | 477 | 1.1 | 1.1 | 7,396 |

Appendix B – Colorado Emission Inventory

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|-------------------------------------------------------------------------|-------------|
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| B-2. Existing Colorado Emission Sources Represented by Background Data | 143 |
| B-3. Colorado Reasonably Foreseeable Emission Sources | 149 |
| B-4. Colorado Emission Source Modeling Input Values | 152 |

Table B-1. Potential Colorado Emission Sources Located Outside the Study Area

| Source Count | Facility Name | Source Description |
|--------------|--------------------------------------------|--------------------------|
| 1 | AMOCO PRODUCTION CO LEMO 17U-01 UNIT #1 | CATERPILLAR 3304 80 HP |
| 2 | AMOCO PRODUCTION CO SOUTH EAST TIFFANY | AJAX DPC,180 HP, ENGINE |
| 3 | CELSIUS ENERGY CO ISLAND BUTTES WELL 6 | AJAX DPC 600 LE SN 83809 |
| 4 | CELSIUS ENERGY CO ISLAND BUTTES WELL 6 | AJAX MDO DP60 |
| 5 | EMERALD GAS OPERATING COMPANY | CATERPILLAR ICE G3512 LE |
| 6 | EMERALD GAS OPERATING COMPANY | WAUKESHA L7042 SN:305951 |
| 7 | ERTEL INC ERTEL FUNERAL HOME | AJAX MOD DP 60 |

Table B-2. Existing Colorado Emission Sources Represented by Background Data

| Source Count | Facility Name | Source Description |
|--------------|---------------------------------------------|----------------------------|
| 1 | 44 CANYON LLC C/O HALLWOOD PETROLEUM INC | CUMMINS 140HP LATERAL |
| 2 | 44 CANYON LLC C/O HALLWOOD PETROLEUM INC | SAND & GRAVEL PIT |
| 3 | 44 CANYON LLC C/O HALLWOOD PETROLEUM INC | CONCRETE BATCH PLANT |
| 4 | 44 CANYON LLC C/O HALLWOOD PETROLEUM INC | CONCRETE BATCH PLANT |
| 5 | 44 CANYON LLC C/O HALLWOOD PETROLEUM INC | CAT G3408TA, SN: 87-111 |
| 6 | 44 CANYON LLC C/O HALLWOOD PETROLEUM INC | WAUKESHA F1197, SN:398947 |
| 7 | 44 CANYON LLC C/O HALLWOOD PETROLEUM INC | GLYCOL REBOILER H-102A |
| 8 | 44 CANYON LLC C/O HALLWOOD PETROLEUM INC | GLYCOL REBOILER H-102B |
| 9 | 44 CANYON LLC C/O HALLWOOD PETROLUEM INC | CUMMINS 365 KW DIESEL GEN |
| 10 | 44 CANYON LLC C/O HALLWOOD PETROLEUM | REGENERATION GAS HEATER |
| 11 | AMAX OIL & GAS INC MCDERMOTT COMP STA | REMEDI-SOIL VAP EXT CONT |
| 12 | AMAX OIL & GAS INC MCDERMOTT COMP STA | WAUKESHA 24756 ENG. 405HP |
| 13 | AMERADA HESS CORP FASSETT GAS UNIT 2 | CRUSHER SN:C52536 |
| 14 | AMERADA HESS CORP FORD OLSON GA UN A 2 | CRUSHER SN:C52536 |
| 15 | AMERADA HESS CORP MILLER GAS UNIT 2 | CONCRETE BATCH PLANT |
| 16 | AMERADA HESS CORP OLSON SMITH GAS UNIT | CONCRETE BATCH PLANT |
| 17 | AMOCO PRODUCTION ELDRIDGE 31-1 | (7) AJAX E-42 ENGINES38HP |
| 18 | AMOCO PRODUCTION HENRICKSON UNIT B #1 | WAUKESHA 303HP COMPRESSOR |
| 19 | AMOCO PRODUCTION CO PICNIC FLATS | WEST DEHYDRATION UNIT |
| 20 | AMOCO PRODUCTION CO PICNIC FLATS | AJAX DPC360LE |
| 21 | AMOCO PRODUCTION CO CONRAD G.U. A#1 | GRAVEL MINING OPERATION |
| 22 | AMOCO PRODUCTION CO HOTTER G.U. A#1 | PORTABLE DIESEL-FIRED _HTR |
| 23 | AMOCO PRODUCTION CO LINDER G.U. A#1 | GRAVEL MINING OPERATION |
| 24 | AMOCO PRODUCTION CO ANDERSON WELL 28-3 | S. UTE 22-33 ENGINE |
| 25 | AMOCO PRODUCTION CO BARNES LEIDY G.U.A#1 | GRAVEL MINING OPERATION |

**Table B-2. Existing Colorado Emission Sources Represented by Background Data
(continued)**

| Source Count | Facility Name | Source Description |
|--------------|------------------------------------------|---------------------------|
| 26 | AMOCO PRODUCTION CO FLORIDA RIVER COMP | (2)WAUKESHA VRG-220 ENGS. |
| 27 | AMOCO PRODUCTION CO FLORIDA RIVER COMP | AJAX DPC-600 495HP CMPRSR |
| 28 | AMOCO PRODUCTION CO FLORIDA RIVER COMP | WAUKESHA L7042GL 862HP |
| 29 | AMOCO PRODUCTION CO GEARHART WELL #1-6 | S. UTE 42-4 ENGINE |
| 30 | AMOCO PRODUCTION CO IGNACIO H2O COLL.SYS | GRAVEL MINING OPERATION |
| 31 | AMOCO PRODUCTION CO J.W.WARD GU A#1 | CIP 50 BBL/DAY STEAMER |
| 32 | AMOCO PRODUCTION CO LORETT FEDERAL GU #1 | WAUKESHA ENGINE NEED INFO |
| 33 | AMOCO PRODUCTION CO SALVADOR COMP STA | WAUKESHA VRG-155-U 20HP |
| 34 | AMOCO PRODUCTION CO ELDRIDGE 25-1 | (7) AJAX E-42 ENGINES38HP |
| 35 | AMOCO PRODUCTION CO ELDRIDGE 30-1 | (2) AJAX DP-60 ENGINES |
| 36 | AMOCO PRODUCTION CO ROBIN FRAZIER A | SCHOFIELD AUTO 31X-5 ENG. |
| 37 | AMOCO PRODUCTION CO ROBIN FRAZIER A | COLO. 32-7 #1 ENGINE |
| 38 | APACHE CORP | WAUKESHA F2895G ENGINE |
| 39 | APACHE CORP | AJAX DPC-180 SALVADOR1 |
| 40 | APACHE CORP | AJAX DPC-360 #80750 ENG. |
| 41 | APACHE CORP | WAUKESHA L7042GL 1000HP |
| 42 | APACHE CORP | AJAX 600 HP |
| 43 | APACHE CORP | AJAX DPC-60 COMPRESSOR |
| 44 | APACHE CORPORATION | SAWMILL |
| 45 | BEE LINE GAS COMPANY | S. UTE 24-10 ENGINE |
| 46 | BEE LINE GAS COMPANY | BONDAD 34-10 #4-25 ENGINE |
| 47 | BEE LINE GAS COMPANY | COLO. 32-7 #5 ENGINE |
| 48 | BEE LINE GAS COMPANY | COLO. 32-7 #4 ENGINE |
| 49 | BLASTING & MINING INC | ORE CRUSHER |
| 50 | BEE LINE GAS COMPANY | S. UTE 24-10 ENGINE |
| 51 | BLASTING & MINING INC | TEEPEE WOOD BURNER-SOUTH |
| 52 | BLASTING & MINING INC | TEEPEE WOOD BURNER-NORTH |
| 53 | BLASTING & MINING INC | COMBUSTION SOURCES (FOUR) |
| 54 | BLASTING & MINING INC | MINE PORTAL HEATER |
| 55 | CELSIUS ENERGY | PLANT INLET HEATER |
| 56 | CELSIUS ENERGY | HOT OIL HEATER |
| 57 | CELSIUS ENERGY | PRODUCTION TEST PACK HTR. |
| 58 | CELSIUS ENERGY | WAUKESHA ENG FOR INJ PUMP |
| 59 | CELSIUS ENERGY | CATERPILLAR SN: 71B900 |
| 60 | CELSIUS ENERGY CO | WAUKESHA SN: 398948 |

**Table B-2. Existing Colorado Emission Sources Represented by Background Data
(continued)**

| Source Count | Facility Name | Source Description |
|--------------|------------------------------------------|---------------------------|
| 61 | CELSIUS ENERGY CO CUTTHROAT WELL 5 SPA | (2)CAT 3512 743HP ENGINES |
| 62 | CELSIUS ENERGY CO CUTTHROAT WELL 5 SPA | SMITH GLYCOL REBOILER |
| 63 | CELSIUS ENERGY CO CUTTHROAT WELL 5 SPA | WAUKESHA L7042G ENGINE |
| 64 | CELSIUS ENERGY CO CUTTHROAT WELL 5 SPA | WAUKESHA SN: 399354 |
| 65 | CELSIUS ENERGY CO CUTTHROAT WELL 5 SPA | WAUKESHA SN: 400640 |
| 66 | CELSIUS ENERGY CO CUTTHROAT WELL 5 SPA | WAUKESHA SN: 400637 |
| 67 | EL PASO NATURAL GAS CO FLORIDA RIVER CS | WAUKESHA ENGINE 400012 |
| 68 | EL PASO NATURAL GAS CO FLORIDA RIVER CS | WAUKESHA ENGINE 400013 |
| 69 | EL PASO NATURAL GAS CO FLORIDA RIVER CS | WAUKESHA VRG 330, 400793 |
| 70 | ELM RIDGE EXPLORATION | EMERGENCY FLARE-VFOS03 FC |
| 71 | FUEL RESOURCES DEV CO FORTY FOUR CANYON | 8 ENGINES |
| 72 | FUEL RESOURCES DEV CO HIGH FLUME 10 9 | WILLIAMS INLET HTR. 854-1 |
| 73 | FUEL RESOURCES DEV CO HIGH FLUME 10 9 | WLLMS HOT OIL HTR #854-1 |
| 74 | FUEL RESOURCES DEV CO HIGH FLUME 10 9 | CE NATCO PROD PACK HEATER |
| 75 | FUEL RESOURCES DEV CO LA POSTA#3/S.UTE56 | TURBINE #2 (SEE PT 005) |
| 76 | FUEL RESOURCES DEV CO MCCULLOCH 20 2 | 300 HP NATURAL GAS ENGINE |
| 77 | FUEL RESOURCES DEV CO MCCULLOCH 21 1 | WAUKESHA F29GL 470HP |
| 78 | FUEL RESOURCES DEV CO MCCULLOCH 28 1 | WAUKESHA F2895 GL 549 HP |
| 79 | FUEL RESOURCES DEV CO MCCULLOCH 28 1 | WAUKESHA F24GL 300HP |
| 80 | FUEL RESOURCES DEV CO S UTE 10 2 | ROCK CRUSHER, GENERATOR |
| 81 | FUEL RESOURCES DEV CO S UTE 15 1 | ROCK CRUSHER, GENERATOR |
| 82 | FUEL RESOURCES DEV CO S UTE 16 5 WELL | WAUKESHA VRG220U ENGINE |
| 83 | FUEL RESOURCES DEV CO SAWMILL CANYON | CATERPILLAR G3412TA LCR |
| 84 | FUEL RESOURCES DEV CO SAWMILL CANYON | INLET HEATER |

**Table B-2. Existing Colorado Emission Sources Represented by Background Data
(continued)**

| Source Count | Facility Name | Source Description |
|--------------|----------------------------------------|---------------------------|
| 85 | FUEL RESOURCES DEV CO SED FEDERAL4 1 | SAND & GRAVEL PIT |
| 86 | FUEL RESOURCES DEV CO SFC LA PALOMA1 2 | CATERPILLAR NAT GAS GENER |
| 87 | GEODYNE RESOURCES INC | SOLAR CENTAUR SN: 4440C |
| 88 | GEODYNE RESOURCES INC | AJAX DP115 PUMPJACK ENG. |
| 89 | GLEN WELLS CONST | GLYCOL DEHYDRATOR SKID #1 |
| 90 | HALLIBURTON ENERGY SVCS | ICE AJAX DPC-105 89HP COM |
| 91 | HOMESTAKE MINING CO BULLDOG MOUNTAIN | WAUKESHA 135 47HP #66486 |
| 92 | HOMESTAKE MINING CO BULLDOG MOUNTAIN | (3) FORD/CSG649 ENG |
| 93 | HOMESTAKE MINING CO BULLDOG MOUNTAIN | (2) AJAX E-42 38HP ICE'S |
| 94 | HOOD MORTUARY | WAUKESHA ENGINE 400019 |
| 95 | HOOD MORTUARY | WAUKESHA ENGINE 399749 |
| 96 | LMH ENVIRONMENTAL INC | WAUKESHA 140 ENGINE 55HP |
| 97 | MARKWEST RESOURCES INC | CLOSED AMINE SWETNG PLANT |
| 98 | MARKWEST RESOURCES INC | CATERPILLAR, SN:71B1982 |
| 99 | MERCY MEDICAL CTR | WAUKESHA 330 ENGINE 47HP |
| 100 | MID AMERICA PIPELINE CO DOLORES STA | WOOD BOILER |
| 101 | MID AMERICA PIPELINE CO DOLORES STA | INLET HEATER OIL-FIRED |
| 102 | MID AMERICA PIPELINE CO DOLORES STA | GLYCOL REBOILER H-102A |
| 103 | MID AMERICA PIPELINE CO DOLORES STA | GLYCOL REBOILER H-102B |
| 104 | MID AMERICA PIPELINE CO IGNACIO STA | INLET HEATER OIL-FIRED |
| 105 | MID AMERICA PIPELINE CO IGNACIO STA | GLYCOL REBOILER H-102A |
| 106 | MID AMERICA PIPELINE CO IGNACIO STA | GLYCOL REBOILER H-102B |
| 107 | NORTHWEST PIPELINE CORP PLEASANT VIEW | WILLIAMS LINE HEATER |
| 108 | NORTHWEST PIPELINE CORP PLEASANT VIEW | CATERPILLAR,SN:6NB00535 |
| 109 | OHIO MATCH CO | WAUKESHA VR310 ENGINE |
| 110 | PABLO OPERATING CO | GENCO BURNER - NO 2 OIL |
| 111 | PABLO OPERATING CO JAQUES #5-F WELL | GENCO BURNER - NO 2 OIL |
| 112 | PALO PETROLEUM | (3)RECIP. I.C. ENGINES |
| 113 | PETROGULF CORP | CUMMINS GTA-743A 240HP |
| 114 | PONDEROSA TIMBER | AJAX DP-70 ENGINE 60HP |
| 115 | PONDEROSA TIMBER | WAUKESHA 140 ENGINE 55HP |
| 116 | PUBLIC SERVICE CO TIFFANY STATION | FORD LSG-875 60HP ENGINE |

**Table B-2. Existing Colorado Emission Sources Represented by Background Data
(continued)**

| Source Count | Facility Name | Source Description |
|--------------|--------------------------------------------|---------------------------|
| 117 | PUBLIC SERVICE CO TIFFANY STATION | WAUKESHA ENG SN:YN3969 |
| 118 | QUESTAR EXPLORATION & PROD CUTTHROAT A | GLYCOL DEHYDRATOR |
| 119 | QUESTAR EXPLORATION & PROD CUTTHROAT A | NAT GAS FIRED IC ENGINE |
| 120 | QUESTAR EXPLORATION & PROD CUTTHROAT A | NAT GAS FIRED IC ENGINE |
| 121 | QUESTAR EXPLORATION & PROD CUTTHROAT A | WAUKESHA SN: 399817 |
| 122 | QUESTAR EXPLORATION & PROD CUTTHROAT A | WAUKESHA SN: 399504 |
| 123 | QUESTAR EXPLORATION & PROD CUTTHROAT A | WAUKESHA SN: 399508 |
| 124 | QUESTAR EXPLORATION & PROD CUTTHROAT A | WAUKESHA SN: 400636 |
| 125 | QUESTAR EXPLORATION & PROD CUTTHROAT A | WAUKESHA SN: 400639 |
| 126 | QUESTAR EXPLORATION & PROD CUTTHROAT A | WAUKESHA SN: 399506 |
| 127 | QUESTAR EXPLORATION & PROD CUTTHROAT A | WAUKESHA SN: 399819 |
| 128 | SG INTERESTS 1, LTD - SOUTH IGNACIO CDP | FORD LSG-423 25HP ENGINE |
| 129 | SHELL CO2 COMPANY, LTD. HOVENWEEP | CIP 50 BBL/DAY STEAMER |
| 130 | SHELL CO2 COMPANY, LTD. HOVENWEEP | CIP 50BBL/DAY STEAMER |
| 131 | SHELL CO2 COMPANY, LTD. HOVENWEEP | (2)38HP AJAX E-42 ENGINES |
| 132 | SHELL WESTERN E&P INC MCELMO DOME | GLYCOL DEHYDRATOR |
| 133 | SMITH ENERGY LP 1988 CACHE OIL FIELD | UNIT 3 LINE HEATER |
| 134 | SOUTHWEST HEALTH SYSTEM | (4) AJAX E42 38HP ENGINES |
| 135 | SOUTHWEST HEALTH SYSTEM | WAUKESHA 145 ENGINE 64HP |
| 136 | TRANSCOLORADO GAS TRANSMISSION CO | SOLAR CENTAUR SN: 4441C |
| 137 | TRANSWESTERN PIPELINE CO LA PLATA 'A' | FLARE PIT |
| 138 | TRANSWESTERN PIPELINE CO LA PLATA 'A' | WAUK NAT GAS ENG @ 549 HP |
| 139 | TRANSWESTERN PIPELINE CO LA PLATA 'A' | WAUK VRG155U PUMP FOR H2O |
| 140 | UTE E CENTRAL DELIVERY POINT | CATERPILLAR 3304 70HP ICE |
| 141 | UTE E CENTRAL DELIVERY POINT | CAT 342T ENG SN 71R540 |
| 142 | VASTAR RESOURCES INC. WELL 22-4; 33-10 | FORD CSG-649 46HP ENGINE |

**Table B-2. Existing Colorado Emission Sources Represented by Background Data
(continued)**

| Source Count | Facility Name | Source Description |
|--------------|----------------------------------------|---------------------------|
| 143 | WEST GAS GATHERING INC | DEHYDRATOR #1, BONDAD 1 |
| 144 | WEST GAS GATHERING INC | DEHYDRATOR 2, BONDAD 2 |
| 145 | WEST GAS GATHERING INC | WAUKESHA L7042GL,BONDAD 2 |
| 146 | WEST GAS GATHERING INC | WAUKESHA L7042GL, BONDAD2 |
| 147 | WEST GAS GATHERING INC | AJAX DPC-280 ENG,SN:77939 |
| 148 | WEST GAS GATHERING INC | GENERAC 74GN, MODEL:CG070 |
| 149 | WEST GAS GATHERING INC | GENERAC 74GN,MODEL:CG070 |
| 150 | WILLIAMS FIELD SERVICES BONDAD 33-9 #3 | INLET HEATER - OIL FIRED |
| 151 | WILLIAMS FIELD SERVICES IGNACIO B PLT | TULDA HEATER DN 96222 |
| 152 | WILLIAMS FIELD SERVICES IGNACIO B PLT | FORD CSG649 V6 ENG 60HP |
| 153 | WILLIAMS FIELD SERVICES IGNACIO B PLT | FORD CSG649 V6 ENG 60HP |
| 154 | WILLIAMS FIELD SERVICES IGNACIO B PLT | AJAX E-42 ENGINE 36HP |
| 155 | WILLIAMS FIELD SERVICES IGNACIO B PLT | ICE: WAUKESHA 7042GL |
| 156 | WILLIAMS FIELD SVCS | AJAX DPC-80 COMPRESSOR |
| 157 | WILLIAMS FIELD SVCS 33 7 24 STEAMER | TURBINE #1 (SEE PT 004) |
| 158 | WILLIAMS FIELD SVCS 33 8 22 STEAMER | GRAVEL MINING OPERATION |
| 159 | WILLIAMS FIELD SVCS 33 8 5 STEAMER | GRAVEL MINING OPERATION |
| 160 | WILLIAMS FIELD SVCS BONDAD 33 9 10 | FORD CSG-649 46HP ENGINE |
| 161 | WILLIAMS FIELD SVCS BONDAD 33 9 11 | (3) SUPERIOR 8G825'S |
| 162 | WILLIAMS FIELD SVCS BONDAD 33 9 5 | AJAX DPC-300 243HP ENGINE |
| 163 | WILLIAMS FIELD SVCS BUENA SUERTA | CATERPILLAR G3306 150 HP |
| 164 | WILLIAMS FIELD SVCS BUENA SUERTA | AJAX DPC600 ICE SN:79631 |
| 165 | WILLIAMS FIELD SVCS BUENA SUERTA | WAUKESHA 7042GL |
| 166 | WILLIAMS FIELD SVCS BUENA SUERTA | WAUKESHA 7042GL SN 402863 |
| 167 | WILLIAMS FIELD SVCS CO 32 7 11 | EVAPORATOR HEATER |
| 168 | WILLIAMS FIELD SVCS IGNACIO 33 7 18 | CAT 3304 COMPRESSR ENGINE |
| 169 | WILLIAMS FIELD SVCS IGNACIO 33 7 SITE | CATERPILLAR 398TA 450 HP |
| 170 | WILLIAMS FIELD SVCS IGNACIO 33-7#25 | WAUKESHA F817GU IC ENGINE |

Table B-3. Colorado Reasonably Foreseeable Emission Sources

| Source Count | Facility Name | Source Description |
|--------------|---------------------------------------------|---------------------------|
| 1 | SG INTERESTS I LTD | CREMATOR A11-1801 |
| 2 | 44 CANYON LLC C/O HALLWOOD PETROLEUM INC | TURBINE SMB1683 GP20388-3 |
| 3 | EL PASO NATURAL GAS COMPANY IGNACIO FLD | TURBINE #1 MD:10-T1302 |
| 4 | EL PASO NATURAL GAS COMPANY IGNACIO FLD | TURBINE SN:0528521R |
| 5 | AMOCO PRODUCTION CO HOTT INJECTION STA | WAUKESHA ENGINE, 401574 |
| 6 | GLEN WELLS CONST | RADCO AMINE HEATER #1 |
| 7 | HALLIBURTON ENERGY SVCS | SOLAR 10-T1300 |
| 8 | AMERADA HESS CORP CRIGLER UTE LEASE | WAUKESHA VRG 300, 389203 |
| 9 | AMERADA HESS CORP IGNACIO BLANCO FIELD | WAUKESHA VRG 330, 389791 |
| 10 | AMERADA HESS CORP HERRERA LEASE | WAUKESHA VRG 330, 399609 |
| 11 | AMOCO PRODUCTION CO NITROGEN INJECTION | WAUKESHA VRG 330, 386468 |
| 12 | QUESTAR EXPLORATION & PROD MIR 4-31 | FORD CSG-649 SN:17772 ICE |
| 13 | SG INTEREST I LTD | AJAX ENG. SN: HRM 85-317T |
| 14 | WILLIAMS FIELD SERVICES IGNACIO B PLT | CAT G3516TA 1085HP COMP#4 |
| 15 | WILLIAMS FIELD SERVICES IGNACIO B PLT | WAUKESHA L5790GL |
| 16 | AMERADA HESS CORP JULIAN GAS UNIT 2 | AJAX E-42 SJBC-CMA-001 |
| 17 | RMI ENVIRONMENTAL SVC INC | AJAX M/N E-42 SN: 65254 |
| 18 | RMI ENVIRONMENTAL SVCS | AJAX DPC 360LE SN 403660 |
| 19 | MERCY MEDICAL CTR | AJAX DPC 360 ENGINE |
| 20 | MOBIL EXPLORATION BONDAD 34 10 4 25 | WAUKESHA L 5790 GL ICE |
| 21 | AMERADA HESS CORP DAVIS GAS UNIT | AJAX M/N DPC 180 SN 75078 |
| 22 | MOBIL EXPLORATION CO 32 7 4 &S UTE42 4 | NAT GAS ENG |
| 23 | MOBIL EXPLORATION CO 32 7 4 &S UTE42 4 | NAT GAS ENG |
| 24 | 44 CANYON LLC C/O HALLWOOD PETROLEUM INC | WAUKESHA ICE H-24GL |
| 25 | AMERADA HESS CORP | AJAX 8 1/2 CMA SN: 60705 |
| 26 | AMERADA HESS CORP HAHN GAS UNIT A 2 | FORD CSG 879 SN 09168C-15 |
| 27 | AMERADA HESS CORP HARMON GAS UNIT A 2 | AJAX MN DP60 SJBC-DP60-01 |
| 28 | WILLIAMS FIELD SVCS MCCARVILLE 1 STA | NAT GAS ENG & 1068 HP |
| 29 | APACHE CORPORATION | NAT GAS ENG |

Table B-3. Colorado Reasonably Foreseeable Emission Sources (continued)

| Source Count | Facility Name | Source Description |
|--------------|------------------------------------------|---------------------------|
| 30 | AMOCO PRODUCTION CO FLORIDA RIVER COMP | WAUKESHA L7042 GL |
| 31 | AMOCO PRODUCTION CO FLORIDA RIVER COMP | CATERPILLAR G399TA ENGINE |
| 32 | STROEHECKER EXCAVATION | CATERPILLAR 398TA MOD JRG |
| 33 | STROEHECKER EXCAVATION | AJAX DPC 360LE SN 403660 |
| 34 | AMOCO PRODUCTION CO SALVADOR COMP STA | C-BROOKS BOILER SN:47334 |
| 35 | AMOCO PRODUCTION CO | ANIMAL CREMATOR NAT GAS |
| 36 | WILLIAMS FIELD SVCS BUENA SUERTA | CATERPILLAR CA 95 3306NA |
| 37 | AMOCO PRODUCTION CO AREA 7 INJECTION STA | WAUKESHA 12V AT27GL |
| 38 | AMOCO PRODUCTION CO AREA 7 INJECTION STA | WAUKESHA 12V AT27GL ENGIN |
| 39 | AMOCO PRODUCTION CO HIGH FLUME CS,AREA 6 | WAUKESHA 12V AT27GL |
| 40 | AMOCO PRODUCTION CO HIGH FLUME CS,AREA 6 | WAUKESHA 12V AT27GL |
| 41 | AMOCO PRODUCTION CO HIGH FLUME CS,AREA 6 | WAUKESHA 12V AT27GL 2768H |
| 42 | WILLIAMS FIELD SERVICES LONE PINE | CATERPILLAR 3306 90HP ICE |
| 43 | AMERADA HESS CORP F U TERRELL GAS UN 2 | MIX ASPHALT PLANT BARBER |
| 44 | STROEHECKER EXCAVATION | FORD LSG 875 ENGINE |
| 45 | MERCY MEDICAL CTR | CAT NAT ENG RATED @ 323HP |
| 46 | WESTERN MOBILE NORTHERN | ICE AJAX DPC-230 184 HP |
| 47 | ANG/FUEL RES.DEV.CO 44 CANYON COMP.STATN | CAT SN: C111614EK03197 |
| 48 | ANG/FUEL RES.DEV.CO 44 CANYON COMP.STATN | CATERPILLAR G3512LE 7532 |
| 49 | AMOCO PRODUCTION CO WHEELER COMP STA | COOPER SN:83937 |
| 50 | WILLIAMS FIELD SVCS LATERAL 2 B STA | CAT SN: C111614EK03197 |
| 51 | AMERADA HESS CORP 11 I C ENGINES | WAUKESHA MODEL F-1197-G |
| 52 | WILLIAMS FIELD SVCS TRUNK J SITE | TO2 SOLAR CENTAUR 60T700S |
| 53 | 44 CANYON LLC C/O HALLWOOD PETROLEUM | NAT GAS ENG RATED @ 514 H |
| 54 | 44 CANYON LLC C/O HALLWOOD PETROLEUM | NAT GAS ENG |
| 55 | 44 CANYON LLC C/O HALLWOOD PETROLEUM | 7 COMPRESSOR ENGINES |
| 56 | AMOCO PRODUCTION CO REA 1 DISPSL | TURBINE #2: GE,SN: 282515 |

Table B-3. Colorado Reasonably Foreseeable Emission Sources (continued)

| Source Count | Facility Name | Source Description |
|--------------|---------------------------------------------|---------------------------|
| 57 | NORTHWEST PIPELINE CORP LA PLATA B STA | STEAM BOILER #3 |
| 58 | NORTHWEST PIPELINE CORP LA PLATA B STA | TURBINE #1-GE,SN: 282514 |
| 59 | NORTHWEST PIPELINE CORP LA PLATA B STA | BOILER - NATGAS FIRED |
| 60 | PALO PETROLEUM | SOLAR TURBINE 2470BHP ENG |
| 61 | AMOCO PRODUCTION COMPANY | NG HEATER AMINE 39.96BTUH |
| 62 | WILLIAMS FIELD SERVICES IGNACIO B PLT | NAT GAS ENG RATED 1380 HP |
| 63 | AMOCO PRODUCTION CO HELEN CRAIG G.U.#1 | ICE SN:4EK01868 |
| 64 | AMOCO PRODUCTION CO MCCAW G.U. D#1 | NAT GAS ENGINE |
| 65 | AMOCO PRODUCTION CO PICCOLI G.U.A #1 | CAT G3516 SN:4EK01677 |
| 66 | AMOCO PRODUCTION CO RAYMOND KONN GUA6#1 | CAT G3516 SN: 4EKO1675 |
| 67 | FUEL RESOURCES DEV CO MCCULLOCH 20 2 | 300 HP NATURAL GAS ENGINE |
| 68 | AMOCO PRODUCTION CO ROBERT DULIN G.U.C#1 | RICHMOND FOXY WDW W/ICE |
| 69 | 44 CANYON LLC C/O HALLWOOD PETROLEUM INC | WAUK L7042GL, SN:402862 |
| 70 | MARKWEST RESOURCES INC CARLILE COMP. | WAUK 7042 GL, SN: 402863 |
| 71 | MARKWEST RESOURCES INC CARLILE COMP. | WAUKESHA L7042GL |
| 72 | APACHE CORPORATION | WAUKESHA L9390 GL 1460 HP |
| 73 | UTE E CENTRAL DELIVERY POINT | WAUKESHA MODEL 1905 170HP |
| 74 | 44 CANYON LLC C/O HALLWOOD PETROLEUM INC | NAT GAS ENG RATED AT 89 H |
| 75 | UTE E CENTRAL DELIVERY POINT | CATERPILLAR 3304 ENGINE |
| 76 | AMOCO PRODUCTION CO MAYFIELD COMP STA | AJAX DPC-360 SERIAL#80754 |
| 77 | AMOCO PRODUCTION CO MAYFIELD COMP STA | AJAX DPC-800 SERIAL#82576 |
| 78 | AMOCO PRODUCTION CO FLORIDA RIVER COMP | WAUK, L70042GL SN:C11100 |
| 79 | 44 CANYON LLC C/O HALLWOOD PETROLEUM INC | CATERPILLAR NAT GAS ENG |
| 80 | 44 CANYON LLC C/O HALLWOOD PETROLEUM INC | NAT GAS ENG 89 HP |
| 81 | NATURAL GAS PROCESSING CO | WAUKESHA RICH BURN MOD F8 |
| 82 | AMOCO PRODUCTION CO RICHARDSON G.U.G#1 | WAUKESHA F1197 |
| 83 | FUEL RESOURCES DEV CO DEER CANYON UTE 16 | CATERPILLAR G3304NA |

Table B-4. Colorado Emission Source Modeling Input Values

| Source Count | Source Description | Unit ID | NOx Emission Rate (g/s) | UTM | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|------------------------------------------|---------------------------|-------------------------|--------------|---------------|------------------|--------------|--------------------|-----------|------------|-----------|----------------|
| | | | | Easting (km) | Northing (km) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 1 | 44 CANYON LLC C/O HALLWOOD PETROLEUM INC | TURBINE SMB1683 GP20388-3 | 0.5 | 196.191 | 4146.440 | 6.1 | 0.5 | 79.9 | 750 | N/A | N/A | 7068 |
| 2 | 44 CANYON LLC C/O HALLWOOD PETROLEUM INC | WAUK L7042GL, SN:402862 | 0.4 | 265.992 | 4104.626 | 5.5 | 0.3 | 30.6 | 255 | N/A | N/A | 6396 |
| 3 | 44 CANYON LLC C/O HALLWOOD PETROLEUM INC | CATERPILLAR NAT GAS ENG | 0.2 | 273.753 | 4126.367 | 4.3 | 0.3 | 5.2 | 865 | N/A | N/A | 7196 |
| 4 | 44 CANYON LLC C/O HALLWOOD PETROLEUM INC | WAUKESHA ICE H-24GL | 0.4 | 240.152 | 4099.231 | 4.9 | 0.2 | 38.4 | 255 | N/A | N/A | 6426 |
| 5 | 44 CANYON LLC C/O HALLWOOD PETROLEUM INC | NAT GAS ENG RATED AT 89 H | 0.2 | 269.053 | 4128.105 | 4.9 | 0.2 | 12.8 | 255 | N/A | N/A | 7013 |
| 6 | 44 CANYON LLC C/O HALLWOOD PETROLEUM INC | NAT GAS ENG 89 HP | 0.3 | 273.753 | 4126.367 | 4.9 | 0.2 | 12.8 | 548 | N/A | N/A | 7196 |
| 7 | 44 CANYON LLC C/O HALLWOOD PETROLEUM INC | SATURN T-1300 TURBINE #2 | 0.5 | 252.500 | 4113.700 | 7.0 | 0.5 | 80.6 | 765 | N/A | N/A | 6511 |
| 8 | 44 CANYON LLC C/O HALLWOOD PETROLEUM INC | CATERPILLAR 3304 ENG 70HP | 0.3 | 253.000 | 4110.000 | 2.1 | 0.1 | 11.9 | 844 | N/A | N/A | 6711 |
| 9 | 44 CANYON LLC, C/O HALLWOOD PETROLEUM | NAT GAS ENG RATED @ 514 H | 0.3 | 252.700 | 4114.400 | 4.9 | 0.2 | 29.2 | 255 | N/A | N/A | 6596 |
| 10 | 44 CANYON LLC, C/O HALLWOOD PETROLEUM | NAT GAS ENG | 0.2 | 252.700 | 4114.400 | 4.9 | 0.2 | 29.2 | 255 | N/A | N/A | 6596 |
| 11 | 44 CANYON LLC, C/O HALLWOOD PETROLEUM | GE,MODEL M-3142, TURBINE | 3.7 | 252.700 | 4114.400 | 13.7 | 1.1 | 4.3 | 755 | N/A | N/A | 6596 |
| 12 | 44 CANYON LLC, C/O HALLWOOD PETROLEUM | 7 COMPRESSOR ENGINES | 28.7 | 252.700 | 4114.400 | 7.6 | 0.6 | 0.0 ^(a) | 672 | N/A | N/A | 6596 |

N/A Not available

^(a) Representative value assumed in the modeling

Table B-4. Colorado Emission Source Modeling Input Values (continued)

| Source Count | Source Description | Unit ID | NOx Emission Rate (g/s) | UTM | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|-----------------------------------------|---------------------------|-------------------------|--------------|---------------|------------------|--------------|--------------------|-----------|------------|-----------|----------------|
| | | | | Easting (km) | Northing (km) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 13 | AMERADA HESS CORP | AJAX 8 1/2 CMA SN: 60705 | 0.1 | 240.600 | 4116.400 | 0.6 | 0.1 | 0.0 ^(a) | 255 | N/A | N/A | 6796 |
| 14 | AMERADA HESS CORP 11 I C ENGINES | WAUKESHA MODEL F-1197-G | 0.5 | 252.200 | 4101.100 | 3.4 | 0.2 | 40.6 | 255 | N/A | N/A | 7131 |
| 15 | AMERADA HESS CORP DAVIS GAS UNIT | AJAX M/N DPC 180 SN 75078 | 0.5 | 239.000 | 4116.500 | 0.6 | 0.1 | 50.8 | 255 | N/A | N/A | 6813 |
| 16 | AMERADA HESS CORP F U TERRELL GAS UN 2 | MIX ASPHALT PLANT BARBER | 0.0 | 248.600 | 4141.300 | 9.1 | 2.3 | 3.2 | 366 | N/A | N/A | 6596 |
| 17 | AMERADA HESS CORP HAHN GAS UNIT A 2 | FORD CSG 879 SN 09168C-15 | 0.2 | 240.600 | 4116.400 | 0.6 | 0.1 | 50.8 | 255 | N/A | N/A | 6796 |
| 18 | AMERADA HESS CORP HARMON GAS UNIT A 2 | AJAX MN DP60 SJBC-DP60-01 | 0.2 | 240.600 | 4116.400 | 0.6 | 0.1 | 50.8 | 255 | N/A | N/A | 6796 |
| 19 | AMERADA HESS CORP JULIAN GAS UNIT 2 | AJAX E-42 SJBC-CMA-001 | 0.1 | 237.400 | 4116.500 | 0.6 | 0.1 | 50.8 | 255 | N/A | N/A | 7373 |
| 20 | AMOCO PROD. CO. - J.B. GARDNER A #1 | FORD CSG-649 | 0.3 | 235.500 | 4107.000 | 1.5 | 0.1 | 22.0 | 644 | N/A | N/A | 6872 |
| 21 | AMOCO PRODUCTION - EVELYN PAYNE GU #1 | SOLAR TAURUS TURBINE #1 | 2.1 | 252.500 | 4114.300 | 15.2 | 1.1 | 30.5 | 450 | N/A | N/A | 6596 |
| 22 | AMOCO PRODUCTION - HENRICKSON UNIT B #1 | (180) PORTABLE 42HP COMPS | 14.0 | 250.000 | 4100.000 | 2.4 | 0.2 | 0.0 ^(a) | 922 | N/A | N/A | 6629 |
| 23 | AMOCO PRODUCTION - HENRICKSON UNIT B #1 | CUMMINS GTA-743A 240HP | 0.7 | 239.500 | 4099.400 | 2.4 | 0.1 | 31.2 | 755 | N/A | N/A | 6396 |
| 24 | AMOCO PRODUCTION - SO. UTE TRIBAL F#1 | SATURN T-1300 TURBINE #3 | 0.5 | 252.500 | 4113.700 | 7.0 | 0.5 | 80.6 | 765 | N/A | N/A | 6511 |
| 25 | AMOCO PRODUCTION CO | COOPER GMVH COMP ENGINE | 1.7 | 193.556 | 4155.430 | 12.8 | 0.7 | 34.4 | 561 | N/A | N/A | 7570 |

N/A Not available

^(a) Representative value assumed in the modeling

Table B-4. Colorado Emission Source Modeling Input Values (continued)

| Source Count | Source Description | Unit ID | NOx Emission Rate (g/s) | UTM | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|----------------------------------------|---------------------------|-------------------------|--------------|---------------|--------------------|--------------------|--------------------|-----------|------------|-----------|----------------|
| | | | | Easting (km) | Northing (km) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 26 | AMOCO PRODUCTION CO | ANIMAL CREMATOR NAT GAS | 0.0 | 245.700 | 4124.300 | 5.2 | 0.3 | 10.1 | 700 | N/A | N/A | 6498 |
| 27 | AMOCO PRODUCTION CO PICNIC FLATS | AJAX DPC-360 ENGINE | 0.9 | 227.560 | 4105.358 | 6.1 | 0.3 | 40.8 | 644 | N/A | N/A | 6471 |
| 28 | AMOCO PRODUCTION CO PICNIC FLATS | S029 AMINE REGENERATOR | 0.6 | 252.700 | 4114.400 | 18.3 | 1.4 | 13.5 | 444 | N/A | N/A | 6596 |
| 29 | AMOCO PRODUCTION CO PICNIC FLATS | E. DEHYDRATOR GLYCOL RBLR | 0.0 | 252.700 | 4114.400 | 4.3 | 0.2 | 0.0 | 866 | N/A | N/A | 6596 |
| 30 | AMOCO PRODUCTION CO PICNIC FLATS | AJAX DPC 360 LE | 0.4 | 241.000 | 4111.300 | 6.7 | 0.3 | 15.1 | 255 | N/A | N/A | 6544 |
| 31 | AMOCO PRODUCTION CO PICNIC FLATS | AJAX DPC-180 COMP. ENGINE | 0.2 | 241.000 | 4111.300 | 6.1 | 0.3 | 6.8 | 511 | N/A | N/A | 6544 |
| 32 | AMOCO PRODUCTION CO PICNIC FLATS | GAS TURB SOLAR 34.81E6BTU | 0.9 | 252.700 | 4114.400 | 9.1 | 1.0 | 52.5 | 704 | N/A | N/A | 6596 |
| 33 | AMOCO PRODUCTION CO PICNIC FLATS | AJAX DPC 300, SN: 75514 | 0.3 | 241.000 | 4111.300 | 6.1 | 0.2 | 13.7 | 522 | N/A | N/A | 6544 |
| 34 | AMOCO PRODUCTION CO PICNIC FLATS | FORD CSG-649 46 HP | 0.1 | 241.000 | 4111.300 | 0.6 | 0.1 | 151.2 | 644 | N/A | N/A | 6544 |
| 35 | AMOCO PRODUCTION CO PICNIC FLATS | CATERPILLAR 3304 70HP ICE | 0.3 | 261.200 | 4108.200 | 2.1 | 0.1 | 11.9 | 866 | N/A | N/A | 6694 |
| 36 | AMOCO PRODUCTION CO PICNIC FLATS | CATERPILLAR 3304 ENGINE | 0.3 | 267.600 | 4109.500 | 2.1 | 0.1 | 11.9 | 866 | N/A | N/A | 6504 |
| 37 | AMOCO PRODUCTION CO HELEN CRAIG G.U.#1 | ICE SN:4EK01868 | 0.7 | 253.221 | 4109.797 | 0.0 | 0.0 ^(a) | 0.0 ^(a) | 294 | N/A | N/A | 6711 |
| 38 | AMOCO PRODUCTION CO MCCAW G.U. D#1 | NAT GAS ENGINE | 0.7 | 253.221 | 4109.797 | 6.4 | 0.4 | 24.4 | 255 | N/A | N/A | 6711 |
| 39 | AMOCO PRODUCTION CO PICCOLI G.U.A #1 | CAT G3516 SN:4EK01677 | 0.7 | 253.221 | 4109.797 | 0.0 ^(a) | 0.0 ^(a) | 0.0 ^(a) | 294 | N/A | N/A | 6711 |
| 40 | AMOCO PRODUCTION CO PINE RIVER 02-29 | RICHARD FOXY WDW W/ICE | 1.2 | 260.000 | 4109.100 | 2.4 | 0.2 | 18.7 | 671 | N/A | N/A | 6796 |

N/A Not available

^(a) Representative value assumed in the modeling

Table B-4. Colorado Emission Source Modeling Input Values (continued)

| Source Count | Source Description | Unit ID | NOx Emission Rate (g/s) | UTM | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|------------------------------------------|---------------------------|-------------------------|--------------|---------------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | | Easting (km) | Northing (km) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 41 | AMOCO PRODUCTION CO RAYMOND KOON GUA6#1 | CAT G3516 SN: 4EK01675 | 0.7 | 253.221 | 4109.797 | 6.4 | 0.4 | 24.4 | 255 | N/A | N/A | 6711 |
| 42 | AMOCO PRODUCTION CO RICHARDSON G.U.G#1 | WAUKESHA F1197 | 0.2 | 277.288 | 4105.998 | 3.0 | 0.1 | 98.2 | 255 | N/A | N/A | 6796 |
| 43 | AMOCO PRODUCTION CO - ROBERT DULIN D #1 | FORD CSG-649 | 0.3 | 235.400 | 4105.400 | 1.5 | 0.6 | 2.2 | 255 | N/A | N/A | 6790 |
| 44 | AMOCO PRODUCTION CO ROBERT DULIN G.U.#1 | WAUKESHA L 3711G_SN:4068 | 0.9 | 260.000 | 4109.100 | 3.7 | 0.2 | 42.2 | 294 | N/A | N/A | 6796 |
| 45 | AMOCO PRODUCTION CO AREA 7 INJECTION STA | WAUKESHA 12V AT27GL | 1.2 | 248.400 | 4111.600 | 8.2 | 0.6 | 30.9 | 517 | N/A | N/A | 6596 |
| 46 | AMOCO PRODUCTION CO AREA 7 INJECTION STA | WAUKESHA 12V AT27GL ENGIN | 1.2 | 248.400 | 4111.600 | 8.2 | 0.6 | 30.9 | 517 | N/A | N/A | 6596 |
| 47 | AMOCO PRODUCTION CO DURANGO AREA | WAUKESHA ENGINE #1 | 1.0 | 248.400 | 4111.600 | 8.2 | 0.6 | 24.4 | 673 | N/A | N/A | 6596 |
| 48 | AMOCO PRODUCTION CO FLORIDA RIVER COMP | WAUK, L70042GL SN:C11100 | 0.6 | 273.600 | 4104.100 | 6.1 | 0.3 | 38.0 | 727 | N/A | N/A | 6524 |
| 49 | AMOCO PRODUCTION CO FLORIDA RIVER COMP | WAUKESHA L7042 GL | 0.7 | 242.300 | 4109.900 | 6.4 | 0.3 | 50.4 | 0 | N/A | N/A | 6481 |
| 50 | AMOCO PRODUCTION CO FLORIDA RIVER COMP | CATERPILLAR G399TA ENGINE | 0.7 | 242.300 | 4109.900 | 6.7 | 0.3 | 31.9 | 664 | N/A | N/A | 6481 |
| 51 | AMOCO PRODUCTION CO FLORIDA RIVER COMP | NAT GAS ENG & 943 HP | 1.2 | 260.200 | 4110.400 | 8.2 | 0.6 | 30.9 | 671 | N/A | N/A | 6796 |
| 52 | AMOCO PRODUCTION CO HIGH FLUME CS,AREA 6 | WAUKESHA 12V AT27GL | 1.2 | 248.400 | 4111.600 | 8.2 | 0.6 | 30.9 | 671 | N/A | N/A | 6596 |

N/A Not available

^(a) Representative value assumed in the modeling

Table B-4. Colorado Emission Source Modeling Input Values (continued)

| Source Count | Source Description | Unit ID | NOx Emission Rate (g/s) | UTM | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|------------------------------------------|---------------------------|-------------------------|--------------|---------------|------------------|--------------|--------------------|-----------|------------|-----------|----------------|
| | | | | Easting (km) | Northing (km) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 53 | AMOCO PRODUCTION CO HIGH FLUME CS,AREA 6 | WAUKESHA 12V AT27GL | 1.2 | 248.400 | 4111.600 | 8.2 | 0.6 | 30.9 | 0 | N/A | N/A | 6596 |
| 54 | AMOCO PRODUCTION CO HIGH FLUME CS,AREA 6 | WAUKESHA 12V AT27GL 2768H | 1.0 | 248.400 | 4111.600 | 8.2 | 0.6 | 24.4 | 752 | N/A | N/A | 6596 |
| 55 | AMOCO PRODUCTION CO HIGH FLUME CS,AREA 6 | WAUKESHA ENGINE #2 | 1.0 | 248.400 | 4111.600 | 8.2 | 0.6 | 24.4 | 752 | N/A | N/A | 6596 |
| 56 | AMOCO PRODUCTION CO HIGH FLUME CS,AREA 6 | WAUKESHA ENGINE #3 | 1.0 | 248.400 | 4111.600 | 8.2 | 0.6 | 24.4 | 752 | N/A | N/A | 6596 |
| 57 | AMOCO PRODUCTION CO HIGH FLUME CS,AREA 6 | WAUKESHA ENGINE #4 | 6.6 | 248.400 | 4111.600 | 13.7 | 1.8 | 40.8 | 728 | N/A | N/A | 6596 |
| 58 | AMOCO PRODUCTION CO REA 1 DISPSL | TURBINE #2: GE,SN: 282515 | 0.3 | 252.700 | 4114.400 | 6.1 | 0.4 | 0.0 ^(a) | 422 | N/A | N/A | 6596 |
| 59 | AMOCO PRODUCTION CO REA 1 DISPSL | REGENERATION HEATER | 0.3 | 252.700 | 4114.400 | 1.8 | 0.1 | 116.7 | 802 | N/A | N/A | 6596 |
| 60 | AMOCO PRODUCTION CO ROBERT DULIN G.U.C#1 | RICHMOND FOXY WDW W/ICE | 0.9 | 260.000 | 4109.100 | 7.6 | 0.4 | 13.5 | 505 | N/A | N/A | 6796 |
| 61 | AMOCO PRODUCTION CO S UTE 23 2 | AJAX DPC-600, SN: 82-093P | 0.0 | 251.600 | 4126.500 | 21.3 | 0.6 | 4.1 | 466 | N/A | N/A | 7108 |
| 62 | AMOCO PRODUCTION CO SALVADOR COMP STA | C-BROOKS BOILER SN:47334 | 0.0 | 245.200 | 4129.900 | 21.3 | 0.6 | 0.9 | 466 | N/A | N/A | 6596 |
| 63 | AMOCO PRODUCTION CO SALVADOR COMP STA | C-BROOKS BOIL SN:47335 | 0.9 | 245.200 | 4129.900 | 0.9 | 0.4 | 0.0 ^(a) | 700 | N/A | N/A | 6596 |
| 64 | AMOCO PRODUCTION CO SALVADOR COMP STA | AJAX DPC-360 ENGINE | 0.6 | 259.900 | 4120.500 | 0.0 | 0.3 | 38.1 | 255 | N/A | N/A | 6855 |
| 65 | AMOCO PRODUCTION CO TIFFANY COMPRESSOR | NATURAL GAS ENGINE | 0.6 | 242.300 | 4109.900 | 0.0 | 0.3 | 38.1 | 255 | N/A | N/A | 6481 |

N/A Not available

^(a) Representative value assumed in the modeling

Table B-4. Colorado Emission Source Modeling Input Values (continued)

| Source Count | Source Description | Unit ID | NOx Emission Rate (g/s) | UTM | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|------------------------------------------|---------------------------|-------------------------|--------------|---------------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | | Easting (km) | Northing (km) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 66 | AMOCO PRODUCTION CO TIFFANY COMPRESSOR | WAUKESHA NAT GAS ENG | 6.6 | 242.300 | 4109.900 | 13.7 | 1.8 | 40.8 | 728 | N/A | N/A | 6481 |
| 67 | AMOCO PRODUCTION CO TIFFANY COMPRESSOR | WAUKESHA 3521GL | 0.3 | 242.300 | 4109.900 | 4.9 | 0.2 | 50.3 | 255 | N/A | N/A | 6481 |
| 68 | AMOCO PRODUCTION CO. - ELDRIDGE 25-2 | AJAX DP-70 60HP ENGINE | 0.1 | 238.600 | 4107.200 | 0.6 | 0.1 | 51.8 | 561 | N/A | N/A | 6862 |
| 69 | AMOCO PRODUCTION COMPANY | NG HEATER AMINE 39.96BTUH | 1.2 | 253.200 | 4115.600 | 2.1 | 0.1 | 109.1 | 603 | N/A | N/A | 6642 |
| 70 | ANG/FUEL RES.DEV.CO 44 CANYON COMP.STATN | CAT SN: C111614EK03197 | 0.7 | 251.600 | 4126.500 | 6.1 | 0.3 | 17.0 | 255 | N/A | N/A | 7108 |
| 71 | ANG/FUEL RES.DEV.CO 44 CANYON COMP.STATN | CATERPILLAR G3512LE 7532 | 0.9 | 251.600 | 4126.500 | 7.6 | 0.4 | 14.4 | 255 | N/A | N/A | 7108 |
| 72 | APACHE CORPORATION | WAUKESHA L9390 GL 1460 HP | 0.8 | 267.200 | 4106.800 | 0.9 | 0.4 | 19.0 | 255 | N/A | N/A | 6422 |
| 73 | BLASTING & MINING INC | WAUKESHA VRG22 SN:398981 | 0.1 | 262.500 | 4098.400 | 2.1 | 0.1 | 35.4 | 839 | N/A | N/A | 7006 |
| 74 | CELSIUS ENERGY CO CUTTHROAT WELL 3 | WAUKESHA VRG 220 SN 38889 | 0.1 | 254.900 | 4112.700 | 2.1 | 0.1 | 35.4 | 839 | N/A | N/A | 6596 |
| 75 | CELSIUS ENERGY CO CUTTHROAT WELL 3 | ICE WAUKESHA VRG 220 | 0.1 | 244.200 | 4117.500 | 1.8 | 0.1 | 35.4 | 839 | N/A | N/A | 6344 |
| 76 | CELSIUS ENERGY CO CUTTHROAT WELL 4 | WAUKESHA SN: 400638 | 0.3 | 252.000 | 4110.000 | 2.1 | 0.9 | 85.6 | 255 | N/A | N/A | 6776 |
| 77 | CELSIUS ENERGY CO CUTTHROAT WELL 5 SPA | WAUKEHSA 220 SN:396333 | 0.1 | 257.800 | 4103.100 | 2.1 | 0.1 | 35.4 | 839 | N/A | N/A | 7124 |

N/A Not available

^(a) Representative value assumed in the modeling

Table B-4. Colorado Emission Source Modeling Input Values (continued)

| Source Count | Source Description | Unit ID | NOx Emission Rate (g/s) | UTM | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|-----------------------------------------|---------------------------|-------------------------|--------------|---------------|------------------|--------------------|--------------------|-----------|------------|-----------|----------------|
| | | | | Easting (km) | Northing (km) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 78 | CELSIUS ENERGY CO MCCLEAN BASIN WELL 2 | AJAX DPC 230 HP SN 402341 | 0.7 | 238.300 | 4108.800 | 6.1 | 0.3 | 13.3 | 516 | N/A | N/A | 6675 |
| 79 | CELSIUS ENERGY CO MCCLEAN BASIN WELL 2 | WAUKESHA VRG 220 | 0.5 | 241.700 | 4115.400 | 5.5 | 0.3 | 36.2 | 633 | N/A | N/A | 6596 |
| 80 | EL PASO NATURAL GAS CO BONDAD COMP STA | WAUKESHA L5790 GL ICE.CN | 0.2 | 243.700 | 4111.500 | 7.6 | 0.4 | 14.7 | 255 | N/A | N/A | 6209 |
| 81 | EL PASO NATURAL GAS CO BONDAD COMP STA | AJAX DPC-540LE | 0.5 | 243.700 | 4111.500 | 5.5 | 0.3 | 36.2 | 255 | N/A | N/A | 6209 |
| 82 | EL PASO NATURAL GAS CO BONDAD COMP STA | WAUKESHA L5790GL.CN | 0.2 | 243.700 | 4111.500 | 4.9 | 0.2 | 34.8 | 255 | N/A | N/A | 6209 |
| 83 | EL PASO NATURAL GAS CO BONDAD COMP STA | NAT GAS ENG | 0.5 | 243.700 | 4111.500 | 6.1 | 0.5 | 79.9 | 750 | N/A | N/A | 6209 |
| 84 | EL PASO NATURAL GAS COMPANY IGNACIO FLD | TURBINE #1 MD:10-T1302 | 0.5 | 196.191 | 4146.440 | 6.1 | 0.5 | 70.9 | 683 | N/A | N/A | 7068 |
| 85 | EL PASO NATURAL GAS COMPANY IGNACIO FLD | TURBINE SN:0528521R | 0.4 | 196.191 | 4146.440 | 0.0 | 0.0 ^(a) | 0.0 ^(a) | 255 | N/A | N/A | 7068 |
| 86 | FOUR CORNERS MATERIALS, INC. | ENERTEK NATGAS DEHYDRATOR | 0.4 | 239.800 | 4099.000 | 0.0 | 0.0 ^(a) | 0.0 ^(a) | 255 | N/A | N/A | 6426 |
| 87 | FOUR CORNERS MATERIALS, INC. | P & A DEHYDRATOR | 0.3 | 239.800 | 4099.000 | 6.7 | 0.3 | 29.7 | 650 | N/A | N/A | 6426 |
| 88 | FOUR CORNERS MATERIALS, INC. | WAUKESHA 1232HP SN#362478 | 0.3 | 239.800 | 4099.000 | 6.7 | 0.3 | 29.7 | 650 | N/A | N/A | 6426 |
| 89 | FOUR CORNERS MATERIALS, INC. | WAUKESHA 1232HP SN#360634 | 0.3 | 239.800 | 4099.000 | 6.7 | 0.3 | 29.7 | 650 | N/A | N/A | 6426 |

N/A Not available

^(a) Representative value assumed in the modeling

Table B-4. Colorado Emission Source Modeling Input Values (continued)

| Source Count | Source Description | Unit ID | NOx Emission Rate (g/s) | UTM | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|------------------------------------------|---------------------------|-------------------------|--------------|---------------|------------------|--------------|--------------------|-----------|------------|-----------|----------------|
| | | | | Easting (km) | Northing (km) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 90 | FOUR CORNERS MATERIALS, INC. | WAUKESHA 1232HP SN#403117 | 0.3 | 239.800 | 4099.000 | 3.7 | 0.3 | 0.0 ^(a) | 255 | N/A | N/A | 6426 |
| 91 | FUEL RESOURCES DEV CO DEER CANYON UTE 16 | CATERPILLAR G3304NA | 0.5 | 281.700 | 4099.100 | 7.0 | 0.5 | 80.6 | 765 | N/A | N/A | 6176 |
| 92 | FUEL RESOURCES DEV CO SED BURNETT 21 | SATURN T-1300 TURBINE #1 | 0.4 | 252.500 | 4113.700 | 2.1 | 0.1 | 0.9 | 964 | N/A | N/A | 6511 |
| 93 | FUEL RESOURCES DEV CO SED FEDERAL3 1 | CATERPILLAR COMPRESSOR | 0.7 | 250.000 | 4111.700 | 26.2 | 1.8 | 7.0 | 601 | N/A | N/A | 6632 |
| 94 | GLEN WELLS CONST | RADCO AMINE HEATER #1 | 0.5 | 253.200 | 4115.600 | 6.1 | 0.5 | 79.9 | 255 | N/A | N/A | 6642 |
| 95 | HALLIBURTON ENERGY SVCS | SOLAR 10-T1300 | 0.7 | 196.191 | 4146.440 | 3.7 | 0.2 | 28.8 | 769 | N/A | N/A | 7068 |
| 96 | HUGOTON ENERGY CORPORATION | WAUKESHA ENGINE SN:123418 | 0.7 | 238.200 | 4124.200 | 2.4 | 0.1 | 31.2 | 755 | N/A | N/A | 7019 |
| 97 | LA PLATA COUNTY HUMANE SOCIETY | CUMMINS GTA-743A 240HP | 7.0 | 239.500 | 4099.400 | 10.4 | 1.2 | 0.6 | 717 | N/A | N/A | 6396 |
| 98 | MARKWEST RESOURCES INC | (3) CENTAUR 40-T5300L | 1.1 | 253.900 | 4109.100 | 2.4 | 0.1 | 44.4 | 255 | N/A | N/A | 6803 |
| 99 | MARKWEST RESOURCES INC | CATERPILLAR 166HP ENGINE | 2.2 | 239.800 | 4099.000 | 11.0 | 2.4 | 7.3 | 706 | N/A | N/A | 6426 |
| 100 | MARKWEST RESOURCES INC | SOLAR CENTAUR SN: 16684R | 0.4 | 253.900 | 4109.100 | 5.5 | 0.3 | 30.6 | 255 | N/A | N/A | 6803 |
| 101 | MARKWEST RESOURCES INC CARLILE COMP. | WAUK 7042 GL, SN: 402863 | 0.6 | 265.992 | 4104.626 | 5.5 | 0.3 | 30.6 | 650 | N/A | N/A | 6396 |
| 102 | MARKWEST RESOURCES INC CARLILE COMP. | WAUKESHA L7042GL | 0.3 | 265.992 | 4104.626 | 6.7 | 0.3 | 13.2 | 255 | N/A | N/A | 6396 |
| 103 | MERCY MEDICAL CTR | AJAX DPC 360 ENGINE | 0.2 | 249.000 | 4125.500 | 4.9 | 0.2 | 34.8 | 255 | N/A | N/A | 6924 |

N/A Not available

^(a) Representative value assumed in the modeling

Table B-4. Colorado Emission Source Modeling Input Values (continued)

| Source Count | Source Description | Unit ID | NOx Emission Rate (g/s) | UTM | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|------------------------------------------|---------------------------|-------------------------|--------------|---------------|------------------|--------------|--------------------|-----------|------------|-----------|----------------|
| | | | | Easting (km) | Northing (km) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 104 | MERCY MEDICAL CTR | CAT NAT ENG RATED @ 323HP | 0.0 | 234.200 | 4107.000 | 1.8 | 0.6 | 0.0 ^(a) | 422 | N/A | N/A | 6567 |
| 105 | MID AMERICA PIPELINE CO DOLORES STA | 2 CLEAVER BROOKS BOILERS | 0.2 | 183.607 | 4140.925 | 1.8 | 0.6 | 0.0 ^(a) | 422 | N/A | N/A | 6075 |
| 106 | MID AMERICA PIPELINE CO DOLORES STA | 2 CLEAVER BROOKS BOILERS | 0.2 | 183.607 | 4140.925 | 6.7 | 0.3 | 14.5 | 516 | N/A | N/A | 6075 |
| 107 | NATURAL GAS PROCESSING | AJAX DPC 360LE | 0.4 | 236.800 | 4113.600 | 2.4 | 0.9 | 17.3 | 255 | N/A | N/A | 6832 |
| 108 | NATURAL GAS PROCESSING CO | WAUKESHA RICH BURN MOD F8 | 0.2 | 275.000 | 4100.300 | 8.5 | 0.9 | 0.0 ^(a) | 755 | N/A | N/A | 6317 |
| 109 | NORTHWEST PIPELINE CORP LA PLATA B STA | STEAM BOILER #3 | 6.6 | 252.700 | 4114.400 | 13.7 | 1.8 | 40.8 | 728 | N/A | N/A | 6596 |
| 110 | NORTHWEST PIPELINE CORP LA PLATA B STA | TURBINE #1-GE,SN: 282514 | 0.2 | 252.700 | 4114.400 | 8.5 | 0.9 | 0.0 ^(a) | 755 | N/A | N/A | 6596 |
| 111 | NORTHWEST PIPELINE CORP LA PLATA B STA | BOILER - NATGAS FIRED | 0.9 | 252.700 | 4114.400 | 8.5 | 0.8 | 0.0 ^(a) | 755 | N/A | N/A | 6596 |
| 112 | PALO PETROLEUM | SOLAR TURBINE 2470BHP ENG | 0.2 | 252.700 | 4114.400 | 1.5 | 0.1 | 21.2 | 1053 | N/A | N/A | 6596 |
| 113 | QUESTAR EXPLORATION & PROD - MIR 4-31 | FORD CSG-649 SN:17772 ICE | 0.2 | 229.102 | 4113.878 | 6.1 | 2.4 | 12.0 | 255 | N/A | N/A | 6996 |
| 114 | QUESTAR EXPLORATION & PROD - CUTTHROAT A | AJAX DPC-180 S/N 053981 | 0.1 | 249.000 | 4110.000 | 0.6 | 0.1 | 50.8 | 255 | N/A | N/A | 6763 |
| 115 | RMI ENVIRONMENTAL SVC INC | AJAX M/N E-42 SN: 65254 | 0.1 | 237.400 | 4116.500 | 6.1 | 0.3 | 15.8 | 255 | N/A | N/A | 7373 |

N/A Not available

^(a) Representative value assumed in the modeling

Table B-4. Colorado Emission Source Modeling Input Values (continued)

| Source Count | Source Description | Unit ID | NOx Emission Rate (g/s) | UTM | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|---------------------------|---------------------------|-------------------------|--------------|---------------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | | Easting (km) | Northing (km) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 116 | RMI ENVIRONMENTAL SVCS | AJAX DPC 360LE SN 403660 | 0.3 | 238.800 | 4111.700 | 6.7 | 0.3 | 29.7 | 650 | N/A | N/A | 6603 |
| 117 | S G INTERESTS I LTD | WAUKESHA 1109HP #C10607/2 | 0.4 | 239.800 | 4099.000 | 6.7 | 0.3 | 29.7 | 255 | N/A | N/A | 6426 |
| 118 | S G INTERESTS I LTD | WAUKESHA 1117HP #C10985/1 | 0.0 | 239.800 | 4099.000 | 3.7 | 0.3 | 13.2 | 878 | N/A | N/A | 6426 |
| 119 | S G INTERESTS I LTD | CAT 3304 GEN. SET - 72HP | 2.6 | 239.800 | 4099.000 | 13.4 | 1.0 | 59.7 | 794 | N/A | N/A | 6426 |
| 120 | S G INTERESTS I LTD | SOLAR CENTAUR SN: 0228H | 1.6 | 253.200 | 4115.500 | 10.7 | 1.0 | 51.9 | 774 | N/A | N/A | 6642 |
| 121 | S G INTERESTS I LTD | SOLAR CENTAUR SN: HC93059 | 0.0 | 253.200 | 4115.500 | 4.9 | 0.5 | 6.2 | 1171 | N/A | N/A | 6642 |
| 122 | S G INTERESTS I LTD | ALL MDL L1701 SN CR190294 | 0.0 | 244.000 | 4129.000 | 4.9 | 0.5 | 6.2 | 1171 | N/A | N/A | 6606 |
| 123 | S G INTERESTS I LTD | ALL MDL L1701 SN CR190294 | 0.4 | 244.000 | 4129.000 | 6.7 | 0.3 | 29.7 | 255 | N/A | N/A | 6606 |
| 124 | SAN JUAN BASIN CONSORTIUM | WAUKESHA 1117HP #C10985/3 | 0.3 | 239.800 | 4099.000 | 6.7 | 0.3 | 29.7 | 650 | N/A | N/A | 6426 |
| 125 | SAN JUAN BASIN CONSORTIUM | WAUKESHA 1117HP #C10985/8 | 0.3 | 239.800 | 4099.000 | 6.7 | 0.3 | 29.7 | 650 | N/A | N/A | 6426 |
| 126 | SAN JUAN BASIN CONSORTIUM | WAUKESHA 1117HP #C10985/7 | 0.3 | 239.800 | 4099.000 | 6.7 | 0.3 | 29.7 | 650 | N/A | N/A | 6426 |
| 127 | SAN JUAN BASIN CONSORTIUM | WAUKESHA 1232HP #C11059/1 | 0.3 | 239.800 | 4099.000 | 6.7 | 0.3 | 29.7 | 255 | N/A | N/A | 6426 |
| 128 | SAN JUAN BASIN CONSORTIUM | WAUKESHA 895HP #13 | 0.3 | 239.800 | 4099.000 | 6.7 | 0.3 | 29.7 | 255 | N/A | N/A | 6426 |

N/A Not available

^(a) Representative value assumed in the modeling

Table B-4. Colorado Emission Source Modeling Input Values (continued)

| Source Count | Source Description | Unit ID | NOx Emission Rate (g/s) | UTM | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|-----------------------------------------|---------------------------|-------------------------|--------------|---------------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | | Easting (km) | Northing (km) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 129 | SAN JUAN BASIN CONSORTIUM | WAUKESHA 895HP #14 | 0.5 | 239.800 | 4099.000 | 7.3 | 0.3 | 17.8 | 755 | N/A | N/A | 6426 |
| 130 | SG INTEREST I LTD | AJAX ENG. SN: HRM 85-317T | 0.3 | 230.682 | 4108.768 | 7.3 | 0.3 | 17.8 | 755 | N/A | N/A | 6760 |
| 131 | SG INTEREST I LTD | WAUKESHA F3521 ENGINE #2 | 0.2 | 230.682 | 4108.768 | 2.1 | 0.1 | 23.8 | 839 | N/A | N/A | 6760 |
| 132 | SG INTEREST I LTD | CATERPILLAR 3304 70HP ICE | 0.5 | 269.000 | 4106.000 | 4.6 | 0.2 | 6.6 | 561 | N/A | N/A | 6596 |
| 133 | SG INTERESTS I, LTD - SOUTH IGNACIO CDP | WAUKESHA F817,SN: 308602 | 0.5 | 229.102 | 4113.878 | 4.6 | 0.2 | 6.6 | 561 | N/A | N/A | 6996 |
| 134 | SG INTERESTS I, LTD - SOUTH IGNACIO CDP | WAUKESHA F817, SN: 171303 | 0.0 | 229.102 | 4113.878 | 5.5 | 0.5 | 6.1 | 1144 | N/A | N/A | 6996 |
| 135 | SG INTERESTS I LTD | CREMATOR A11-1801 | 0.3 | 182.413 | 4139.497 | 6.7 | 0.3 | 29.7 | 650 | N/A | N/A | 6035 |
| 136 | SG INTERESTS I, LTD. - SUNNYSIDE C.S. | WAUKESHA 1232HP #C10461/4 | 0.3 | 239.800 | 4099.000 | 6.7 | 0.3 | 29.7 | 650 | N/A | N/A | 6426 |
| 137 | SG INTERESTS I, LTD. - SUNNYSIDE C.S. | WAUKESHA 1160HP #C10461/5 | 0.3 | 239.800 | 4099.000 | 6.7 | 0.3 | 29.7 | 650 | N/A | N/A | 6426 |
| 138 | SG INTERESTS I, LTD. - SUNNYSIDE C.S. | WAUKESHA 1109HP #C10607/1 | 0.2 | 239.800 | 4099.000 | 2.4 | 0.2 | 7.7 | 922 | N/A | N/A | 6426 |
| 139 | SHELL CO2 COMPANY - YELLOW JACKET | WAUKESHA ENGINE 399752 | 0.2 | 256.800 | 4118.900 | 2.4 | 0.2 | 7.7 | 922 | N/A | N/A | 6757 |
| 140 | SHELL CO2 COMPANY - YELLOW JACKET | WAUKESHA ENGINE 396325 | 0.2 | 276.300 | 4116.000 | 2.4 | 0.2 | 7.7 | 922 | N/A | N/A | 7321 |
| 141 | SHELL CO2 COMPANY - YELLOW JACKET | WAUKESHA VRG 330, 399859 | 0.2 | 257.100 | 4115.600 | 2.4 | 0.2 | 7.7 | 922 | N/A | N/A | 6596 |
| 142 | SHELL WESTERN E&P INC COW CANYON CLOSED | WAUKESHA VRG 330, 389779 | 0.2 | 248.800 | 4120.900 | 2.4 | 0.2 | 7.7 | 922 | N/A | N/A | 6796 |

N/A Not available

^(a) Representative value assumed in the modeling

Table B-4. Colorado Emission Source Modeling Input Values (continued)

| Source Count | Source Description | Unit ID | NOx Emission Rate (g/s) | UTM | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|------------------------------------------|----------------------------|-------------------------|--------------|---------------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | | Easting (km) | Northing (km) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 143 | SHELL WESTERN E&P INC COW CANYON CLOSED | WAUKESHA VRG 330, 399842 | 0.2 | 269.400 | 4130.400 | 2.4 | 0.2 | 7.7 | 922 | N/A | N/A | 7193 |
| 144 | SHELL WESTERN E&P INC COW CANYON CLOSED | WAUKESHA VRG 330, 389456 | 0.4 | 249.800 | 4112.900 | 1.5 | 0.1 | 16.9 | 866 | N/A | N/A | 6590 |
| 145 | TBI EXPLORATION CO SED STATE 1 36 | WAUKESHA119 7 115HP ENGINE | 1.6 | 250.000 | 4113.300 | 13.4 | 1.0 | 59.7 | 794 | N/A | N/A | 6573 |
| 146 | TEXACO EXPLORATION & PROD INC | SOLAR CENTAUR SN: 0228H | 2.4 | 253.200 | 4115.500 | 8.2 | 1.8 | 12.1 | 603 | N/A | N/A | 6642 |
| 147 | TEXACO EXPLORATION & PROD UTE C WELL NO2 | SOLAR T-3000 SN:1668C4R | 2.4 | 253.900 | 4109.100 | 8.2 | 1.8 | 12.0 | 603 | N/A | N/A | 6803 |
| 148 | TEXACO EXPLORATION & PROD UTE E WEL NO2 | SOLAR T3000 SN:8009663R91 | 0.2 | 253.900 | 4109.100 | 4.0 | 0.2 | 40.7 | 811 | N/A | N/A | 6803 |
| 149 | THE HANOVER COMPANY - CAIN 31-1 | CATERPILLAR 376HP ENGINE | 0.6 | 258.200 | 4117.800 | 3.7 | 0.1 | 47.9 | 836 | N/A | N/A | 6599 |
| 150 | THE HANOVER COMPANY - CAIN 31-2 | WAUKESHA F1905G, SN:70493 | 0.6 | 258.200 | 4117.800 | 2.1 | 0.1 | 0.6 | 865 | N/A | N/A | 6599 |
| 151 | UTE E CENTRAL DELIVERY POINT | WAUKESHA MODEL 1905 170HP | 0.3 | 267.500 | 4107.800 | 2.1 | 0.1 | 11.9 | 866 | N/A | N/A | 6396 |
| 152 | UTE E CENTRAL DELIVERY POINT | CATERPILLAR 3304 ENGINE | 0.2 | 269.100 | 4103.200 | 1.8 | 0.1 | 25.5 | 811 | N/A | N/A | 6396 |

N/A Not available

^(a) Representative value assumed in the modeling

Table B-4. Colorado Emission Source Modeling Input Values (continued)

| Source Count | Source Description | Unit ID | NOx Emission Rate (g/s) | UTM | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|-----------------------------------------|---------------------------|-------------------------|--------------|---------------|--------------------|--------------------|--------------------|-----------|------------|-----------|----------------|
| | | | | Easting (km) | Northing (km) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 153 | VASTAR RESOURCES INC. - WELL 4-3; 32-10 | CAT G3408TA 400HP ENGINE | 0.2 | 258.200 | 4117.800 | 2.1 | 0.1 | 12.2 | 255 | N/A | N/A | 6599 |
| 154 | WESTERN MOBILE NORTHERN INC | WAUKESHA VRG330 SN 402613 | 0.2 | 219.392 | 4110.886 | 4.9 | 0.3 | 11.4 | 500 | N/A | N/A | 6629 |
| 155 | WESTERN MOBILE NORTHERN INC | ICE AJAX DPC-230 184 HP | 0.0 | 251.000 | 4105.000 | 0.0 ^(a) | 0.0 ^(a) | 0.0 ^(a) | 255 | N/A | N/A | 7396 |
| 156 | WESTERN MOBILE NORTHERN INC | ELASTEC SMARTASH RECOVERY | 0.1 | 276.700 | 4103.300 | 6.4 | 0.3 | 8.1 | 255 | N/A | N/A | 6576 |
| 157 | WESTERN MOBILE NORTHERN INC | ICE AJAX DPC 180 144 HP | 0.1 | 251.000 | 4105.000 | 0.0 ^(a) | 0.0 ^(a) | 0.0 ^(a) | 294 | N/A | N/A | 7396 |
| 158 | WESTERN MOBILE NORTHERN INC | FORD ICE SN00693605RG .XP | 0.3 | 260.000 | 4107.500 | 4.9 | 0.3 | 6.7 | 528 | N/A | N/A | 6796 |
| 159 | WESTERN MOBILE NORTHERN INC | AJAX DPC 140 | 0.4 | 251.000 | 4105.000 | 2.1 | 0.1 | 18.0 | 844 | N/A | N/A | 7396 |
| 160 | WILLIAMS FIELD SERVICES - LONE PINE | CATERPILLAR 3306 90HP ICE | 2.1 | 248.400 | 4113.300 | 15.2 | 1.1 | 30.5 | 450 | N/A | N/A | 6596 |
| 161 | WILLIAMS FIELD SERVICES - LONE PINE | SOLAR TAURUS TURBINE #1 | 2.1 | 252.500 | 4114.300 | 15.2 | 1.1 | 30.5 | 450 | N/A | N/A | 6596 |
| 162 | WILLIAMS FIELD SERVICES - LONE PINE | SOLAR TAURUS TURBINE #2 | 0.3 | 252.500 | 4114.300 | 6.4 | 0.3 | 40.5 | 255 | N/A | N/A | 6596 |
| 163 | WILLIAMS FIELD SERVICES IGNACIO B PLT | NAT GAS ENG RATED 1380 HP | 0.6 | 253.200 | 4115.600 | 7.3 | 0.3 | 36.8 | 689 | N/A | N/A | 6642 |
| 164 | WILLIAMS FIELD SERVICES IGNACIO B PLT | CAT G3516TA 1085HP COMP#4 | 0.6 | 234.000 | 4106.500 | 5.5 | 0.3 | 35.3 | 255 | N/A | N/A | 6540 |
| 165 | WILLIAMS FIELD SERVICES IGNACIO B PLT | WAUKESHA L5790GL | 2.8 | 234.200 | 4107.000 | 4.3 | 0.2 | 69.2 | 644 | N/A | N/A | 6567 |

N/A Not available

^(a) Representative value assumed in the modeling

Table B-4. Colorado Emission Source Modeling Input Values (continued)

| Source Count | Source Description | Unit ID | NOx Emission Rate (g/s) | UTM | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|------------------------------------------|---------------------------|-------------------------|--------------|---------------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | | Easting (km) | Northing (km) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 166 | WILLIAMS FIELD SERVICES IGNACIO B PLT | CAT G399TA COMP #1 660HP | 0.4 | 234.200 | 4107.000 | 2.1 | 0.1 | 12.2 | 644 | N/A | N/A | 6567 |
| 167 | WILLIAMS FIELD SERVICES IGNACIO B PLT | CAT G399TA COMP #2 660HP | 0.4 | 234.200 | 4107.000 | 2.1 | 0.1 | 12.2 | 644 | N/A | N/A | 6567 |
| 168 | WILLIAMS FIELD SERVICES IGNACIO B PLT | SUPERIOR 6G825 #3 460HP | 1.9 | 234.200 | 4107.000 | 4.6 | 0.2 | 60.7 | 811 | N/A | N/A | 6567 |
| 169 | WILLIAMS FIELD SERVICES IGNACIO B PLT | FORD CSG649 V6 ENG 60HP | 0.1 | 234.200 | 4107.000 | 2.7 | 0.1 | 58.9 | 644 | N/A | N/A | 6567 |
| 170 | WILLIAMS FIELD SERVICES IGNACIO B PLT | FORD LSG875 TRIPLEX1 90HP | 0.2 | 234.200 | 4107.000 | 3.0 | 0.1 | 53.4 | 644 | N/A | N/A | 6567 |
| 171 | WILLIAMS FIELD SERVICES IGNACIO B PLT | FORD LSG875 V8 ENG 90HP | 0.2 | 233.980 | 4106.500 | 3.0 | 0.1 | 53.4 | 644 | N/A | N/A | 6540 |
| 172 | WILLIAMS FIELD SVCS | WAUKESHA SN: C106791 | 0.9 | 257.800 | 4108.700 | 7.6 | 0.4 | 27.4 | 633 | N/A | N/A | 6875 |
| 173 | WILLIAMS FIELD SVCS BONDAD 33 9 NO7 WELL | CUMMINS GTA-743A ENGINE | 0.6 | 256.300 | 4114.100 | 2.4 | 0.1 | 25.4 | 755 | N/A | N/A | 6593 |
| 174 | WILLIAMS FIELD SVCS BUENA SUERTA | CATERPILLAR CA 95 3306NA | 0.3 | 246.800 | 4111.400 | 2.7 | 0.1 | 33.5 | 255 | N/A | N/A | 6406 |
| 175 | WILLIAMS FIELD SVCS BUENA SUERTA | NATURAL GAS ENGINE | 0.2 | 276.000 | 4100.500 | 1.2 | 0.2 | 32.9 | 255 | N/A | N/A | 6196 |
| 176 | WILLIAMS FIELD SVCS BUENA SUERTA | WAUKESHA L5788G 460 HP | 0.4 | 274.200 | 4099.900 | 0.0 | 0.0 | 0.0 | 294 | N/A | N/A | 6422 |
| 177 | WILLIAMS FIELD SVCS BUENA SUERTA | DORMAN DA 85 GDAGT 81HP | 0.5 | 246.800 | 4111.400 | 2.1 | 0.1 | 32.4 | 255 | N/A | N/A | 6406 |
| 178 | WILLIAMS FIELD SVCS BUENA SUERTA | FORD VSG 4131 00698 CANC | 0.1 | 261.000 | 4107.800 | 0.0 | 0.0 | 0.0 | 294 | N/A | N/A | 6694 |
| 179 | WILLIAMS FIELD SVCS IGNACIO 33 7 SITE | CAT G399 TALE 59C01159 | 0.6 | 243.800 | 4108.200 | 6.4 | 0.2 | 77.4 | 255 | N/A | N/A | 6196 |

N/A Not available

^(a) Representative value assumed in the modeling

Table B-4. Colorado Emission Source Modeling Input Values (continued)

| Source Count | Source Description | Unit ID | NOx Emission Rate (g/s) | UTM | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|--------------------------------------|---------------------------|-------------------------|--------------|---------------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | | Easting (km) | Northing (km) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 180 | WILLIAMS FIELD SVCS LATERAL 2 B STA | CAT SN: C111614EK03197 | 0.7 | 251.600 | 4126.500 | 6.1 | 0.3 | 17.0 | 255 | N/A | N/A | 7108 |
| 181 | WILLIAMS FIELD SVCS MCCARVILLE 1 STA | NAT GAS ENG & 1068 HP | 0.6 | 241.000 | 4111.300 | 6.1 | 0.1 | 8.3 | 749 | N/A | N/A | 6544 |
| 182 | WILLIAMS FIELD SVCS PLA 9 STA | WAUKESHA VRG330 NO. 40262 | 0.2 | 227.808 | 4110.854 | 2.1 | 0.9 | 12.2 | 255 | N/A | N/A | 6822 |
| 183 | WILLIAMS FIELD SVCS PLA 9 STA | WAUKESHA SN:C-12756/7 ICE | 0.4 | 237.200 | 4099.200 | 4.9 | 0.2 | 38.3 | 720 | N/A | N/A | 6570 |
| 184 | WILLIAMS FIELD SVCS PLA 9 STA | WAUKESHA F18GL 400HP ICE | 0.2 | 241.720 | 4099.183 | 4.9 | 0.2 | 12.6 | 255 | N/A | N/A | 6816 |
| 185 | WILLIAMS FIELD SVCS PLA 9 STA | WAUKESHA ICE SN:414003 | 0.6 | 248.479 | 4111.562 | 6.1 | 0.4 | 29.7 | 649 | N/A | N/A | 6596 |
| 186 | WILLIAMS FIELD SVCS PLA 9 STA | WAUKESHA NAT GAS ENGINE | 0.4 | 241.720 | 4099.183 | 4.9 | 0.2 | 38.4 | 255 | N/A | N/A | 6816 |
| 187 | WILLIAMS FIELD SVCS PLA 9 STA | WAUKESHA L 7042 GL ICE | 0.5 | 238.900 | 4112.100 | 6.7 | 0.3 | 38.5 | 631 | N/A | N/A | 6642 |
| 188 | WILLIAMS FIELD SVCS PLA 9 STA | WAUKESHA L 7042 G ICE | 0.4 | 238.900 | 4112.100 | 6.7 | 0.3 | 22.3 | 823 | N/A | N/A | 6642 |
| 189 | WILLIAMS FIELD SVCS PLA 9 STA | WAUKESHA L 7042 G ICE | 0.4 | 238.900 | 4112.100 | 6.7 | 0.3 | 22.3 | 823 | N/A | N/A | 6642 |
| 190 | WILLIAMS FIELD SVCS PLA 9 STA | CATERPILLAR G34212LE | 0.3 | 237.200 | 4099.200 | 5.5 | 0.3 | 46.6 | 255 | N/A | N/A | 6570 |
| 191 | WILLIAMS FIELD SVCS PLA 9 STA | CATERPILLAR 3512LE | 0.8 | 248.479 | 4111.562 | 6.1 | 0.2 | 40.8 | 255 | N/A | N/A | 6596 |
| 192 | WILLIAMS FIELD SVCS PLA 9 STA | WAUKESHA L7042GL ENG | 0.4 | 241.720 | 4099.183 | 6.7 | 0.3 | 40.9 | 637 | N/A | N/A | 6816 |
| 193 | WILLIAMS FIELD SVCS PLA 9 STA | WAUKESHA L 7042 ENGINE | 0.4 | 241.720 | 4099.183 | 6.7 | 0.3 | 40.9 | 637 | N/A | N/A | 6816 |

N/A Not available

^(a) Representative value assumed in the modeling

Table B-4. Colorado Emission Source Modeling Input Values (continued)

| Source Count | Source Description | Unit ID | NOx Emission Rate (g/s) | UTM | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|----------------------------------|---------------------------|-------------------------|--------------|---------------|------------------|--------------|--------------------|-----------|------------|-----------|----------------|
| | | | | Easting (km) | Northing (km) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 194 | WILLIAMS FIELD SVCS PLA 9 STA | WAUKESHA L7042 GL ENGINE | 0.4 | 241.720 | 4099.183 | 6.7 | 0.3 | 40.9 | 637 | N/A | N/A | 6816 |
| 195 | WILLIAMS FIELD SVCS PLA 9 STA | CUMMING, MODEL G-855 | 0.9 | 262.300 | 4123.300 | 2.4 | 1.2 | 25.4 | 255 | N/A | N/A | 7196 |
| 196 | WILLIAMS FIELD SVCS PLA 9 STA | CATERPILLAR 379 TA 350 HP | 1.0 | 248.479 | 4111.562 | 4.6 | 0.2 | 28.7 | 865 | N/A | N/A | 6596 |
| 197 | WILLIAMS FIELD SVCS PLA 9 STA | WAUKESHA F1197 | 0.2 | 262.474 | 4125.121 | 3.0 | 0.1 | 98.2 | 255 | N/A | N/A | 7396 |
| 198 | WILLIAMS FIELD SVCS PLA 9 STA | CATERPILLAR G3307 | 0.1 | 263.187 | 4119.244 | 2.4 | 0.1 | 38.4 | 255 | N/A | N/A | 6783 |
| 199 | WILLIAMS FIELD SVCS PLA 9 STA | CATERPILLAR G34212LE | 0.3 | 237.200 | 4099.200 | 5.5 | 0.3 | 46.6 | 255 | N/A | N/A | 6570 |
| 200 | WILLIAMS FIELD SVCS TRUNK J SITE | TO2 SOLAR CENTAUR 60T700S | 0.6 | 252.500 | 4114.500 | 13.7 | 1.0 | 14.9 | 744 | N/A | N/A | 6596 |
| 201 | WILLIAMS FIELD SVCS TRUNK J SITE | SOLAR CENTAUR 50-HSN 0026 | 0.6 | 252.500 | 4114.500 | 8.8 | 1.0 | 0.0 ^(a) | 799 | N/A | N/A | 6596 |

N/A Not available

^(a) Representative value assumed in the modeling

Appendix C – New Mexico Emission Inventory

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|-------------------------------------------------------|-------------|
| C-1. New Mexico Emission Source Modeling Input Values | 169 |

Table C-1. New Mexico Emission Source Modeling Input Values

| Source Count | Source Description | Unit ID | NOx Emission Rate (g/s) | UTM | | Stack Parameters | | | | Building | | Elevation (m) |
|--------------|------------------------------------------|---------|-------------------------|-------------|--------------|------------------|--------------|----------------|-----------|------------|-----------|---------------|
| | | | | Easting (m) | Northing (m) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 1 | Williams Field Services/El Cedro Gp/340M | nm01 | 0.57 | 285600 | 4062800 | 22.0 | 1.0 | 150.0 | 702.0 | N/A | N/A | 1966 |
| 2 | Williams Field Services/El Cedro Gp/340M | nm02 | 0.57 | 285600 | 4062800 | 22.0 | 1.0 | 150.0 | 702.0 | N/A | N/A | 1966 |
| 3 | Williams Field Services/El Cedro Gp/340M | nm03 | 0.57 | 285600 | 4062800 | 22.0 | 1.0 | 150.0 | 702.0 | N/A | N/A | 1966 |
| 4 | Williams Field Services/El Cedro Gp/340M | nm04 | 0.57 | 285600 | 4062800 | 22.0 | 1.0 | 150.0 | 702.0 | N/A | N/A | 1966 |
| 5 | Williams Field Services/El Cedro Gp/340M | nm05 | 3.99 | 285600 | 4062800 | 6.7 | 0.3 | 47.2 | 645.4 | N/A | N/A | 1966 |
| 6 | Williams Field Services/Manz CDP 31-6/PS | nm06 | 0.01 | 284200 | 4079400 | 4.6 | 0.2 | 20.0 | 1273.2 | N/A | N/A | 1955 |
| 7 | Williams Field Services/Manz CDP 31-6/PS | nm07 | 0.01 | 284200 | 4079400 | 4.6 | 0.2 | 20.0 | 1273.2 | N/A | N/A | 1955 |
| 8 | Williams Field Services/Manz CDP 31-6/PS | nm08 | 0.57 | 284200 | 4079400 | 22.0 | 1.0 | 150.0 | 702.0 | N/A | N/A | 1955 |
| 9 | Williams Field Services/Manz CDP 31-6/PS | nm09 | 9.11 | 284200 | 4079400 | 6.7 | 0.3 | 47.2 | 645.4 | N/A | N/A | 1955 |
| 10 | Williams Field Services/Trunk L Cs/1527M | nm10 | 0.03 | 289500 | 4057600 | 0.0 | 0.0 | 0.0 | 0.0 | N/A | N/A | 2000 |
| 11 | Williams Field Services/Trunk L Cs/1527M | nm11 | 0.03 | 289500 | 4057600 | 0.0 | 0.0 | 0.0 | 0.0 | N/A | N/A | 2000 |
| 12 | Williams Field Services/Trunk L Cs/1527M | nm12 | 0.08 | 289500 | 4057600 | 7.6 | 0.3 | 32.6 | 697.0 | N/A | N/A | 2000 |
| 13 | Williams Field Services/Trunk L Cs/1527M | nm13 | 0.47 | 289500 | 4057600 | 22.0 | 1.0 | 106.0 | 714.0 | N/A | N/A | 2000 |
| 14 | Williams Field Services/Trunk L Cs/1527M | nm14 | 0.47 | 289500 | 4057600 | 22.0 | 1.0 | 106.0 | 714.0 | N/A | N/A | 2000 |
| 15 | Williams Field Services/Trunk L Cs/1527M | nm15 | 0.47 | 289500 | 4057600 | 22.0 | 1.0 | 106.0 | 714.0 | N/A | N/A | 2000 |

N/A – Not available

Table C-1. New Mexico Emission Source Modeling Input Values (continued)

| Source Count | Source Description | Unit ID | NOx Emission Rate (g/s) | UTM | | Stack Parameters | | | | Building | | Elevation (m) |
|--------------|------------------------------------------|---------|-------------------------|-------------|--------------|------------------|--------------|----------------|-----------|------------|-----------|---------------|
| | | | | Easting (m) | Northing (m) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 16 | Williams Field Services/Trunk L Cs/1527M | nm16 | 0.47 | 289500 | 4057600 | 22.0 | 1.0 | 106.0 | 714.0 | N/A | N/A | 2000 |
| 17 | Williams Field Services/Trunk L Cs/1527M | nm17 | 0.47 | 289500 | 4057600 | 22.0 | 1.0 | 106.0 | 714.0 | N/A | N/A | 2000 |
| 18 | Williams Field Services/Trunk L Cs/1527M | nm18 | 0.47 | 289500 | 4057600 | 22.0 | 1.0 | 106.0 | 714.0 | N/A | N/A | 2000 |
| 19 | Williams Field Services/Trunk L Cs/1527M | nm19 | 0.47 | 289500 | 4057600 | 22.0 | 1.0 | 106.0 | 714.0 | N/A | N/A | 2000 |
| 20 | Williams Field Services/Trunk L Cs/1527M | nm20 | 6.60 | 289500 | 4057600 | 6.7 | 0.3 | 32.3 | 652.0 | N/A | N/A | 2000 |
| 21 | Williams Field Services/Trunk L Cs/1527M | nm21 | 0.03 | 289500 | 4057600 | 20.0 | 2.0 | 10.0 | 700.0 | N/A | N/A | 2000 |
| 22 | Williams Field Services/Trunk L Cs/1527M | nm22 | 0.03 | 289500 | 4057600 | 20.0 | 2.0 | 10.0 | 700.0 | N/A | N/A | 2000 |
| 23 | Williams Field Services/Trunk L Cs/1527M | nm23 | 0.03 | 289500 | 4057600 | 20.0 | 2.0 | 10.0 | 700.0 | N/A | N/A | 2000 |
| 24 | Williams Field Services/Trunk L Cs/1527M | nm24 | 0.10 | 289500 | 4057600 | 6.1 | 0.6 | 3.0 | 644.3 | N/A | N/A | 2000 |
| 25 | Williams Field Services/Thompson C. S./0 | nm25 | 0.78 | 223709.9 | 4080850 | 6.7 | 0.3 | 64.0 | 679.8 | N/A | N/A | 1769 |
| 26 | Mid-America Pipeline/Huerfano/888M3 | nm26 | 0.72 | 239500 | 4040000 | 6.1 | 0.6 | 41.2 | 786.5 | N/A | N/A | 1989 |
| 27 | Mid-America Pipeline/Huerfano/888M3 | nm27 | 0.72 | 238400 | 4041000 | 6.1 | 0.6 | 41.2 | 786.5 | N/A | N/A | 1989 |
| 28 | Williams Field Services/32-7cdp Cs/1032M | nm28 | 0.57 | 272100 | 4090200 | 22.0 | 1.0 | 162.0 | 801.0 | N/A | N/A | 2060 |
| 29 | Williams Field Services/32-7cdp Cs/1032M | nm29 | 0.57 | 272100 | 4090200 | 22.0 | 1.0 | 162.0 | 801.0 | N/A | N/A | 2060 |
| 30 | Williams Field Services/32-7cdp Cs/1032M | nm30 | 0.57 | 272100 | 4090200 | 22.0 | 1.0 | 162.0 | 801.0 | N/A | N/A | 2060 |

N/A – Not available

Table C-1. New Mexico Emission Source Modeling Input Values (continued)

| Source Count | Source Description | Unit ID | NOx Emission Rate (g/s) | UTM | | Stack Parameters | | | | Building | | Elevation (m) |
|--------------|------------------------------------------|---------|-------------------------|-------------|--------------|------------------|--------------|----------------|-----------|------------|-----------|---------------|
| | | | | Easting (m) | Northing (m) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 31 | Williams Field Services/32-7cdp Cs/1032M | nm31 | 6.80 | 272100 | 4090200 | 6.7 | 0.3 | 49.4 | 700.4 | N/A | N/A | 2060 |
| 32 | Williams Field Services/32-7cdp Cs/1032M | nm32 | 0.01 | 272100 | 4090200 | 4.6 | 0.3 | 20.1 | 1273.2 | N/A | N/A | 2060 |
| 33 | Williams Field Services/32-9 CDP/924M2R2 | nm33 | 0.01 | 245100 | 4086900 | 3.0 | 0.2 | 1.6 | 588.7 | N/A | N/A | 1900 |
| 34 | Williams Field Services/Trunk C Boost.18 | nm34 | 0.58 | 242500 | 4088500 | 22.0 | 1.0 | 150.0 | 704.0 | N/A | N/A | 1875 |
| 35 | Williams Field Services/Trunk C Boost.18 | nm35 | 0.58 | 242500 | 4088500 | 22.0 | 1.0 | 150.0 | 704.0 | N/A | N/A | 1875 |
| 36 | Williams Field Services/Trunk C Boost.18 | nm36 | 0.58 | 242500 | 4088500 | 6.7 | 0.3 | 47.0 | 646.5 | N/A | N/A | 1875 |
| 37 | Williams Field Services/Trunk C Boost.18 | nm37 | 2.30 | 242500 | 4088500 | 6.7 | 0.3 | 47.0 | 646.5 | N/A | N/A | 1875 |
| 38 | Williams Field Services/Horton Comp/2280 | nm38 | 4.29 | 225361 | 4093959 | 7.3 | 0.3 | 36.6 | 769.3 | N/A | N/A | 1884 |

N/A – Not available

Appendix D – Tribal Emission Inventory

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| D-2. CDPHE Permit Emission Inventory | 176 |
| D-3. Tribal Near Field Emission Source Modeling Input Values | 178 |
| D-4. Tribal Far Field Emission Source Modeling Input Values | 184 |

Table D-1. EPA Part 71 Permit Emission Inventory

| Source Description | Unit ID | UTM Easting (km) | UTM Northing (km) | NOx (t/yr) | Stack Height (m) | Stack Diameter (m) | Stack Velocity (m/s) | Stack Temp (°K) |
|----------------------------------------|------------|------------------|-------------------|------------|----------------------|---------------------|----------------------|-----------------|
| Amoco Production Co Florida River | turbine | 243.74 | 4115.89 | 91.5 | 10.67 ⁽¹⁾ | 1.01 ⁽¹⁾ | 51.94 ⁽²⁾ | --- |
| Amoco Production Co Florida River | turbine | 243.74 | 4115.89 | 100.7 | 13.41 ⁽¹⁾ | 1.01 ⁽¹⁾ | 59.74 ⁽²⁾ | --- |
| Amoco Production Co Florida River | heater | 243.74 | 4115.89 | 32.1 | 3.5 ⁽¹⁾ | 0.46 ⁽¹⁾ | 3.5 ⁽²⁾ | --- |
| Amoco Production Co Florida River | heater | 243.74 | 4115.89 | 50.3 | 3.5 | 0.46 | 3.5 | --- |
| Amoco Production Co Florida River | dehydrator | 243.74 | 4115.89 | 7.12 | 3.5 | 0.46 | 3.5 | --- |
| Amoco Production Co Florida River | heater | 243.74 | 4115.89 | 4.4 | 3.5 | 0.46 | 3.5 | --- |
| Amoco Production Co Florida River | flare | 243.74 | 4115.89 | 3.1 | 3.5 | 0.46 | 3.5 | --- |
| Amoco Production Co Florida River | compressor | 243.74 | 4115.89 | 21.5 | 4.6 ⁽¹⁾ | 0.5 ⁽¹⁾ | 15.8 ⁽²⁾ | --- |
| Conoco Argenta CDP | compressor | 239.18 | 4113.22 | 25.7 | --- | --- | --- | --- |
| Conoco Argenta CDP | compressor | 239.18 | 4113.22 | 25.7 | --- | --- | --- | --- |
| Conoco Argenta CDP | compressor | 239.18 | 4113.22 | 25.7 | --- | --- | --- | --- |
| Conoco Argenta CDP | compressor | 239.18 | 4113.22 | 168.1 | --- | --- | --- | --- |
| Conoco Argenta CDP | compressor | 239.18 | 4113.22 | 25.7 | --- | --- | --- | --- |
| Conoco Argenta CDP | compressor | 239.18 | 4113.22 | 25.7 | --- | --- | --- | --- |
| Conoco Argenta CDP | compressor | 239.18 | 4113.22 | 25.7 | --- | --- | --- | --- |
| Coyote Gulch Treating Plant | compressor | 227.8 | 4100.95 | 43 | --- | --- | --- | --- |
| Coyote Gulch Treating Plant | compressor | 227.8 | 4100.95 | 43 | --- | --- | --- | --- |
| Coyote Gulch Treating Plant | compressor | 227.8 | 4100.95 | 32 | --- | --- | --- | --- |
| Coyote Gulch Treating Plant | reboiler | 227.8 | 4100.95 | 20 | --- | --- | --- | --- |
| Coyote Gulch Treating Plant | reboiler | 227.8 | 4100.95 | 20 | --- | --- | --- | --- |
| Coyote Gulch Treating Plant | reboiler | 227.8 | 4100.95 | 2 | --- | --- | --- | --- |
| Coyote Gulch Treating Plant | heater | 227.8 | 4100.95 | 24 | --- | --- | --- | --- |
| Coyote Gulch Treating Plant | heater | 227.8 | 4100.95 | 36 | --- | --- | --- | --- |
| Coyote Gulch Treating Plant | reboiler | 227.8 | 4100.95 | 1 | --- | --- | --- | --- |
| El Paso Natural Gas Bondad Compres Sta | turbine | 253.466 | 4109.5 | 83 | --- | --- | --- | --- |
| El Paso Natural Gas Bondad Compres Sta | turbine | 253.466 | 4109.5 | 83 | --- | --- | --- | --- |
| El Paso Natural Gas Bondad Compres Sta | turbine | 253.466 | 4109.5 | 83 | --- | --- | --- | --- |
| Red Cedar Arkansas Loop Plant | compressor | 252.9 | 4103.61 | 18.58 | 5.81 | 4.88 | 37.4 | 646.5 |
| Red Cedar Arkansas Loop Plant | compressor | 252.9 | 4103.61 | 19.04 | --- | --- | --- | --- |

⁽¹⁾ Stack height and diameter in ft

⁽²⁾ Stack velocity in ft/sec

Table D-1. EPA Part 71 Permit Emission Inventory (continued)

| Source Description | Unit ID | UTM Easting (km) | UTM Northing (km) | NOx (t/yr) | Stack Height (m) | Stack Diameter (m) | Stack Velocity (m/s) | Stack Temp (°K) |
|-------------------------------------------|------------------|------------------|-------------------|------------|------------------|--------------------|----------------------|-----------------|
| Red Cedar Arkansas Loop Plant | compressor | 252.9 | 4103.61 | 36.47 | 5.46 | 5.49 | 46.63 | 684 |
| Red Cedar Arkansas Loop Plant | compressor | 252.9 | 4103.61 | 37.24 | 5.46 | 5.49 | 46.63 | 684 |
| Red Cedar Arkansas Loop Plant | compressor | 252.9 | 4103.61 | 36.47 | 2.9 | 6.1 | 46.3 | 664.8 |
| Red Cedar Arkansas Loop Plant | compressor | 252.9 | 4103.61 | 36.47 | 5.46 | 5.49 | 46.63 | 684 |
| Red Cedar Arkansas Loop Plant | generator | 252.9 | 4103.61 | 16.28 | --- | --- | --- | --- |
| Red Cedar Arkansas Loop Plant | generator | 252.9 | 4103.61 | 16.28 | --- | --- | --- | --- |
| Red Cedar Arkansas Loop Plant | generator | 252.9 | 4103.61 | 16.28 | --- | --- | --- | --- |
| Red Cedar Arkansas Loop Plant | heater | 252.9 | 4103.61 | 16.92 | --- | --- | --- | --- |
| Red Cedar Arkansas Loop Plant | heater | 252.9 | 4103.61 | 20.75 | --- | --- | --- | --- |
| Red Cedar Arkansas Loop Plant | heater | 252.9 | 4103.61 | 1.27 | --- | --- | --- | --- |
| Red Cedar Diamond Back Compressor Station | compressor | 246.9 | 4101.96 | 19.27 | --- | --- | --- | --- |
| Red Cedar Diamond Back Compressor Station | compressor | 246.9 | 4101.96 | 19.27 | --- | --- | --- | --- |
| Red Cedar Diamond Back Compressor Station | compressor | 246.9 | 4101.96 | 19.27 | --- | --- | --- | --- |
| Red Cedar Bondad Compres Sta | compressor | 243.63 | 4098.8 | 5.2 | --- | --- | --- | --- |
| Red Cedar Bondad Compres Sta | compressor | 243.63 | 4098.8 | 19.44 | --- | --- | --- | --- |
| Red Cedar Bondad Compres Sta | compressor | 243.63 | 4098.8 | 19.44 | --- | --- | --- | --- |
| Red Cedar Bondad Compres Sta | compressor | 243.63 | 4098.8 | 19.44 | --- | --- | --- | --- |
| Red Cedar Bondad Compres Sta | compressor | 243.63 | 4098.8 | 19.44 | --- | --- | --- | --- |
| Red Cedar Bondad Compres Sta | compressor | 243.63 | 4098.8 | 19.44 | --- | --- | --- | --- |
| Red Cedar Bondad Compres Sta | compressor | 243.63 | 4098.8 | 19.44 | --- | --- | --- | --- |
| Red Cedar Bondad Compres Sta | compressor | 243.63 | 4098.8 | 19.44 | --- | --- | --- | --- |
| Red Cedar Bondad Compres Sta | reboiler | 243.63 | 4098.8 | 0.88 | --- | --- | --- | --- |
| Red Cedar Antler Gas Plant | pump driver | 231.12 | 4100.9 | 50.67 | --- | --- | --- | --- |
| Red Cedar Antler Gas Plant | pump driver | 231.12 | 4100.9 | 2.89 | --- | --- | --- | --- |
| Red Cedar Antler Gas Plant | generator driver | 231.12 | 4100.9 | 50.67 | --- | --- | --- | --- |
| Red Cedar Antler Gas Plant | generator driver | 231.12 | 4100.9 | 2.89 | --- | --- | --- | --- |
| Red Cedar Antler Gas Plant | reboiler burner | 231.12 | 4100.9 | 31.04 | --- | --- | --- | --- |

Table D-1. EPA Part 71 Permit Emission Inventory (continued)

| Source Description | Unit ID | UTM Easting (km) | UTM Northing (km) | NOx (t/yr) | Stack Height (m) | Stack Diameter (m) | Stack Velocity (m/s) | Stack Temp (°K) |
|--------------------------------------------|-----------------|------------------|-------------------|------------|------------------|--------------------|----------------------|-----------------|
| Red Cedar Antler Gas Plant | reboiler burner | 231.12 | 4100.9 | 0.61 | --- | --- | --- | --- |
| Red Cedar Antler Gas Plant | compressor | 231.12 | 4100.9 | 23.18 | --- | --- | --- | --- |
| Red Cedar Antler Gas Plant | compressor | 231.12 | 4100.9 | 23.18 | --- | --- | --- | --- |
| Red Willow Coyote Gulch Compressor Station | compressor | 229.25 | 4100.73 | 19.44 | --- | --- | --- | --- |
| Red Willow Coyote Gulch Compressor Station | compressor | 229.25 | 4100.73 | 19.44 | --- | --- | --- | --- |
| Red Willow Coyote Gulch Compressor Station | compressor | 229.25 | 4100.73 | 19.44 | --- | --- | --- | --- |
| Red Willow Coyote Gulch Compressor Station | compressor | 229.25 | 4100.73 | 25.92 | --- | --- | --- | --- |
| Red Willow Coyote Gulch Compressor Station | compressor | 229.25 | 4100.73 | 19.44 | --- | --- | --- | --- |
| Red Willow Coyote Gulch Compressor Station | compressor | 229.25 | 4100.73 | 19.44 | --- | --- | --- | --- |
| Red Willow Coyote Gulch Compressor Station | compressor | 229.25 | 4100.73 | 19.44 | --- | --- | --- | --- |
| Red Willow Coyote Gulch Compressor Station | generator | 229.25 | 4100.73 | 3.38 | --- | --- | --- | --- |
| Transwestern La Plata A Comp Sta | compressor | 247.63 | 4114.52 | 32 | 13.72 | 1 | 14.94 | 798.6 |
| Transwestern La Plata A Comp Sta | compressor | 247.63 | 4114.52 | 19 | 13.72 | 1.01 | 6.1 | 769.11 |

Table D-2. CDPHE Permit Emission Inventory

| Source Description | Unit ID | UTM Easting (km) | UTM Northing (km) | NOx (t/yr) | Stack Height (m) | Stack Diameter (m) | Stack Velocity (m/s) | Stack Temp (°K) |
|-----------------------------------|----------------------------|------------------|-------------------|------------|--------------------|--------------------|----------------------|------------------|
| AMOCO PROD CO PICNIC FLATS | CAT G399TA COMP #1 660HP | 234.2 | 4107 | 31.8 | 14.0 | 0.5 | 226.9 | 700 |
| AMOCO PROD CO PICNIC FLATS | CAT G399TA COMP #2 660HP | 234.2 | 4107 | 12.7 | 14.0 | 0.5 | 226.9 | 700 |
| AMOCO PROD CO PICNIC FLATS | SUPERIOR 6G825 #3 460HP | 234.2 | 4107 | 66.7 | 15.0 | 0.5 | 199.2 | 1000 |
| AMOCO PROD CO PICNIC FLATS | CAT G3516TA 1085HP COMP#4 | 234 | 4106.5 | 21 | 24.0 | 1 | 120.8 | 781 |
| AMOCO PROD CO PICNIC FLATS | FORD CSG649 V6 ENG 60HP | 234.2 | 4107 | 4.3 | 9.0 | 0.17 | 193.2 | 700 |
| AMOCO PROD CO PICNIC FLATS | FORD LSG875 TRIPLEX1 90HP | 234.2 | 4107 | 7.3 | 10.0 | 0.2 | 175.3 | 700 |
| AMOCO PROD CO PICNIC FLATS | FORD LSG875 V8 ENG 90HP | 233.98 | 4106.5 | 7.3 | 10.0 | 0.2 | 175.3 | 700 |
| AMOCO PROD CO PICNIC FLATS | FORD CSG649 V6 ENG 60HP | 234.2 | 4107 | --- | 9.0 | 0.17 | 193.2 | 700 |
| AMOCO PROD CO PICNIC FLATS | FORD CSG649 V6 ENG 60HP | 234.2 | 4107 | --- | 9.0 | 0.2 | 193.2 | 700 |
| AMOCO PROD CO PICNIC FLATS | AJAX E-42 ENGINE 36HP | 234.2 | 4107 | --- | 11.0 | 0.5 | 32.1 | 565 |
| AMOCO PROD CO PICNIC FLATS | WAUKESHA L5790GL | 234.2 | 4107 | 21.5 | 18.0 | 1 | 115.8 | 0 |
| AMOCO PROD CO PICNIC FLATS | CAT NAT ENG RATED @ 323HP | 234.2 | 4107 | --- | 16.0 | 0.8 | 114.2 | 0 |
| AMOCO PROD CO SE TIFFANY | WAUKESHA L5788G 460 HP | 274.2 | 4099.9 | 13.1 | 0.0 | 0 | 0 | 70 |
| AMOCO PROD CO TIFFANY COMP STA | AJAX DPC-360 SERIAL#80754 | 273.6 | 4104.1 | 29.9 | 22.0 | 1 | 54.1 | 0 |
| AMOCO PROD CO TIFFANY COMP STA | AJAX DPC-800 SERIAL#82576 | 273.6 | 4104.1 | --- | 8.0 | 1.2 | 71.9 | 700 |
| AMOCO PROD CO TIFFANY COMP STA | WAUK, L70042GL SN:C11100 | 273.6 | 4104.1 | 22.2 | 20.0 | 1 | 124.8 | 727 |
| EL PASO NG CO BONDAD COMP STA | SOLAR T3000 SN:8009663R91 | 253.9 | 4109.1 | 82.4 | 27.0 | 6 | 39.4 | 625 |
| EL PASO NG CO BONDAD COMP STA | SOLAR T-3000 SN:1668C4R | 253.9 | 4109.1 | 82.4 | 27.0 | 6 | 39.6 | 625 |
| EL PASO NG CO BONDAD COMP STA | SOLAR CENTAR SN: 16684R | 253.9 | 4109.1 | 76.4 | 36.0 | 8 | 24.1 | 811 |
| EL PASO NG CO BONDAD COMP STA | (3) CENTAUR 40-T5300L | 253.9 | 4109.1 | 244.2 | 34.0 | 4 | 1.9 | 831 |
| EMERALD GAS OPERATING CO | AJAX DPC-360 ENGINE | 761.1 | 4105 | 31.3 | 20.0 | 0.83 | 134 | 700 |
| EMERALD GAS OPERATING CO | AJAX DPC360LE | 244.4 | 4118.3 | --- | 20.0 | 0.8 | 88.4 | 480 |
| PUBLIC SERVICE CO TIFFANY STATION | (3) SUPERIOR 8G825'S | 276.7 | 4103.3 | --- | 18.0 | 0.8 | 36.5 | 1340 |
| PUBLIC SERVICE CO TIFFANY STATION | ELASTEC SMARTASH RECOVERY | 276.7 | 4103.3 | 0.0051 | 0.0 ^(a) | 0 ^(a) | 0 ^(a) | 0 ^(a) |
| WEST GAS GATHERING INC | AJAX DPC-280 ENG.SN:77939 | 243.8 | 4108.5 | --- | 16.0 | 1 | 207.2 | 0 ^(a) |
| WEST GAS GATHERING INC | WAUKESHA L7042GL,BONDA D 2 | 243.8 | 4108.5 | --- | 18.0 | 7 | 231.2 | 0 ^(a) |
| WEST GAS GATHERING INC | WAUKESHA L7042GL, BONDAD2 | 243.8 | 4108.5 | --- | 18.0 | 0.7 | 231.2 | 0 ^(a) |
| WEST GAS GATHERING INC | GENERAC 74GN, MODEL:CG070 | 243.8 | 4108.5 | --- | 15.0 | 2 | 318.1 | 0 ^(a) |

^(a) Representative value assumed in the modeling

Table D-2. CDPHE Permit Emission Inventory (continued)

| Source Description | Unit ID | UTM Easting (km) | UTM Northing (km) | NOx (t/yr) | Stack Height (m) | Stack Diameter (m) | Stack Velocity (m/s) | Stack Temp (°K) |
|-------------------------------|---------------------------|------------------|-------------------|------------|--------------------|--------------------|----------------------|------------------|
| WEST GAS GATHERING INC | GENERAC 74GN,MODEL:CG 070 | 243.8 | 4108.5 | --- | 15.0 | 2 | 318.3 | 0 ^(a) |
| WEST GAS GATHERING INC | DEHYDRATOR #1, BONDAD 1 | 243.8 | 4108.5 | --- | 18.0 | 1.5 | 150 | 0 |
| WEST GAS GATHERING INC | DEHYDRATOR 2, BONDAD 2 | 243.8 | 4108.5 | --- | 0.0 ^(a) | 0 ^(a) | 0 ^(a) | 0 ^(a) |
| WILLIAMS FIELD SVCS PLA 9 STA | P & A DEHYDRATOR | --- | --- | 13 | --- | --- | --- | --- |
| WILLIAMS FIELD SVCS PLA 9 STA | ENERTEK NG DEHYDRATOR | --- | --- | 13 | --- | --- | --- | --- |
| WILLIAMS FIELD SVCS PLA 9 STA | WAUKESHA 1232HP SN#362478 | 239.8 | 4099 | --- | 22.0 | 1.03 | 97.4 | 711 |
| WILLIAMS FIELD SVCS PLA 9 STA | WAUKESHA 1232HP SN#360634 | 239.8 | 4099 | --- | 22.0 | 1.03 | 97.4 | 711 |
| WILLIAMS FIELD SVCS PLA 9 STA | WAUKESHA 1232HP SN#403117 | 239.8 | 4099 | --- | 22.0 | 1.03 | 97.4 | 711 |
| WILLIAMS FIELD SVCS PLA 9 STA | WAUKESHA 1232HP #C10461/4 | 239.8 | 4099 | --- | 22.0 | 1.03 | 97.4 | 711 |
| WILLIAMS FIELD SVCS PLA 9 STA | WAUKESHA 1160HP #C10461/5 | 239.8 | 4099 | --- | 22.0 | 1.03 | 97.4 | 711 |
| WILLIAMS FIELD SVCS PLA 9 STA | WAUKESHA 1109HP #C10607/1 | 239.8 | 4099 | --- | 22.0 | 1.03 | 97.4 | 711 |
| WILLIAMS FIELD SVCS PLA 9 STA | WAUKESHA 1109HP #C10607/2 | 239.8 | 4099 | --- | 22.0 | 1.03 | 97.4 | 711 |
| WILLIAMS FIELD SVCS PLA 9 STA | CAT 3304 GEN. SET - 72HP | 239.8 | 4099 | --- | 12.0 | 1 | 43.2 | 1120 |
| WILLIAMS FIELD SVCS PLA 9 STA | WAUKESHA 1117HP #C10985/1 | 239.8 | 4099 | 13 | 22.0 | 1.03 | 97.4 | 0 ^(a) |
| WILLIAMS FIELD SVCS PLA 9 STA | WAUKESHA 1117HP #C10985/3 | 239.8 | 4099 | 13 | 22.0 | 1.03 | 97.4 | 0 ^(a) |
| WILLIAMS FIELD SVCS PLA 9 STA | WAUKESHA 1117HP #C10985/8 | 239.8 | 4099 | --- | 22.0 | 1.03 | 97.4 | 711 |
| WILLIAMS FIELD SVCS PLA 9 STA | WAUKESHA 1117HP #C10985/7 | 239.8 | 4099 | --- | 22.0 | 1.03 | 97.4 | 711 |
| WILLIAMS FIELD SVCS PLA 9 STA | WAUKESHA 1232HP #C11059/1 | 239.8 | 4099 | --- | 22.0 | 1.03 | 97.4 | 711 |
| WILLIAMS FIELD SVCS PLA 9 STA | WAUKESHA 895HP #13 | 239.8 | 4099 | --- | 22.0 | 1 | 97.4 | 0 ^(a) |
| WILLIAMS FIELD SVCS PLA 9 STA | WAUKESHA 895HP #14 | 239.8 | 4099 | --- | 22.0 | 1 | 97.4 | 0 ^(a) |
| WILLIAMS FIELD SVCS PLA 9 STA | CATERPILLAR 166HP ENGINE | 239.8 | 4099 | --- | 8.0 | 0.4 | 145.7 | 0 ^(a) |

^(a) Representative value assumed in the modeling

Table D-3. Tribal Near Field Emission Source Modeling Input Values

| Source Count | Source Description | Unit ID | NOx Emission Rate (g/s) | UTM | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|------------------------------------|---------|-------------------------|--------------|---------------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | | Easting (km) | Northing (km) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 1 | Florida River Compression Facility | tr1 | 2.6 | 243.740 | 4115.890 | 3.25 | 0.307848 | 15.83 | 685.13 | N/A | N/A | 1950 |
| 2 | Florida River Compression Facility | tr2 | 2.9 | 243.740 | 4115.890 | 4.09 | 0.307848 | 18.21 | 696.54 | N/A | N/A | 1950 |
| 3 | Florida River Compression Facility | tr3 | 0.9 | 243.740 | 4115.890 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 1950 |
| 4 | Florida River Compression Facility | tr4 | 1.4 | 243.740 | 4115.890 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 1950 |
| 5 | Florida River Compression Facility | tr5 | 0.2 | 243.740 | 4115.890 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 1950 |
| 6 | Florida River Compression Facility | tr6 | 0.1 | 243.740 | 4115.890 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 1950 |
| 7 | Florida River Compression Facility | tr7 | 0.1 | 243.740 | 4115.890 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 1950 |
| 8 | Florida River Compression Facility | tr8 | 0.6 | 243.740 | 4115.890 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 1950 |
| 9 | Four Queens Central Facility | tr9 | 1.1 | 224.850 | 4107.440 | 0.91 | 0.4572 | 42.76 | 614.82 | N/A | N/A | 2011 |
| 10 | Four Queens Central Facility | tr10 | 1.1 | 224.850 | 4107.440 | 0.91 | 0.4572 | 42.76 | 614.82 | N/A | N/A | 2011 |
| 11 | Four Queens Central Facility | tr11 | 1.1 | 224.850 | 4107.440 | 0.91 | 0.4572 | 42.76 | 614.82 | N/A | N/A | 2011 |
| 12 | Four Queens Central Facility | tr12 | 0.4 | 224.850 | 4107.440 | 3.05 | 0.1524 | 9.75 | 847.04 | N/A | N/A | 2011 |
| 13 | Salvador I/II Central Facility | tr13 | 0.8 | 267.570 | 4106.450 | 6.86 | 0.353568 | 36.42 | 630.37 | N/A | N/A | 1950 |
| 14 | Salvador I/II Central Facility | tr14 | 1.0 | 267.570 | 4106.450 | 6.71 | 0.3048 | 47.85 | 645.93 | N/A | N/A | 1950 |
| 15 | Salvador I/II Central Facility | tr15 | 1.0 | 267.570 | 4106.450 | 6.71 | 0.3048 | 47.85 | 645.93 | N/A | N/A | 1950 |
| 16 | Salvador I/II Central Facility | tr16 | 0.5 | 267.570 | 4106.450 | 5.49 | 0.21336 | 56.85 | 644.26 | N/A | N/A | 1950 |
| 17 | Argenta CDP Compressor Facility | tr17 | 0.7 | 239.180 | 4113.220 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 2011 |
| 18 | Argenta CDP Compressor Facility | tr18 | 0.7 | 239.180 | 4113.220 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 2011 |
| 19 | Argenta CDP Compressor Facility | tr19 | 2.2 | 239.180 | 4113.220 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 2011 |
| 20 | Argenta CDP Compressor Facility | tr20 | 4.8 | 239.180 | 4113.220 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 2011 |
| 21 | Argenta CDP Compressor Facility | tr21 | 0.7 | 239.180 | 4113.220 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 2011 |
| 22 | Argenta CDP Compressor Facility | tr22 | 0.7 | 239.180 | 4113.220 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 2011 |
| 23 | Argenta CDP Compressor Facility | tr23 | 0.7 | 239.180 | 4113.220 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 2011 |
| 24 | Coyote Gulch Treating Plant | tr24 | 1.2 | 227.800 | 4100.950 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 1889 |
| 25 | Coyote Gulch Treating Plant | tr25 | 1.2 | 227.800 | 4100.950 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 1889 |
| 26 | Coyote Gulch Treating Plant | tr26 | 0.9 | 227.800 | 4100.950 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 1889 |
| 27 | Coyote Gulch Treating Plant | tr27 | 0.6 | 227.800 | 4100.950 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 1889 |
| 28 | Coyote Gulch Treating Plant | tr28 | 0.6 | 227.800 | 4100.950 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 1889 |
| 29 | Coyote Gulch Treating Plant | tr29 | 0.1 | 227.800 | 4100.950 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 1889 |
| 30 | Coyote Gulch Treating Plant | tr30 | 0.7 | 227.800 | 4100.950 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 1889 |
| 31 | Coyote Gulch Treating Plant | tr31 | 1.0 | 227.800 | 4100.950 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 1889 |
| 32 | Coyote Gulch Treating Plant | tr32 | 0.0 | 227.800 | 4100.950 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 1889 |
| 33 | Bondad Compressor Station | tr33 | 2.4 | 253.466 | 4109.500 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 2060 |
| 34 | Bondad Compressor Station | tr34 | 2.4 | 253.466 | 4109.500 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 2060 |
| 35 | Bondad Compressor Station | tr35 | 2.4 | 253.466 | 4109.500 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 2060 |

N/A – Not available

Table D-3. Tribal Near Field Emission Source Modeling Input Values (continued)

| Source Count | Source Description | Unit ID | NOx Emission Rate (g/s) | UTM | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|---------------------------------|---------|-------------------------|--------------|---------------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | | Easting (km) | Northing (km) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 36 | La Plata B Compressor Station | tr36 | 2.0 | 250.740 | 4114.500 | 15.24 | 1.0668 | 30.48 | 783.15 | N/A | N/A | 2011 |
| 37 | La Plata B Compressor Station | tr37 | 2.0 | 250.740 | 4114.500 | 15.24 | 1.0668 | 30.48 | 783.15 | N/A | N/A | 2011 |
| 38 | La Plata B Compressor Station | tr38 | 0.1 | 250.740 | 4114.500 | 15.24 | 1.28016 | 243.84 | 460.93 | N/A | N/A | 2011 |
| 39 | La Plata B Compressor Station | tr39 | 0.1 | 250.740 | 4114.500 | 15.24 | 1.28016 | 243.84 | 460.93 | N/A | N/A | 2011 |
| 40 | Tiffany Compressor Station | tr40 | 1.6 | 277.186 | 4102.670 | 5.49 | 0.24384 | 11.13 | 999.82 | N/A | N/A | 2011 |
| 41 | Tiffany Compressor Station | tr41 | 1.6 | 277.186 | 4102.670 | 5.49 | 0.24384 | 11.13 | 999.82 | N/A | N/A | 2011 |
| 42 | Tiffany Compressor Station | tr42 | 1.6 | 277.186 | 4102.670 | 5.49 | 0.24384 | 11.13 | 999.82 | N/A | N/A | 2011 |
| 43 | Arkansas Loop Plant | tr43 | 0.5 | 252.900 | 4103.610 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 2205 |
| 44 | Arkansas Loop Plant | tr44 | 0.5 | 252.900 | 4103.610 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 2205 |
| 45 | Arkansas Loop Plant | tr45 | 1.0 | 252.900 | 4103.610 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 2205 |
| 46 | Arkansas Loop Plant | tr46 | 1.1 | 252.900 | 4103.610 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 2205 |
| 47 | Arkansas Loop Plant | tr47 | 1.0 | 252.900 | 4103.610 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 2205 |
| 48 | Arkansas Loop Plant | tr48 | 1.0 | 252.900 | 4103.610 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 2205 |
| 49 | Arkansas Loop Plant | tr49 | 0.5 | 252.900 | 4103.610 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 2205 |
| 50 | Arkansas Loop Plant | tr50 | 0.5 | 252.900 | 4103.610 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 2205 |
| 51 | Arkansas Loop Plant | tr51 | 0.5 | 252.900 | 4103.610 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 2205 |
| 52 | Arkansas Loop Plant | tr52 | 0.5 | 252.900 | 4103.610 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 2205 |
| 53 | Arkansas Loop Plant | tr53 | 0.6 | 252.900 | 4103.610 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 2205 |
| 54 | Arkansas Loop Plant | tr54 | 0.0 | 252.900 | 4103.610 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 2205 |
| 55 | Capote Compressor Station | tr55 | 0.6 | 249.500 | 4105.400 | 2.34 | 1.487424 | 11.50 | 619.47 | N/A | N/A | 2071 |
| 56 | Capote Compressor Station | tr56 | 0.6 | 249.500 | 4105.400 | 2.34 | 1.487424 | 11.50 | 619.47 | N/A | N/A | 2071 |
| 57 | Capote Compressor Station | tr57 | 0.6 | 249.500 | 4105.400 | 2.34 | 1.487424 | 11.50 | 619.47 | N/A | N/A | 2071 |
| 58 | Capote Compressor Station | tr58 | 0.6 | 249.500 | 4105.400 | 2.34 | 1.487424 | 11.50 | 619.47 | N/A | N/A | 2071 |
| 59 | Capote Compressor Station | tr59 | 0.6 | 249.500 | 4105.400 | 2.34 | 1.487424 | 11.50 | 619.47 | N/A | N/A | 2071 |
| 60 | Capote Compressor Station | tr60 | 0.6 | 249.500 | 4105.400 | 2.34 | 1.487424 | 11.50 | 619.47 | N/A | N/A | 2071 |
| 61 | Sidewinder Compressor Station | tr61 | 5.7 | 246.900 | 4101.960 | 1.76 | 0.92964 | 11.50 | 619.47 | N/A | N/A | 2017 |
| 62 | Sidewinder Compressor Station | tr62 | 0.6 | 246.900 | 4101.960 | 1.76 | 0.92964 | 11.50 | 619.47 | N/A | N/A | 2017 |
| 63 | Sidewinder Compressor Station | tr63 | 0.1 | 246.900 | 4101.960 | 1.76 | 0.92964 | 11.50 | 619.47 | N/A | N/A | 2017 |
| 64 | Diamond Back Compressor Station | tr64 | 0.6 | 246.900 | 4101.960 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 2017 |
| 65 | Diamond Back Compressor Station | tr65 | 0.6 | 246.900 | 4101.960 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 2017 |
| 66 | Diamond Back Compressor Station | tr66 | 0.6 | 246.900 | 4101.960 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 2017 |
| 67 | Bondad Compressor Station | tr67 | 0.1 | 243.630 | 4098.800 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 2060 |
| 68 | Bondad Compressor Station | tr68 | 0.6 | 243.630 | 4098.800 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 2060 |
| 69 | Bondad Compressor Station | tr69 | 0.6 | 243.630 | 4098.800 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 2060 |
| 70 | Bondad Compressor Station | tr70 | 0.6 | 243.630 | 4098.800 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 2060 |

N/A – Not available

Table D-3. Tribal Near Field Emission Source Modeling Input Values (continued)

| Source Count | Source Description | Unit ID | NOx Emission Rate (g/s) | UTM | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|---------------------------------|---------|-------------------------|--------------|---------------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | | Easting (km) | Northing (km) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 71 | Bondad Compressor Station | tr71 | 0.6 | 243.630 | 4098.800 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 2060 |
| 72 | Bondad Compressor Station | tr72 | 0.6 | 243.630 | 4098.800 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 2060 |
| 73 | Bondad Compressor Station | tr73 | 0.6 | 243.630 | 4098.800 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 2060 |
| 74 | Bondad Compressor Station | tr74 | 0.6 | 243.630 | 4098.800 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 2060 |
| 75 | Bondad Compressor Station | tr75 | 0.6 | 243.630 | 4098.800 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 2060 |
| 76 | Bondad Compressor Station | tr76 | 0.0 | 243.630 | 4098.800 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 2060 |
| 77 | Antler Gas Plant | tr77 | 1.5 | 231.120 | 4100.900 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 1950 |
| 78 | Antler Gas Plant | tr78 | 0.1 | 231.120 | 4100.900 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 1950 |
| 79 | Antler Gas Plant | tr79 | 1.5 | 231.120 | 4100.900 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 1950 |
| 80 | Antler Gas Plant | tr80 | 0.1 | 231.120 | 4100.900 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 1950 |
| 81 | Antler Gas Plant | tr81 | 0.9 | 231.120 | 4100.900 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 1950 |
| 82 | Antler Gas Plant | tr82 | 0.0 | 231.120 | 4100.900 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 1950 |
| 83 | Antler Gas Plant | tr83 | 0.7 | 231.120 | 4100.900 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 1950 |
| 84 | Antler Gas Plant | tr84 | 0.7 | 231.120 | 4100.900 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 1950 |
| 85 | Coyote Gulch Compressor Station | tr85 | 0.6 | 229.250 | 4100.730 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 1940 |
| 86 | Coyote Gulch Compressor Station | tr86 | 0.6 | 229.250 | 4100.730 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 1940 |
| 87 | Coyote Gulch Compressor Station | tr87 | 0.6 | 229.250 | 4100.730 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 1940 |
| 88 | Coyote Gulch Compressor Station | tr88 | 0.7 | 229.250 | 4100.730 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 1940 |
| 89 | Coyote Gulch Compressor Station | tr89 | 0.6 | 229.250 | 4100.730 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 1940 |
| 90 | Coyote Gulch Compressor Station | tr90 | 0.6 | 229.250 | 4100.730 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 1940 |
| 91 | Coyote Gulch Compressor Station | tr91 | 0.6 | 229.250 | 4100.730 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 1940 |
| 92 | Coyote Gulch Compressor Station | tr92 | 0.1 | 229.250 | 4100.730 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 1940 |
| 93 | South Ignacio Central Delivery | tr93 | 3.6 | 266.240 | 4104.300 | 2.05 | 1.115568 | 11.50 | 619.47 | N/A | N/A | 1950 |
| 94 | South Ignacio Central Delivery | tr94 | 0.5 | 266.240 | 4104.300 | 2.05 | 1.115568 | 11.50 | 619.47 | N/A | N/A | 1950 |
| 95 | South Ignacio Central Delivery | tr95 | 0.5 | 266.240 | 4104.300 | 2.05 | 1.115568 | 11.50 | 619.47 | N/A | N/A | 1950 |
| 96 | South Ignacio Central Delivery | tr96 | 0.6 | 266.240 | 4104.300 | 2.05 | 1.115568 | 11.50 | 619.47 | N/A | N/A | 1950 |
| 97 | La Plata A Compressor Station | tr97 | 0.9 | 247.630 | 4114.520 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 2021 |
| 98 | La Plata A Compressor Station | tr98 | 0.5 | 247.630 | 4114.520 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 2021 |
| 99 | Treating Site #1 | tr99 | 0.3 | 263.132 | 4099.757 | 8.97 | 0.3048 | 34.63 | 823.71 | N/A | N/A | 2114 |
| 100 | Treating Site #1 | tr100 | 0.3 | 263.135 | 4099.749 | 8.94 | 0.3048 | 34.63 | 823.71 | N/A | N/A | 2132 |
| 101 | Treating Site #1 | tr101 | 0.1 | 263.125 | 4099.702 | 2.21 | 0.0762 | 41.39 | 977.59 | N/A | N/A | 2132 |
| 102 | Treating Site #1 | tr102 | 0.6 | 263.073 | 4099.743 | 2.51 | 0.0762 | 62.76 | 810.37 | N/A | N/A | 2132 |
| 103 | Treating Site #1 | tr103 | 0.3 | 263.139 | 4099.692 | 4.08 | 0.100584 | 112.29 | 701.48 | N/A | N/A | 2132 |
| 104 | Treating Site #2 | tr104 | 0.3 | 255.827 | 4099.163 | 8.89 | 0.3048 | 34.63 | 823.71 | N/A | N/A | 2093 |
| 105 | Treating Site #2 | tr105 | 0.3 | 255.831 | 4099.156 | 8.92 | 0.3048 | 34.63 | 823.71 | N/A | N/A | 2093 |

N/A – Not available

Table D-3. Tribal Near Field Emission Source Modeling Input Values (continued)

| Source Count | Source Description | Unit ID | NOx Emission Rate (g/s) | UTM | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|--------------------|---------|-------------------------|--------------|---------------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | | Easting (km) | Northing (km) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 106 | Treating Site #2 | tr106 | 0.1 | 255.843 | 4099.114 | 2.29 | 0.0762 | 41.39 | 977.59 | N/A | N/A | 2093 |
| 107 | Treating Site #2 | tr107 | 0.6 | 255.835 | 4099.149 | 5.77 | 0.3048 | 54.53 | 677.59 | N/A | N/A | 2093 |
| 108 | Treating Site #4 | tr108 | 0.2 | 252.856 | 4098.978 | 7.70 | 0.204216 | 49.59 | 858.15 | N/A | N/A | 2134 |
| 109 | Treating Site #4 | tr109 | 0.2 | 252.593 | 4098.899 | 7.67 | 0.204216 | 49.59 | 858.15 | N/A | N/A | 2135 |
| 110 | Treating Site #4 | tr110 | 0.3 | 252.693 | 4098.944 | 8.93 | 0.3048 | 34.63 | 823.71 | N/A | N/A | 2135 |
| 111 | Treating Site #4 | tr111 | 1.5 | 252.645 | 4098.973 | 4.00 | 0.100584 | 57.76 | 818.71 | N/A | N/A | 2135 |
| 112 | Treating Site #4 | tr112 | 0.9 | 252.594 | 4098.915 | 2.86 | 0.100584 | 83.24 | 977.59 | N/A | N/A | 2135 |
| 113 | Treating Site #4 | tr113 | 0.3 | 252.663 | 4098.981 | 4.08 | 0.100584 | 112.29 | 701.48 | N/A | N/A | 2135 |
| 114 | Treating Site #5 | tr114 | 0.1 | 249.846 | 4100.260 | 6.83 | 0.1524 | 49.53 | 831.48 | N/A | N/A | 2021 |
| 115 | Treating Site #5 | tr115 | 2.1 | 249.844 | 4100.254 | 4.09 | 0.1524 | 49.53 | 831.48 | N/A | N/A | 2021 |
| 116 | Treating Site #5 | tr116 | 0.3 | 249.840 | 4100.245 | 8.81 | 0.3048 | 34.63 | 823.71 | N/A | N/A | 2021 |
| 117 | Treating Site #5 | tr117 | 0.2 | 249.850 | 4100.272 | 7.29 | 0.204216 | 49.62 | 858.15 | N/A | N/A | 2021 |
| 118 | Treating Site #5 | tr118 | 0.5 | 249.889 | 4100.222 | 2.87 | 0.0762 | 48.13 | 828.71 | N/A | N/A | 2021 |
| 119 | Treating Site #6 | tr119 | 0.3 | 246.728 | 4102.322 | 8.79 | 0.3048 | 34.63 | 823.71 | N/A | N/A | 2071 |
| 120 | Treating Site #6 | tr120 | 0.3 | 246.729 | 4102.311 | 8.92 | 0.3048 | 34.63 | 823.71 | N/A | N/A | 2071 |
| 121 | Treating Site #6 | tr121 | 0.3 | 246.730 | 4102.278 | 4.08 | 0.100584 | 112.29 | 701.48 | N/A | N/A | 2071 |
| 122 | Treating Site #6 | tr122 | 1.5 | 246.731 | 4102.284 | 3.63 | 0.100584 | 57.79 | 818.71 | N/A | N/A | 2071 |
| 123 | Treating Site #6 | tr123 | 0.1 | 246.754 | 4102.310 | 3.79 | 0.064008 | 59.62 | 977.59 | N/A | N/A | 2021 |
| 124 | Treating Site #6 | tr124 | 0.3 | 246.754 | 4102.310 | 8.92 | 0.3048 | 34.63 | 823.71 | N/A | N/A | 2021 |
| 125 | Treating Site #7 | tr125 | 1.5 | 240.427 | 4102.260 | 4.11 | 0.100584 | 57.79 | 818.71 | N/A | N/A | 1964 |
| 126 | Treating Site #7 | tr126 | 0.5 | 240.406 | 4102.260 | 3.83 | 0.100584 | 27.07 | 828.71 | N/A | N/A | 1964 |
| 127 | Treating Site #7 | tr127 | 2.1 | 240.484 | 4102.237 | 4.09 | 0.1524 | 49.53 | 831.48 | N/A | N/A | 1954 |
| 128 | Treating Site #7 | tr128 | 0.1 | 240.491 | 4102.241 | 6.61 | 0.1524 | 49.53 | 831.48 | N/A | N/A | 1954 |
| 129 | Treating Site #7 | tr129 | 0.3 | 240.506 | 4102.245 | 8.73 | 0.3048 | 34.63 | 823.71 | N/A | N/A | 1954 |
| 130 | Treating Site #9 | tr130 | 0.2 | 236.635 | 4106.568 | 7.62 | 0.204216 | 49.62 | 858.15 | N/A | N/A | 2193 |
| 131 | Treating Site #9 | tr131 | 0.2 | 236.636 | 4106.559 | 7.70 | 0.204216 | 49.62 | 858.15 | N/A | N/A | 2193 |
| 132 | Treating Site #9 | tr132 | 0.2 | 236.637 | 4106.549 | 7.71 | 0.204216 | 49.62 | 858.15 | N/A | N/A | 2193 |
| 133 | Treating Site #9 | tr133 | 0.1 | 236.622 | 4106.536 | 7.62 | 0.0762 | 41.39 | 977.59 | N/A | N/A | 2193 |
| 134 | Treating Site #6B | tr134 | 5.5 | 246.630 | 4103.560 | 2.69 | 1.115568 | 10.56 | 740.77 | N/A | N/A | 2021 |
| 135 | Treating Site #6B | tr135 | 0.5 | 246.630 | 4103.560 | 2.69 | 1.115568 | 9.29 | 656.51 | N/A | N/A | 2021 |
| 136 | Treating Site #6B | tr136 | 0.8 | 246.630 | 4103.560 | 0.77 | 0.277368 | 19.13 | 705.58 | N/A | N/A | 2021 |
| 137 | Treating Site #6B | tr137 | 0.3 | 246.630 | 4103.560 | 1.64 | 1.115568 | 10.56 | 712.99 | N/A | N/A | 2021 |
| 138 | Treating Site #7B | tr138 | 5.5 | 240.350 | 4103.780 | 0.77 | 1.115568 | 19.13 | 705.58 | N/A | N/A | 2011 |
| 139 | Treating Site #7B | tr139 | 4.1 | 240.350 | 4103.780 | 1.76 | 1.115568 | 16.62 | 744.47 | N/A | N/A | 2011 |
| 140 | Treating Site #7B | tr140 | 0.6 | 240.350 | 4103.780 | 1.76 | 1.115568 | 16.62 | 744.47 | N/A | N/A | 2011 |

N/A – Not available

Table D-3. Tribal Near Field Emission Source Modeling Input Values (continued)

| Source Count | Source Description | Unit ID | NOx Emission Rate (g/s) | UTM | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|------------------------------|---------|-------------------------|--------------|---------------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | | Easting (km) | Northing (km) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 141 | Treating Site #7B | tr141 | 0.1 | 240.350 | 4103.780 | 0.70 | 0.277368 | 12.62 | 798.48 | N/A | N/A | 2093 |
| 142 | Treating Site #8 | tr142 | 0.5 | 239.015 | 4107.000 | 2.69 | 0.557784 | 10.56 | 607.74 | N/A | N/A | 2093 |
| 143 | Treating Site #8 | tr143 | 0.5 | 239.015 | 4107.000 | 2.69 | 0.557784 | 10.56 | 607.74 | N/A | N/A | 2134 |
| 144 | Treating Site #8 | tr144 | 5.5 | 239.015 | 4107.000 | 2.69 | 1.115568 | 10.56 | 740.77 | N/A | N/A | 2135 |
| 145 | Treating Site #8 | tr145 | 0.5 | 239.015 | 4107.000 | 2.69 | 1.115568 | 9.29 | 656.51 | N/A | N/A | 2135 |
| 146 | Treating Site #8 | tr146 | 0.3 | 239.015 | 4107.000 | 0.77 | 0.277368 | 19.13 | 705.58 | N/A | N/A | 2135 |
| 147 | Treating Site #8 | tr147 | 0.1 | 239.015 | 4107.000 | 1.16 | 0.277368 | 12.60 | 798.48 | N/A | N/A | 2135 |
| 148 | PLA-9 Central Delivery Point | tr148 | 0.3 | 239.800 | 4099.200 | 6.71 | 0.313944 | 48.87 | 699.82 | N/A | N/A | 2135 |
| 149 | PLA-9 Central Delivery Point | tr149 | 0.3 | 239.800 | 4099.200 | 6.71 | 0.313944 | 48.87 | 699.82 | N/A | N/A | 2021 |
| 150 | PLA-9 Central Delivery Point | tr150 | 0.3 | 239.800 | 4099.200 | 6.71 | 0.313944 | 48.87 | 699.82 | N/A | N/A | 2021 |
| 151 | PLA-9 Central Delivery Point | tr151 | 0.3 | 239.800 | 4099.200 | 6.71 | 0.313944 | 48.87 | 699.82 | N/A | N/A | 2021 |
| 152 | PLA-9 Central Delivery Point | tr152 | 0.3 | 239.800 | 4099.200 | 6.71 | 0.313944 | 48.87 | 699.82 | N/A | N/A | 2021 |
| 153 | PLA-9 Central Delivery Point | tr153 | 0.3 | 239.800 | 4099.200 | 6.71 | 0.313944 | 48.87 | 699.82 | N/A | N/A | 2021 |
| 154 | PLA-9 Central Delivery Point | tr154 | 0.3 | 239.800 | 4099.200 | 6.71 | 0.313944 | 48.87 | 699.82 | N/A | N/A | 2071 |
| 155 | PLA-9 Central Delivery Point | tr155 | 0.3 | 239.800 | 4099.200 | 6.71 | 0.313944 | 48.87 | 699.82 | N/A | N/A | 2071 |
| 156 | PLA-9 Central Delivery Point | tr156 | 0.3 | 239.800 | 4099.200 | 6.71 | 0.313944 | 48.87 | 699.82 | N/A | N/A | 2071 |
| 157 | PLA-9 Central Delivery Point | tr157 | 0.3 | 239.800 | 4099.200 | 6.71 | 0.313944 | 48.87 | 699.82 | N/A | N/A | 2071 |
| 158 | PLA-9 Central Delivery Point | tr158 | 0.3 | 239.800 | 4099.200 | 6.71 | 0.313944 | 48.87 | 699.82 | N/A | N/A | 2021 |
| 159 | PLA-9 Central Delivery Point | tr159 | 0.3 | 239.800 | 4099.200 | 6.71 | 0.313944 | 48.87 | 699.82 | N/A | N/A | 2021 |
| 160 | PLA-9 Central Delivery Point | tr160 | 0.3 | 239.800 | 4099.200 | 6.71 | 0.313944 | 48.87 | 699.82 | N/A | N/A | 1964 |
| 161 | PLA-9 Central Delivery Point | tr161 | 1.1 | 239.800 | 4099.200 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 1964 |
| 162 | Ignacio Plant | tr162 | 0.2 | 252.700 | 4114.400 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 1954 |
| 163 | Ignacio Plant | tr163 | 0.3 | 252.700 | 4114.400 | 2.60 | 0.277368 | 1.86 | 674.94 | N/A | N/A | 1954 |
| 164 | Ignacio Plant | tr164 | 0.3 | 252.700 | 4114.400 | 2.60 | 0.277368 | 1.86 | 674.94 | N/A | N/A | 1954 |
| 165 | Ignacio Plant | tr165 | 0.3 | 252.700 | 4114.400 | 2.60 | 0.326136 | 1.86 | 674.94 | N/A | N/A | 2193 |
| 166 | Ignacio Plant | tr166 | 0.6 | 252.700 | 4114.400 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 2193 |
| 167 | Ignacio Plant | tr167 | 0.9 | 252.915 | 4114.521 | 2.79 | 0.298704 | 16.00 | 646.24 | N/A | N/A | 2193 |
| 168 | Ignacio Plant | tr168 | 6.3 | 252.908 | 4114.445 | 2.32 | 0.185928 | 1.86 | 628.64 | N/A | N/A | 2193 |
| 169 | Ignacio Plant | tr169 | 6.3 | 252.908 | 4114.445 | 2.32 | 0.185928 | 1.86 | 628.64 | N/A | N/A | 2021 |
| 170 | Ignacio Plant | tr170 | 6.3 | 252.908 | 4114.445 | 2.32 | 0.185928 | 1.86 | 628.64 | N/A | N/A | 2021 |
| 171 | Ignacio Plant | tr171 | 6.3 | 252.908 | 4114.445 | 2.32 | 0.185928 | 1.86 | 628.64 | N/A | N/A | 2021 |
| 172 | Ignacio Plant | tr172 | 6.3 | 252.908 | 4114.445 | 2.32 | 0.185928 | 1.86 | 628.64 | N/A | N/A | 2021 |
| 173 | Ignacio Plant | tr173 | 6.3 | 252.908 | 4114.445 | 2.32 | 0.185928 | 1.86 | 628.64 | N/A | N/A | 2011 |
| 174 | Ignacio Plant | tr174 | 6.3 | 252.908 | 4114.445 | 2.32 | 0.185928 | 1.86 | 628.64 | N/A | N/A | 2011 |
| 175 | Ignacio Plant | tr175 | 6.6 | 252.908 | 4114.445 | 4.18 | 0.185928 | 1.86 | 659.51 | N/A | N/A | 2011 |

N/A – Not available

Table D-3. Tribal Near Field Emission Source Modeling Input Values (continued)

| Source Count | Source Description | Unit ID | NOx Emission Rate (g/s) | UTM | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|----------------------------------|---------|-------------------------|--------------|---------------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | | Easting (km) | Northing (km) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 176 | Ignacio Plant | tr176 | 6.6 | 252.767 | 4114.379 | 4.18 | 0.557784 | 12.43 | 674.94 | N/A | N/A | 2011 |
| 177 | Ignacio Plant | tr177 | 7.1 | 252.805 | 4114.378 | 4.18 | 0.557784 | 12.43 | 674.94 | N/A | N/A | 2011 |
| 178 | BP Amoco, Inc. | tr178 | 0.2 | 252.886 | 4114.517 | 4.36 | 0.326136 | 1.32 | 644.26 | N/A | N/A | 2011 |
| 179 | BP Amoco, Inc. | tr179 | 0.6 | 275200 | 4106100 | 3.05 | 0.1524 | 69.16 | 422.04 | N/A | N/A | 2007 |
| 180 | Texaco (Enervest Operating, LLC) | tr180 | 0.6 | 230000 | 4105000 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 2011 |
| 181 | Texaco (Enervest Operating, LLC) | tr181 | 0.6 | 234200 | 4119200 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 2365 |
| 182 | Texaco (Enervest Operating, LLC) | tr182 | 0.1 | 240200 | 4105000 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 2011 |
| 183 | Texaco (Enervest Operating, LLC) | tr183 | 0.1 | 230000 | 4104800 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 2011 |
| 184 | Red Willow Production Company | tr184 | 1.0 | 240000 | 4107000 | 3.05 | 0.1524 | 5.00 | 422.04 | N/A | N/A | 2132 |
| 185 | Williams Field Services | tr185 | 2.6 | 252000 | 4104000 | 6.71 | 0.1524 | 5.00 | 822.59 | N/A | N/A | 2239 |
| 186 | Williams Field Services | tr186 | 0.5 | 252000 | 4104000 | 6.71 | 0.310896 | 22.35 | 642.59 | N/A | N/A | 2239 |

N/A – Not available

Table D-4. Tribal Far Field Emission Source Modeling Input Values

| Source Count | Source Description | Unit ID | NOx Emission Rate (g/s) | UTM | | Stack Parameters | | | | Building | | Elevation (m) |
|--------------|-------------------------------|---------|-------------------------|-------------|--------------|------------------|--------------|----------------|-----------|------------|-----------|---------------|
| | | | | Easting (m) | Northing (m) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 1 | Amoco Production Company | TR001 | 0.62 | 243,740 | 4,115,890 | 4.57 | 0.457 | 15.80 | 588.6 | N/A | N/A | 2,164 |
| 2 | BP Amoco, Inc. | TR002 | 0.81 | 267,570 | 4,107,440 | 22.50 | 1.160 | 119.50 | 675.0 | N/A | N/A | 2,098 |
| 3 | BP Amoco, Inc. | TR003 | 1.00 | 267,570 | 4,107,440 | 22.00 | 1.000 | 157.00 | 703.0 | N/A | N/A | 2,098 |
| 4 | BP Amoco, Inc. | TR004 | 1.00 | 267,570 | 4,107,440 | 22.00 | 1.000 | 157.00 | 703.0 | N/A | N/A | 2,098 |
| 5 | BP Amoco, Inc. | TRE005 | 0.46 | 267,570 | 4,107,440 | 18.00 | 0.700 | 186.50 | 700.0 | N/A | N/A | 2,164 |
| 6 | El Paso Natural Gas Company | TR006 | 2.39 | 239,180 | 4,106,450 | 6.00 | 0.457 | 34.50 | 588.6 | N/A | N/A | 2,217 |
| 7 | El Paso Natural Gas Company | TR007 | 2.39 | 239,180 | 4,106,450 | 6.00 | 0.457 | 34.50 | 588.6 | N/A | N/A | 2,217 |
| 8 | El Paso Natural Gas Company | TR008 | 2.39 | 239,180 | 4,106,450 | 6.00 | 0.457 | 34.50 | 588.6 | N/A | N/A | 2,164 |
| 9 | Red Cedar Gathering Company | TR009 | 0.55 | 239,180 | 4,106,450 | 7.67 | 4.880 | 37.74 | 655.4 | N/A | N/A | 2,229 |
| 10 | Red Cedar Gathering Company | TR010 | 0.55 | 239,180 | 4,113,220 | 7.67 | 4.880 | 37.74 | 655.4 | N/A | N/A | 2,229 |
| 11 | Red Cedar Gathering Company | TR011 | 0.55 | 239,180 | 4,113,220 | 7.67 | 4.880 | 37.74 | 655.4 | N/A | N/A | 2,229 |
| 12 | Red Cedar Gathering Company | TR012 | 0.55 | 239,180 | 4,113,220 | 7.67 | 4.880 | 37.74 | 655.4 | N/A | N/A | 2,229 |
| 13 | Red Cedar Gathering Company | TR013 | 0.55 | 227,800 | 4,113,220 | 7.67 | 4.880 | 37.74 | 655.4 | N/A | N/A | 2,229 |
| 14 | Red Cedar Gathering Company | TR014 | 0.55 | 227,800 | 4,113,220 | 7.67 | 4.880 | 37.74 | 655.4 | N/A | N/A | 2,171 |
| 15 | Red Cedar Gathering Company | TR015 | 5.73 | 227,800 | 4,113,220 | 5.79 | 3.050 | 37.74 | 655.4 | N/A | N/A | 2,171 |
| 16 | Red Cedar Gathering Company | TR016 | 0.55 | 227,800 | 4,113,220 | 5.79 | 3.050 | 37.74 | 655.4 | N/A | N/A | 2,171 |
| 17 | Red Cedar Gathering Company | TR017 | 0.06 | 227,800 | 4,100,950 | 5.79 | 3.050 | 37.74 | 655.4 | N/A | N/A | 2,171 |
| 18 | Red Cedar Gathering Company | TR018 | 0.55 | 227,800 | 4,100,950 | 4.57 | 0.457 | 15.80 | 588.6 | N/A | N/A | 2,171 |
| 19 | Red Cedar Gathering Company | TR019 | 0.55 | 227,800 | 4,100,950 | 4.57 | 0.457 | 15.80 | 588.6 | N/A | N/A | 2,171 |
| 20 | Red Cedar Gathering Company | TR020 | 0.55 | 227,800 | 4,100,950 | 4.57 | 0.457 | 15.80 | 588.6 | N/A | N/A | 2,217 |
| 21 | SG Interests Inc. | TR021 | 0.93 | 227,800 | 4,100,950 | 6.71 | 3.660 | 37.74 | 655.4 | N/A | N/A | 2,098 |
| 22 | SG Interests Inc. | TR022 | 0.53 | 253,466 | 4,100,950 | 6.71 | 3.660 | 37.74 | 655.4 | N/A | N/A | 2,098 |
| 23 | SG Interests Inc. | TR023 | 0.53 | 253,466 | 4,100,950 | 6.71 | 3.660 | 37.74 | 655.4 | N/A | N/A | 2,098 |
| 24 | SG Interests Inc. | TR024 | 0.56 | 253,466 | 4,100,950 | 6.71 | 3.660 | 37.74 | 655.4 | N/A | N/A | 2,176 |
| 25 | Transwestern Pipeline Company | TR025 | 0.92 | 250,740 | 4,100,950 | 6.10 | 0.800 | 23.90 | 589.0 | N/A | N/A | 2,176 |
| 26 | Transwestern Pipeline Company | TR026 | 0.55 | 250,740 | 4,109,500 | 6.10 | 0.800 | 23.90 | 589.0 | N/A | N/A | 2,275 |
| 27 | BP Wolf Point | TR027 | 0.75 | 250,740 | 4,109,500 | 4.60 | 0.500 | 16.90 | 589.0 | N/A | N/A | 1,930 |
| 28 | BP Wolf Point | TR028 | 0.75 | 250,740 | 4,109,500 | 4.60 | 0.500 | 16.90 | 589.0 | N/A | N/A | 1,930 |
| 29 | BP Wolf Point | TR029 | 0.75 | 277,186 | 4,114,500 | 4.60 | 0.500 | 16.90 | 589.0 | N/A | N/A | 1,930 |
| 30 | BP Dry Creek | TR030 | 0.72 | 277,186 | 4,114,500 | 4.60 | 0.500 | 16.90 | 589.0 | N/A | N/A | 2,273 |
| 31 | BP Dry Creek | TR031 | 0.72 | 277,186 | 4,114,500 | 4.60 | 0.500 | 16.90 | 589.0 | N/A | N/A | 2,273 |
| 32 | BP Dry Creek | TR032 | 0.72 | 252,900 | 4,114,500 | 4.60 | 0.500 | 16.90 | 589.0 | N/A | N/A | 2,273 |
| 33 | BP Dry Creek | TR033 | 1.01 | 252,900 | 4,102,670 | 4.60 | 0.500 | 16.90 | 589.0 | N/A | N/A | 2,273 |
| 34 | BP Miria | TR034 | 0.31 | 252,900 | 4,102,670 | 6.10 | 0.800 | 23.90 | 589.0 | N/A | N/A | 2,228 |
| 35 | BP Miria | TR035 | 0.31 | 252,900 | 4,102,670 | 6.10 | 0.800 | 23.90 | 589.0 | N/A | N/A | 2,228 |

N/A – Not available

Table D-4. Tribal Far Field Emission Source Modeling Input Values (continued)

| Source Count | Source Description | Unit ID | NOx Emission Rate (g/s) | UTM | | Stack Parameters | | | | Building | | Elevation (m) |
|--------------|--------------------|---------|-------------------------|-------------|--------------|------------------|--------------|----------------|-----------|------------|-----------|---------------|
| | | | | Easting (m) | Northing (m) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 36 | BP Miria | TR036 | 0.31 | 252,900 | 4,103,610 | 6.10 | 0.800 | 23.90 | 589.0 | N/A | N/A | 2,228 |
| 37 | BP Empanada | TR037 | 0.72 | 242,157 | 4,104,930 | 4.60 | 0.500 | 16.90 | 589.0 | N/A | N/A | 2,098 |
| 38 | BP Empanada | TR038 | 0.72 | 242,157 | 4,104,930 | 4.60 | 0.500 | 16.90 | 589.0 | N/A | N/A | 2,098 |
| 39 | BP Empanada | TR039 | 0.72 | 242,157 | 4,104,930 | 4.60 | 0.500 | 16.90 | 589.0 | N/A | N/A | 2,098 |

N/A – Not available

Appendix E – SUIT RFS Emission Inventory

| Table | Page |
|-----------------------------------------------------|-------------|
| E-1. SUIT RFS Emission Source Modeling Input Values | 187 |

Table E-1. SUIT RFS Emission Source Modeling Input Values

| Source Count | Source Description | Unit ID | NOx Emission Rate (g/s) | UTM | | Stack Parameters | | | | Building | | Elevation (m) |
|--------------|-------------------------------------|---------|-------------------------|-------------|--------------|------------------|--------------|----------------|-----------|------------|-----------|---------------|
| | | | | Easting (m) | Northing (m) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 1 | Allison (500 hp total) | al001 | 0.21 | 273,982 | 4,099,639 | 7.62 | 0.30 | 37.70 | 636.00 | N/A | N/A | 1,963 |
| 2 | Well emissions | al002 | 0.10 | 273,982 | 4,099,639 | 5.00 | 0.20 | 5.00 | 500.00 | N/A | N/A | 1,963 |
| 3 | Amoco 1 (5000 total) | al003 | 1.04 | 268,244 | 4,118,871 | 10.00 | 0.49 | 64.00 | 796.90 | N/A | N/A | 2,074 |
| 4 | Amoco 1 (5000 total) | al004 | 1.04 | 256,705 | 4,114,771 | 10.00 | 0.49 | 64.00 | 796.90 | N/A | N/A | 2,011 |
| 5 | Amoco ECBM 3 (5000 total) | al005 | 1.04 | 268,254 | 4,118,871 | 10.00 | 0.49 | 64.00 | 796.90 | N/A | N/A | 2,074 |
| 6 | Amoco ECBM 3 (5000 total) | al006 | 1.04 | 256,715 | 4,114,771 | 10.00 | 0.49 | 64.00 | 796.90 | N/A | N/A | 2,011 |
| 7 | Well emissions | al007 | 0.10 | 256,715 | 4,114,771 | 5.00 | 0.20 | 5.00 | 500.00 | N/A | N/A | 2,011 |
| 8 | Red Cedar Bondad 1 (5000 total) | al008 | 1.04 | 243,994 | 4,108,081 | 10.00 | 0.49 | 64.00 | 796.90 | N/A | N/A | 1,889 |
| 9 | Red Cedar Bondad 2 (5000 total) | al009 | 1.04 | 243,984 | 4,108,081 | 10.00 | 0.49 | 64.00 | 796.90 | N/A | N/A | 1,889 |
| 10 | Well emissions | al010 | 0.10 | 238,626 | 4,101,428 | 5.00 | 0.20 | 5.00 | 500.00 | N/A | N/A | 2,013 |
| 11 | Well emissions | al012 | 0.10 | 240,659 | 4,105,185 | 5.00 | 0.20 | 5.00 | 500.00 | N/A | N/A | 1,950 |
| 12 | Amoco ECBM 1 (5000hp total) | al013 | 1.04 | 252,132 | 4,119,478 | 10.00 | 0.49 | 64.00 | 796.90 | N/A | N/A | 2,072 |
| 13 | Amoco ECBM 2 (5000hp total) | al014 | 1.04 | 252,142 | 4,119,478 | 10.00 | 0.49 | 64.00 | 796.90 | N/A | N/A | 2,072 |
| 14 | Well emissions | al015 | 0.10 | 252,142 | 4,119,478 | 5.00 | 0.20 | 5.00 | 500.00 | N/A | N/A | 2,072 |
| 15 | Well emissions | al023 | 0.10 | 233,700 | 4,107,400 | 5.00 | 0.20 | 5.00 | 500.00 | N/A | N/A | 2,160 |
| 16 | Well emissions | al027 | 0.10 | 233,700 | 4,106,869 | 5.00 | 0.20 | 5.00 | 500.00 | N/A | N/A | 1,987 |
| 17 | Burlington Northern 1 (6400 hp tot) | al028 | 0.89 | 230,651 | 4,100,957 | 10.00 | 0.46 | 30.97 | 635.78 | N/A | N/A | 1,987 |
| 18 | Burlington Northern 1 (6400 hp tot) | al029 | 0.89 | 230,661 | 4,100,957 | 10.00 | 0.46 | 30.97 | 635.78 | N/A | N/A | 1,950 |
| 19 | Burlington Northern 1 (6400 hp tot) | al030 | 0.89 | 230,671 | 4,100,957 | 10.00 | 0.46 | 30.97 | 635.78 | N/A | N/A | 1,950 |
| 20 | Well emissions | al031 | 0.10 | 230,641 | 4,100,957 | 5.00 | 0.20 | 5.00 | 500.00 | N/A | N/A | 1,950 |
| 21 | El Paso gas 5000hp turbine | al032 | 2.08 | 237,293 | 4,116,737 | 13.40 | 1.00 | 59.70 | 794.00 | N/A | N/A | 1,950 |
| 22 | Well emissions | al033 | 0.10 | 237,293 | 4,116,737 | 5.00 | 0.20 | 5.00 | 500.00 | N/A | N/A | 2,199 |
| 23 | Fuelco (500 hp total) | al034 | 0.21 | 238,761 | 4,117,114 | 9.14 | 0.21 | 31.00 | 880.00 | N/A | N/A | 2,199 |
| 24 | Hallwood 1 (2500 hp total) | al035 | 0.42 | 228,834 | 4,109,244 | 8.00 | 0.39 | 45.70 | 644.00 | N/A | N/A | 2,072 |
| 25 | Well emissions | al036 | 0.10 | 228,844 | 4,109,244 | 5.00 | 0.20 | 5.00 | 500.00 | N/A | N/A | 2,072 |
| 26 | Indep. ECBM 1 (5000 hp total) | al037 | 1.04 | 252,132 | 4,119,478 | 10.00 | 0.49 | 64.00 | 796.90 | N/A | N/A | 2,072 |
| 27 | Indep. ECBM 2 (5000 hp total) | al038 | 1.04 | 252,132 | 4,119,478 | 10.00 | 0.49 | 64.00 | 796.90 | N/A | N/A | 2,072 |
| 28 | Well emissions | al039 | 0.10 | 252,132 | 4,119,478 | 5.00 | 0.20 | 5.00 | 500.00 | N/A | N/A | 2,072 |
| 29 | Mark west (1500 hp total) | al040 | 0.63 | 251,010 | 4,105,000 | 10.00 | 0.43 | 61.00 | 713.00 | N/A | N/A | 2,072 |
| 30 | Indept Misc 1 (700 hp total) | al041 | 0.42 | 261,287 | 4,104,861 | 5.00 | 0.30 | 18.80 | 541.00 | N/A | N/A | 2,238 |
| 31 | Red Cedar / Bondad 1 (3000 hp tot) | al042 | 0.63 | 243,984 | 4,108,081 | 10.00 | 0.43 | 61.00 | 713.00 | N/A | N/A | 2,102 |
| 32 | Red Cedar / Bondad 2 (3000 hp tot) | al043 | 0.63 | 243,994 | 4,108,081 | 10.00 | 0.43 | 61.00 | 713.00 | N/A | N/A | 1,889 |
| 33 | Well emissions | al044 | 0.10 | 243,974 | 4,108,081 | 5.00 | 0.20 | 5.00 | 500.00 | N/A | N/A | 1,889 |
| 34 | Amoco Henderson A #1 1 (913 hp tot) | al045 | 0.15 | 236,746 | 4,099,203 | 5.00 | 0.30 | 18.80 | 541.00 | N/A | N/A | 1,889 |
| 35 | Amoco Henderson A #1 1 (913 hp tot) | al046 | 0.15 | 236,746 | 4,099,203 | 5.00 | 0.30 | 18.80 | 541.00 | N/A | N/A | 1,989 |

N/A – Not available

Table E-1. SUIT RFS Emission Source Modeling Input Values (continued)

| Source Count | Source Description | Unit ID | NOx Emission Rate (g/s) | UTM | | Stack Parameters | | | | Building | | Elevation (m) |
|--------------|--------------------------------------|---------|-------------------------|-------------|--------------|------------------|--------------|----------------|-----------|------------|-----------|---------------|
| | | | | Easting (m) | Northing (m) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 36 | Amoco Henderson A #1 1 (1200 hp tot) | al047 | 0.23 | 235,184 | 4,100,847 | 9.14 | 0.21 | 31.00 | 880.00 | N/A | N/A | 1,989 |
| 37 | Amoco Henderson A #1 1 (1200 hp tot) | al048 | 0.23 | 235,184 | 4,100,847 | 9.14 | 0.21 | 31.00 | 880.00 | N/A | N/A | 2,033 |
| 38 | Well emissions | al049 | 0.10 | 235,184 | 4,100,847 | 5.00 | 0.20 | 5.00 | 500.00 | N/A | N/A | 2,033 |
| 39 | Amoco 00 #1 1 (913 hp total) | al050 | 0.22 | 235,184 | 4,100,847 | 5.00 | 0.30 | 18.80 | 541.00 | N/A | N/A | 2,033 |
| 40 | Amoco 00 #1 1 (913 hp total) | al051 | 0.15 | 235,184 | 4,100,847 | 5.00 | 0.30 | 18.80 | 541.00 | N/A | N/A | 2,033 |
| 41 | Amoco H #2 1 (913 hp total) | al052 | 0.22 | 235,484 | 4,110,411 | 9.14 | 0.21 | 31.00 | 880.00 | N/A | N/A | 2,033 |
| 42 | Amoco H #2 1 (913 hp total) | al053 | 0.15 | 235,484 | 4,110,411 | 9.14 | 0.21 | 31.00 | 880.00 | N/A | N/A | 2,271 |
| 43 | Well emissions | al054 | 0.10 | 235,484 | 4,110,411 | 5.00 | 0.20 | 5.00 | 500.00 | N/A | N/A | 2,271 |
| 44 | Well emissions | al057 | 0.10 | 267,210 | 4,106,610 | 5.00 | 0.20 | 5.00 | 500.00 | N/A | N/A | 1,950 |
| 45 | SG (1500 hp total) | al058 | 0.63 | 266,432 | 4,104,330 | 10.00 | 0.43 | 61.00 | 713.00 | N/A | N/A | 1,950 |
| 46 | T Black Ridge (1342 hp total) | al059 | 0.56 | 236,743 | 4,108,241 | 8.00 | 0.39 | 45.70 | 685.00 | N/A | N/A | 1,950 |
| 47 | Well emissions | al060 | 0.10 | 236,733 | 4,108,241 | 5.00 | 0.20 | 5.00 | 500.00 | N/A | N/A | 2,127 |
| 48 | T Bondad (1342 hp total) | al061 | 0.56 | 243,262 | 4,108,407 | 8.00 | 0.39 | 45.70 | 685.00 | N/A | N/A | 2,127 |
| 49 | T Cabin 1 (5296 hp total) | al062 | 1.10 | 240,042 | 4,103,443 | 10.00 | 0.48 | 64.00 | 796.90 | N/A | N/A | 1,919 |
| 50 | T Cabin 2 (5296 hp total) | al063 | 1.10 | 240,052 | 4,103,443 | 10.00 | 0.48 | 64.00 | 796.90 | N/A | N/A | 1,950 |
| 51 | Well emissions | al064 | 0.10 | 240,042 | 4,103,443 | 5.00 | 0.20 | 5.00 | 500.00 | N/A | N/A | 1,950 |
| 52 | T Coyote Gulch 1 (4000 hp total) | al065 | 0.83 | 226,949 | 4,100,723 | 10.00 | 0.30 | 64.00 | 908.00 | N/A | N/A | 1,950 |
| 53 | T Coyote Gulch 2 (4000 hp total) | al066 | 0.83 | 226,959 | 4,100,723 | 10.00 | 0.30 | 64.00 | 908.00 | N/A | N/A | 1,858 |
| 54 | Well emissions | al067 | 0.10 | 226,939 | 4,100,723 | 5.00 | 0.20 | 5.00 | 500.00 | N/A | N/A | 1,858 |
| 55 | Tiffany (1000 hp total) | al068 | 0.42 | 273,500 | 4,103,900 | 7.62 | 0.30 | 37.70 | 636.00 | N/A | N/A | 1,858 |
| 56 | Well emissions | al069 | 0.10 | 273,500 | 4,103,900 | 5.00 | 0.20 | 5.00 | 500.00 | N/A | N/A | 1,960 |
| 57 | Trail Canyon (ark Loop) | al070 | 1.12 | 252,785 | 4,103,619 | 8.00 | 0.39 | 45.70 | 685.00 | N/A | N/A | 1,960 |
| 58 | Well emissions | al071 | 0.10 | 252,775 | 4,103,619 | 5.00 | 0.20 | 5.00 | 500.00 | N/A | N/A | 2,198 |
| 59 | Tribal ECBM 1 (5000 hp total) | al072 | 1.04 | 252,785 | 4,103,619 | 10.00 | 0.49 | 64.00 | 796.90 | N/A | N/A | 2,198 |
| 60 | Tribal ECBM 2 (5000 hp total) | al073 | 1.04 | 252,795 | 4,103,619 | 10.00 | 0.49 | 64.00 | 796.90 | N/A | N/A | 2,198 |
| 61 | Well emissions | al074 | 0.10 | 252,775 | 4,103,619 | 5.00 | 0.20 | 5.00 | 500.00 | N/A | N/A | 2,198 |
| 62 | Tribe Animas (1342 hp total) | al075 | 0.56 | 242,558 | 4,116,655 | 8.00 | 0.39 | 45.70 | 775.00 | N/A | N/A | 2,198 |
| 63 | Well emissions | al076 | 0.10 | 242,558 | 4,116,655 | 5.00 | 0.20 | 5.00 | 500.00 | N/A | N/A | 1,951 |
| 64 | Vastar #1 | al076 | 0.51 | 263,232 | 4,099,857 | 8.00 | 0.39 | 45.70 | 644.00 | N/A | N/A | 1,951 |
| 65 | Well emissions | al078 | 0.10 | 263,232 | 4,099,857 | 5.00 | 0.20 | 5.00 | 500.00 | N/A | N/A | 2,103 |
| 66 | Vastar #2 | al079 | 0.51 | 255,837 | 4,099,173 | 8.00 | 0.39 | 45.70 | 644.00 | N/A | N/A | 2,103 |
| 67 | Well emissions | al080 | 0.10 | 255,837 | 4,099,173 | 5.00 | 0.20 | 5.00 | 500.00 | N/A | N/A | 2,090 |
| 68 | Vastar 4 | al081 | 1.23 | 252,676 | 4,098,991 | 10.00 | 0.48 | 64.00 | 796.90 | N/A | N/A | 2,090 |
| 69 | Well emissions | al082 | 0.10 | 252,676 | 4,098,991 | 5.00 | 0.20 | 5.00 | 500.00 | N/A | N/A | 2,133 |
| 70 | Vastar 6B | al083 | 0.82 | 245,314 | 4,101,508 | 10.00 | 0.30 | 64.00 | 908.00 | N/A | N/A | 2,133 |

N/A – Not available

Table E-1. SUIT RFS Emission Source Modeling Input Values (continued)

| Source Count | Source Description | Unit ID | NOx Emission Rate (g/s) | UTM | | Stack Parameters | | | | Building | | Elevation (m) |
|--------------|--------------------------|---------|-------------------------|-------------|--------------|------------------|--------------|----------------|-----------|------------|-----------|---------------|
| | | | | Easting (m) | Northing (m) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 71 | Well emissions | al084 | 0.10 | 245,314 | 4,101,508 | 5.00 | 0.20 | 5.00 | 500.00 | N/A | N/A | 2,011 |
| 72 | Vastar 7b | al085 | 0.82 | 237,002 | 4,117,273 | 10.00 | 0.30 | 64.00 | 908.00 | N/A | N/A | 2,011 |
| 73 | Well emissions | al086 | 0.10 | 237,002 | 4,117,273 | 5.00 | 0.20 | 5.00 | 500.00 | N/A | N/A | 2,144 |
| 74 | Vastar 8 | al087 | 0.82 | 238,984 | 4,106,892 | 10.00 | 0.30 | 64.00 | 908.00 | N/A | N/A | 2,144 |
| 75 | Well emissions | al088 | 0.10 | 238,984 | 4,106,892 | 5.00 | 0.20 | 5.00 | 500.00 | N/A | N/A | 2,048 |
| 76 | Vastar ECBM 5000 | al089 | 2.08 | 249,759 | 4,098,862 | 13.10 | 0.65 | 55.00 | 908.00 | N/A | N/A | 2,048 |
| 77 | Well emissions | al090 | 0.10 | 249,759 | 4,098,862 | 5.00 | 0.20 | 5.00 | 500.00 | N/A | N/A | 2,133 |
| 78 | Vastar ECBM 5000 | al091 | 2.08 | 249,769 | 4,098,862 | 13.10 | 0.65 | 55.00 | 908.00 | N/A | N/A | 2,133 |
| 79 | Well emissions | al092 | 0.10 | 249,769 | 4,098,862 | 5.00 | 0.20 | 5.00 | 500.00 | N/A | N/A | 2,133 |
| 80 | Vastar ECBM 5000 | al093 | 2.08 | 249,779 | 4,098,862 | 13.10 | 0.65 | 55.00 | 908.00 | N/A | N/A | 2,133 |
| 81 | Well emissions | al094 | 0.10 | 249,779 | 4,098,862 | 5.00 | 0.20 | 5.00 | 500.00 | N/A | N/A | 2,132 |
| 82 | Vastar ECBM 5000 | al095 | 2.08 | 249,789 | 4,098,862 | 13.10 | 0.65 | 55.00 | 908.00 | N/A | N/A | 2,132 |
| 83 | Well emissions | al096 | 0.10 | 249,789 | 4,098,862 | 5.00 | 0.20 | 5.00 | 500.00 | N/A | N/A | 2,132 |
| 84 | Amoco/Vastar 1 (2000 hp) | al097 | 0.83 | 240,800 | 4,105,800 | 10.00 | 0.30 | 64.00 | 908.00 | N/A | N/A | 2,132 |
| 85 | dc3000 | ?????? | 1.25 | 252,900 | 4,102,670 | 7.00 | 0.50 | 16.90 | 589.00 | N/A | N/A | 2,273 |

N/A – Not available

Appendix F – Farmington RMP Emission Inventory

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Table F-1. Summary of Emissions

| | Separators | Wellhead Engines | Compressors |
|----------------------------|-------------------|-------------------------|--------------------|
| Number of Emission Sources | 13,275 | 4,971 | 144 |
| NOx Emissions (t/yr) | 1,425 | 31,639 | 5,210 |

Table F-2. Determination of Potential Emission Source Locations

Number of existing wells per Township

| Township | Range | | | | | | | | | | | | |
|----------|-------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| | 14W | 13W | 12W | 11W | 10W | 09W | 08W | 07W | 06W | 05W | 04W | 03W | 02W |
| 32N | 2 | 6 | 5 | 4 | 4 | 6 | 7 | 6 | 4 | 3 | 4 | 0 | 0 |
| 31N | 2 | 7 | 5 | 5 | 3 | 3 | 2 | 6 | 3 | 3 | 2 | 2 | 0 |
| 30N | 3 | 6 | 7 | 6 | 5 | 4 | 3 | 2 | 3 | 5 | 2 | 2 | 2 |
| 29N | 2 | 7 | 5 | 4 | 6 | 6 | 5 | 5 | 5 | 7 | 2 | 2 | 0 |
| 28N | 0 | 6 | 6 | 5 | 5 | 7 | 5 | 7 | 7 | 5 | 3 | 2 | 2 |
| 27N | 0 | 2 | 7 | 6 | 6 | 6 | 6 | 6 | 6 | 5 | 4 | 3 | 2 |
| 26N | 0 | 2 | 3 | 5 | 7 | 7 | 4 | 3 | 3 | 5 | 4 | 4 | 2 |
| 25N | 0 | 0 | 3 | 4 | 3 | 3 | 2 | 2 | 3 | 2 | 2 | 3 | 2 |
| 24N | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 2 | 4 | 2 | 2 | 0 | 2 |

Distribution of existing wells per Township (percent)

| Township | Range | | | | | | | | | | | | |
|----------|-------|------|------|------|------|------|------|------|------|------|------|------|------|
| | 14W | 13W | 12W | 11W | 10W | 09W | 08W | 07W | 06W | 05W | 04W | 03W | 02W |
| 32N | 0.49 | 1.46 | 1.22 | 0.97 | 0.97 | 1.46 | 1.70 | 1.46 | 0.97 | 0.73 | 0.97 | 0.00 | 0.00 |
| 31N | 0.49 | 1.70 | 1.22 | 1.22 | 0.73 | 0.73 | 0.49 | 1.46 | 0.73 | 0.73 | 0.49 | 0.49 | 0.00 |
| 30N | 0.73 | 1.46 | 1.70 | 1.46 | 1.22 | 0.97 | 0.73 | 0.49 | 0.73 | 1.22 | 0.49 | 0.49 | 0.49 |
| 29N | 0.49 | 1.70 | 1.22 | 0.97 | 1.46 | 1.46 | 0.73 | 1.22 | 1.22 | 1.70 | 0.49 | 0.49 | 0.00 |
| 28N | 0.00 | 1.46 | 1.46 | 1.22 | 1.22 | 1.70 | 1.22 | 1.70 | 1.70 | 1.22 | 0.73 | 0.49 | 0.49 |
| 27N | 0.00 | 0.49 | 1.70 | 1.46 | 1.46 | 1.46 | 1.46 | 1.46 | 1.46 | 1.22 | 0.97 | 0.73 | 0.49 |
| 26N | 0.00 | 0.49 | 0.73 | 1.22 | 1.70 | 1.70 | 0.97 | 0.73 | 0.73 | 1.22 | 0.97 | 0.97 | 0.49 |
| 25N | 0.00 | 0.00 | 0.73 | 0.97 | 0.73 | 0.73 | 0.49 | 0.49 | 0.73 | 0.49 | 0.49 | 0.73 | 0.49 |
| 24N | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.49 | 0.49 | 0.97 | 0.49 | 0.49 | 0.00 | 0.49 |

Table F-2. Determination of Potential Emission Source Locations (continued)

Assumed number of wells per Township

| Township | Range | | | | | | | | | | | | |
|----------|-------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| | 14W | 13W | 12W | 11W | 10W | 09W | 08W | 07W | 06W | 05W | 04W | 03W | 02W |
| 32N | 0.9 | 2.8 | 2.3 | 1.8 | 1.8 | 2.8 | 3.2 | 2.8 | 1.8 | 1.4 | 1.8 | 0.0 | 0.0 |
| 31N | 0.9 | 3.2 | 2.3 | 2.3 | 1.4 | 1.4 | 0.9 | 2.8 | 1.4 | 1.4 | 0.9 | 0.9 | 0.0 |
| 30N | 1.4 | 2.8 | 3.2 | 2.8 | 2.3 | 1.8 | 1.4 | 0.9 | 1.4 | 2.3 | 0.9 | 0.9 | 0.9 |
| 29N | 0.9 | 3.2 | 2.3 | 1.8 | 2.8 | 2.8 | 2.3 | 2.3 | 2.3 | 3.2 | 0.9 | 0.9 | 0.0 |
| 28N | 0.0 | 2.8 | 2.8 | 2.3 | 2.3 | 3.2 | 2.3 | 3.2 | 3.2 | 2.3 | 1.4 | 0.9 | 0.9 |
| 27N | 0.0 | 0.9 | 3.2 | 2.8 | 2.8 | 2.8 | 2.8 | 2.8 | 2.8 | 2.3 | 1.8 | 1.4 | 0.9 |
| 26N | 0.0 | 0.9 | 1.4 | 2.3 | 3.2 | 3.2 | 1.8 | 1.4 | 1.4 | 2.3 | 1.8 | 1.8 | 0.9 |
| 25N | 0.0 | 0.0 | 1.4 | 1.8 | 1.4 | 1.4 | 0.9 | 0.9 | 1.4 | 0.9 | 0.9 | 1.4 | 0.9 |
| 24N | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.9 | 0.9 | 1.8 | 0.9 | 0.9 | 0.0 | 0.9 |

Note: This represents combining 35 wells into a single modeling source; each value indicates the proposed number of wells per Township

Assumed distribution of central compressor stations per Township

| Township | Range | | | | | | | | | | | | |
|----------|-------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| | 14W | 13W | 12W | 11W | 10W | 09W | 08W | 07W | 06W | 05W | 04W | 03W | 02W |
| 32N | 0 | 1 | 1 | 1 | 0 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 |
| 31N | 0 | 1 | 1 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 |
| 30N | 0 | 1 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 |
| 29N | 0 | 1 | 0 | 0 | 1 | 1 | 1 | 1 | 1 | 1 | 0 | 0 | 0 |
| 28N | 0 | 1 | 1 | 1 | 1 | 1 | 0 | 1 | 1 | 0 | 0 | 0 | 0 |
| 27N | 0 | 0 | 1 | 0 | 1 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 |
| 26N | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 25N | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 24N | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

Table F-3. Existing Wellhead Engine Type, Number, Power and Emission Factors

| Engine Type | Number | Average Horsepower (hp) | Average Emission Factor (g/hp-hr) | Distribution of Engines (percent) | Weighted Horsepower (hp) | Weighted Emission Factor (g/hp-hr) |
|-----------------|--------|-------------------------|-----------------------------------|-----------------------------------|--------------------------|------------------------------------|
| Rich Burn-Small | 1,409 | 59.4 | 12.61 | 51 | 30.32 | 6.44 |
| Rich Burn-Med. | 253 | 181.8 | 10.58 | 9 | 16.67 | 0.97 |
| Lean Burn-Small | 7 | 51 | 4.20 | 0 | 0.13 | 0.01 |
| Lean Burn-Med. | 181 | 318.9 | 3.06 | 7 | 20.91 | 0.20 |
| Pump Jacks | 910 | 16.4 | 6.76 | 33 | 5.41 | 2.23 |
| Totals | 2,760 | | | 100 | 73.44 | 9.85 |

Table F-4 Separator Emission Calculations ⁽¹⁾

| | Individual NOx (lb/MMscf) ⁽²⁾ | Individual NOx (lb/hr) ⁽³⁾ | Individual NOx (t/yr) ⁽³⁾ | Number of Wells | Number of Separators ⁽⁴⁾ | Total NOx (t/yr) ⁽²⁾ |
|------------|------------------------------------------|---------------------------------------|--------------------------------------|-----------------|-------------------------------------|---------------------------------|
| Separators | 100 | 0.025 | 0.107 | 13,275 | 13,275 | 1,425 |

⁽¹⁾ Assumes separators operate year-around (8760 hr/yr) at 100 percent capacity load

⁽²⁾ EPA (AP-42 Section 1.4 emission factor)

⁽³⁾ Based on average natural gas heat capacity of 1,000 Btu/scf, and separator flame rate of 0.25 MMBtu/hr

⁽⁴⁾ Assumes every well has a separator

Table F-5 Small Wellhead Engine Emission Calculations ⁽¹⁾

| Small Wellhead Engines | Individual NOx (g/hp-hr) ⁽²⁾ | Individual NOx (t/yr) ⁽²⁾ | Number of Wells | Number of Wellhead Engines ⁽³⁾ | Total NOx (t/yr) ⁽²⁾ |
|-------------------------------|-----------------------------------------|--------------------------------------|-----------------|-------------------------------------------|---------------------------------|
| Existing at 100 percent load | 9.62 | 6.36 | 9,942 | 4,971 | 31,639 |
| Existing at 54 percent load | 9.62 | 3.44 | 9,942 | 4,971 | 17,085 |
| Lean-burn at 100 percent load | 2.0 | 1.3 | 9,942 | 4,971 | 6,578 |
| Lean-burn at 54 percent load | 2.0 | 0.71 | 9,942 | 4,971 | 3,552 |

⁽¹⁾ Assumes 68.6 hp wellhead engines operate year-around (8760 hr/yr)

⁽²⁾ Based on average natural gas heat capacity of 1,000 Btu/scf, and wellhead engine rate of 10,000 Btu/hp-hr

⁽³⁾ Assumes one wellhead engine for every two wells

Table F-6 Central Compressor Station Emission Calculations

| Central Compressor Station | Individual NOx (g/sec) | Individual NOx (t/yr) | Number of Units ⁽³⁾ | Total NOx (g/sec) | Total NOx (t/yr) |
|----------------------------|------------------------|-----------------------|--------------------------------|-------------------|------------------|
| Compressor ⁽¹⁾ | 4.171 | 145 | 36 | 149 | 5,210 |
| Dehydrator ⁽²⁾ | 0.001 | 0.029 | 36 | 0.03 | 1.04 |
| Combined | 4.172 | 145 | 36 | 150 | 5,211 |

⁽¹⁾ Assumes 10,000 hp Central Compressor Station (four 2,500 hp engines) operate year-around (8760 hr/yr) at 100 percent load and 1.5 g/hp-hr NOx emission rate

⁽²⁾ Based on average natural gas heat capacity of 1,000 Btu/scf, and dehydrator flame rate of 2.43 MMBtu/hr

⁽³⁾ Assumes every compressor station has a dehydrator

Table F-7 Combined Emissions and Modeling Assumptions

| Source Type | Total NOx (t/yr) | Number of Modeled Sources | Each Modeled Source NOx (t/yr) |
|----------------------------------------------|---------------------|---------------------------------|--------------------------------------|
| Separators | 1,425 | 190 | 7.5 |
| Existing Wellhead Engine at 54 percent load | 17,085 | 190 | 90.0 |
| Compressor | 5,210 | 36 | 145 |
| Dehydrator | 1.04 | 36 | 0.029 |
| Combined | 23,721 | 226 | 105 |
| | | | |
| Separators | 1,425 | 190 | 7.5 |
| Lean-burn Wellhead Engine at 54 percent load | 3,552 | 190 | 18.7 |
| Compressor | 5,210 | 36 | 145 |
| Dehydrator | 1.04 | 36 | 0.029 |
| Combined | 10,188 | 226 | 45 |

Table F-8 Far Field Modeling Input Values (Assuming 9.6 g/hp-hr NOx Wellhead Engines)

| Source Count | Source Type | Location/ID | NOx Emission Rate (g/s) | UTM | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|----------------|-------------|-------------------------|-------------|--------------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | | Easting (m) | Northing (m) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 1 | Well emissions | 14W32NA | 2.8066 | 203235 | 4096434 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6209 |
| 2 | Well emissions | 14W31NA | 2.8066 | 203173 | 4088127 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5796 |
| 3 | Well emissions | 14W29NA | 2.8066 | 203147 | 4068123 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5415 |
| 4 | Well emissions | 13W32NA | 2.8066 | 215344 | 4095670 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5973 |
| 5 | Well emissions | 13W32NB | 2.8066 | 214344 | 4095670 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6009 |
| 6 | Well emissions | 13W32NC | 2.8066 | 216344 | 4095670 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5989 |
| 7 | Well emissions | 13W31NA | 2.8066 | 214525 | 4087566 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5796 |
| 8 | Well emissions | 13W31NB | 2.8066 | 213525 | 4087566 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5796 |
| 9 | Well emissions | 13W31NC | 2.8066 | 215525 | 4087566 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5763 |
| 10 | Well emissions | 13W31ND | 2.8066 | 214525 | 4088566 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5796 |
| 11 | Well emissions | 13W30NA | 2.8066 | 214071 | 4077901 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5596 |
| 12 | Well emissions | 13W30NB | 2.8066 | 213071 | 4077901 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5494 |
| 13 | Well emissions | 13W30NC | 2.8066 | 215071 | 4077901 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5697 |
| 14 | Well emissions | 13W29NA | 2.8066 | 213627 | 4068389 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5241 |
| 15 | Well emissions | 13W29NB | 2.8066 | 212627 | 4068389 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5238 |
| 16 | Well emissions | 13W29NC | 2.8066 | 214627 | 4068389 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5278 |
| 17 | Well emissions | 13W29ND | 2.8066 | 213627 | 4069389 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5337 |
| 18 | Well emissions | 13W28NA | 2.8066 | 213090 | 4059806 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6016 |
| 19 | Well emissions | 13W28NB | 2.8066 | 212090 | 4059806 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6012 |
| 20 | Well emissions | 13W28NC | 2.8066 | 214090 | 4059806 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6012 |
| 21 | Well emissions | 13W27NA | 2.8066 | 212581 | 4051683 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6042 |
| 22 | Well emissions | 13W26NA | 2.8066 | 212073 | 4043560 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6291 |
| 23 | Well emissions | 12W32NA | 2.8066 | 224108 | 4095578 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6061 |
| 24 | Well emissions | 12W32NB | 2.8066 | 223108 | 4095578 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5996 |
| 25 | Well emissions | 12W31NA | 2.8066 | 223567 | 4086997 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6143 |
| 26 | Well emissions | 12W31NB | 2.8066 | 222567 | 4086997 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6173 |
| 27 | Well emissions | 12W31NC | 2.8066 | 224567 | 4086997 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6291 |
| 28 | Well emissions | 12W30NA | 2.8066 | 223122 | 4077486 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5753 |
| 29 | Well emissions | 12W30NB | 2.8066 | 222122 | 4077486 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5799 |
| 30 | Well emissions | 12W30NC | 2.8066 | 224122 | 4077486 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5717 |
| 31 | Well emissions | 12W29NA | 2.8066 | 222957 | 4067496 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5596 |
| 32 | Well emissions | 12W29NB | 2.8066 | 221957 | 4067496 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5596 |
| 33 | Well emissions | 12W29NC | 2.8066 | 223957 | 4067496 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5596 |
| 34 | Well emissions | 12W28NA | 2.8066 | 222448 | 4059374 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5720 |
| 35 | Well emissions | 12W28NB | 2.8066 | 221448 | 4059374 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5648 |

Table F-8 Far Field Modeling Input Values (Assuming 9.6 g/hp-hr NOx Wellhead Engines)(continued)

| Source Count | Source Type | Location/ID | NOx Emission Rate (g/s) | UTM | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|----------------|-------------|-------------------------|-------------|--------------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | | Easting (m) | Northing (m) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 36 | Well emissions | 12W28NC | 2.8066 | 223448 | 4059374 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5802 |
| 37 | Well emissions | 12W27NA | 2.8066 | 221949 | 4051405 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5796 |
| 38 | Well emissions | 12W27NB | 2.8066 | 220949 | 4051405 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5796 |
| 39 | Well emissions | 12W27NC | 2.8066 | 222949 | 4051405 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5930 |
| 40 | Well emissions | 12W27ND | 2.8066 | 221949 | 4052405 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5812 |
| 41 | Well emissions | 12W26NA | 2.8066 | 221451 | 4043437 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6101 |
| 42 | Well emissions | 12W25NA | 2.8066 | 220952 | 4035468 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6196 |
| 43 | Well emissions | 11W32NA | 2.8066 | 234283 | 4097339 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6580 |
| 44 | Well emissions | 11W32NB | 2.8066 | 233283 | 4097339 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6813 |
| 45 | Well emissions | 11W32NC | 2.8066 | 234283 | 4098339 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6580 |
| 46 | Well emissions | 11W31NA | 2.8066 | 234105 | 4086728 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5960 |
| 47 | Well emissions | 11W31NB | 2.8066 | 233105 | 4086728 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5996 |
| 48 | Well emissions | 11W30NA | 2.8066 | 233971 | 4077162 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5897 |
| 49 | Well emissions | 11W30NB | 2.8066 | 232971 | 4077162 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5796 |
| 50 | Well emissions | 11W30NC | 2.8066 | 234971 | 4077162 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5996 |
| 51 | Well emissions | 11W29NA | 2.8066 | 233815 | 4067574 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5524 |
| 52 | Well emissions | 11W29NB | 2.8066 | 232815 | 4067574 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5546 |
| 53 | Well emissions | 11W28NA | 2.8066 | 233660 | 4059187 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5648 |
| 54 | Well emissions | 11W28NB | 2.8066 | 232660 | 4059187 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5796 |
| 55 | Well emissions | 11W27NA | 2.8066 | 233526 | 4050867 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6229 |
| 56 | Well emissions | 11W27NB | 2.8066 | 232526 | 4050867 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6298 |
| 57 | Well emissions | 11W27NC | 2.8066 | 234526 | 4050867 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6048 |
| 58 | Well emissions | 11W26NA | 2.8066 | 233393 | 4042547 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6396 |
| 59 | Well emissions | 11W26NB | 2.8066 | 232393 | 4042547 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6376 |
| 60 | Well emissions | 11W25NA | 2.8066 | 233259 | 4034227 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6360 |
| 61 | Well emissions | 11W25NB | 2.8066 | 232259 | 4034227 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6317 |
| 62 | Well emissions | 10W32NA | 2.8066 | 243226 | 4097050 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6826 |
| 63 | Well emissions | 10W32NB | 2.8066 | 242226 | 4097050 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6826 |
| 64 | Well emissions | 10W31NA | 2.8066 | 242692 | 4086528 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6170 |
| 65 | Well emissions | 10W30NA | 2.8066 | 242380 | 4076917 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6403 |
| 66 | Well emissions | 10W30NB | 2.8066 | 241380 | 4076917 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6596 |
| 67 | Well emissions | 10W30NC | 2.8066 | 243380 | 4076917 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6396 |
| 68 | Well emissions | 10W29NA | 2.8066 | 241980 | 4067374 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5796 |
| 69 | Well emissions | 10W29NB | 2.8066 | 240980 | 4067374 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5602 |
| 70 | Well emissions | 10W29NC | 2.8066 | 242980 | 4067374 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5796 |

Table F-8 Far Field Modeling Input Values (Assuming 9.6 g/hp-hr NOx Wellhead Engines)(continued)

| Source Count | Source Type | Location/ID | NOx Emission Rate (g/s) | UTM | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|----------------|-------------|-------------------------|-------------|--------------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | | Easting (m) | Northing (m) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 71 | Well emissions | 10W28NA | 2.8066 | 241646 | 4058942 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6032 |
| 72 | Well emissions | 10W28NB | 2.8066 | 240646 | 4058942 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6170 |
| 73 | Well emissions | 10W27NA | 2.8066 | 241335 | 4050400 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6196 |
| 74 | Well emissions | 10W27NB | 2.8066 | 240335 | 4050400 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6193 |
| 75 | Well emissions | 10W27NC | 2.8066 | 242335 | 4050400 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6396 |
| 76 | Well emissions | 10W27ND | 2.8066 | 241335 | 4051400 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6396 |
| 77 | Well emissions | 10W26NA | 2.8066 | 241023 | 4041857 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6668 |
| 78 | Well emissions | 10W26NB | 2.8066 | 240023 | 4041857 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6632 |
| 79 | Well emissions | 10W26NC | 2.8066 | 242023 | 4041857 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6639 |
| 80 | Well emissions | 10W25NA | 2.8066 | 240712 | 4033315 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6596 |
| 81 | Well emissions | 10W25NB | 2.8066 | 239712 | 4033315 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6596 |
| 82 | Well emissions | 9W32NA | 2.8066 | 253036 | 4096716 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 7000 |
| 83 | Well emissions | 9W32NB | 2.8066 | 252036 | 4096716 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6983 |
| 84 | Well emissions | 9W32NC | 2.8066 | 254036 | 4096716 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 7019 |
| 85 | Well emissions | 9W31NA | 2.8066 | 252814 | 4086283 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6396 |
| 86 | Well emissions | 9W30NA | 2.8066 | 252613 | 4076584 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6091 |
| 87 | Well emissions | 9W30NB | 2.8066 | 251613 | 4076584 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6019 |
| 88 | Well emissions | 9W29NA | 2.8066 | 252369 | 4067062 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5897 |
| 89 | Well emissions | 9W29NB | 2.8066 | 251369 | 4067062 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5770 |
| 90 | Well emissions | 9W29NC | 2.8066 | 253369 | 4067062 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6019 |
| 91 | Well emissions | 9W28NA | 2.8066 | 252169 | 4058564 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6799 |
| 92 | Well emissions | 9W28NB | 2.8066 | 251169 | 4058564 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6996 |
| 93 | Well emissions | 9W28NC | 2.8066 | 253169 | 4058564 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6796 |
| 94 | Well emissions | 9W27NA | 2.8066 | 252013 | 4049799 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6202 |
| 95 | Well emissions | 9W27NB | 2.8066 | 251013 | 4049799 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6229 |
| 96 | Well emissions | 9W27NC | 2.8066 | 253013 | 4049799 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6196 |
| 97 | Well emissions | 9W26NA | 2.8066 | 251857 | 4041034 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6389 |
| 98 | Well emissions | 9W26NB | 2.8066 | 250857 | 4041034 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6396 |
| 99 | Well emissions | 9W26NC | 2.8066 | 252857 | 4041034 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6383 |
| 100 | Well emissions | 9W26ND | 2.8066 | 251857 | 4042034 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6330 |
| 101 | Well emissions | 9W25NA | 2.8066 | 251701 | 4032269 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6596 |
| 102 | Well emissions | 8W32nA | 2.8066 | 262246 | 4096383 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6796 |
| 103 | Well emissions | 8W32nB | 2.8066 | 261246 | 4096383 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6796 |
| 104 | Well emissions | 8W32nC | 2.8066 | 263246 | 4096383 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6813 |
| 105 | Well emissions | 8W31nA | 2.8066 | 261957 | 4086060 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6426 |

Table F-8 Far Field Modeling Input Values (Assuming 9.6 g/hp-hr NOx Wellhead Engines)(continued)

| Source Count | Source Type | Location/ID | NOx Emission Rate (g/s) | UTM | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|----------------|-------------|-------------------------|-------------|--------------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | | Easting (m) | Northing (m) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 106 | Well emissions | 8W30nA | 2.8066 | 261734 | 4076339 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6396 |
| 107 | Well emissions | 8W29nA | 2.8066 | 261490 | 4066795 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6596 |
| 108 | Well emissions | 8W29nB | 2.8066 | 260490 | 4066795 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6596 |
| 109 | Well emissions | 8W28nA | 2.8066 | 261267 | 4058275 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5996 |
| 110 | Well emissions | 8W28nB | 2.8066 | 260267 | 4058275 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5973 |
| 111 | Well emissions | 8W27nA | 2.8066 | 261023 | 4049288 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6052 |
| 112 | Well emissions | 8W27nB | 2.8066 | 260023 | 4049288 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6596 |
| 113 | Well emissions | 8W27nC | 2.8066 | 262023 | 4049288 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6124 |
| 114 | Well emissions | 8W26nA | 2.8066 | 260778 | 4040300 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 7036 |
| 115 | Well emissions | 8W26nB | 2.8066 | 259778 | 4040300 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6888 |
| 116 | Well emissions | 8W26nC | 2.8066 | 261778 | 4040300 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6806 |
| 117 | Well emissions | 8W25nA | 2.8066 | 260533 | 4031313 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6612 |
| 118 | Well emissions | 7W32nA | 2.8066 | 271968 | 4096027 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6796 |
| 119 | Well emissions | 7W32nB | 2.8066 | 270968 | 4096027 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6396 |
| 120 | Well emissions | 7W32nC | 2.8066 | 272968 | 4096027 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6796 |
| 121 | Well emissions | 7W31nA | 2.8066 | 271678 | 4085794 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6419 |
| 122 | Well emissions | 7W31nB | 2.8066 | 270678 | 4085794 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6517 |
| 123 | Well emissions | 7W31nC | 2.8066 | 272678 | 4085794 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6399 |
| 124 | Well emissions | 7W30nA | 2.8066 | 271478 | 4076161 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6576 |
| 125 | Well emissions | 7W29nA | 2.8066 | 271211 | 4066506 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6596 |
| 126 | Well emissions | 7W29nB | 2.8066 | 270211 | 4066506 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6596 |
| 127 | Well emissions | 7W28nA | 2.8066 | 271033 | 4057986 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6796 |
| 128 | Well emissions | 7W28nB | 2.8066 | 270033 | 4057986 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6396 |
| 129 | Well emissions | 7W28nC | 2.8066 | 272033 | 4057986 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6678 |
| 130 | Well emissions | 7W27nA | 2.8066 | 270789 | 4048776 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6603 |
| 131 | Well emissions | 7W27nB | 2.8066 | 269789 | 4048776 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6596 |
| 132 | Well emissions | 7W27nC | 2.8066 | 271789 | 4048776 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6662 |
| 133 | Well emissions | 7W26nA | 2.8066 | 270544 | 4039566 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6796 |
| 134 | Well emissions | 7W25nA | 2.8066 | 270299 | 4030356 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6776 |
| 135 | Well emissions | 7W24nA | 2.8066 | 270055 | 4021146 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 7000 |
| 136 | Well emissions | 6W32nA | 2.8066 | 281436 | 4095756 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6016 |
| 137 | Well emissions | 6W32nB | 2.8066 | 280436 | 4095756 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6170 |
| 138 | Well emissions | 6W31nA | 2.8066 | 280978 | 4085519 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6196 |
| 139 | Well emissions | 6W30nA | 2.8066 | 280629 | 4075905 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6596 |
| 140 | Well emissions | 6W29nA | 2.8066 | 280244 | 4066328 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6458 |

Table F-8 Far Field Modeling Input Values (Assuming 9.6 g/hp-hr NOx Wellhead Engines)(continued)

| Source Count | Source Type | Location/ID | NOx Emission Rate (g/s) | UTM | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|----------------|-------------|-------------------------|-------------|--------------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | | Easting (m) | Northing (m) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 141 | Well emissions | 6W29nB | 2.8066 | 279244 | 4066328 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6485 |
| 142 | Well emissions | 6W28nA | 2.8066 | 279914 | 4057650 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6530 |
| 143 | Well emissions | 6W28nB | 2.8066 | 278914 | 4057650 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6396 |
| 144 | Well emissions | 6W28nC | 2.8066 | 280914 | 4057650 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6596 |
| 145 | Well emissions | 6W27nA | 2.8066 | 279602 | 4048184 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6596 |
| 146 | Well emissions | 6W27nB | 2.8066 | 278602 | 4048184 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6596 |
| 147 | Well emissions | 6W27nC | 2.8066 | 280602 | 4048184 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6560 |
| 148 | Well emissions | 6W26nA | 2.8066 | 279290 | 4038717 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6642 |
| 149 | Well emissions | 6W25nA | 2.8066 | 278978 | 4029250 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6596 |
| 150 | Well emissions | 6W24nA | 2.8066 | 279978 | 4029250 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6596 |
| 151 | Well emissions | 6W24nB | 2.8066 | 280978 | 4029250 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6596 |
| 152 | Well emissions | 5W32nA | 2.8066 | 290521 | 4095426 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6796 |
| 153 | Well emissions | 5W31nA | 2.8066 | 290187 | 4085260 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6416 |
| 154 | Well emissions | 5W30nA | 2.8066 | 290187 | 4086260 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6652 |
| 155 | Well emissions | 5W30nB | 2.8066 | 289187 | 4086260 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6639 |
| 156 | Well emissions | 5W29nA | 2.8066 | 289498 | 4066039 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6698 |
| 157 | Well emissions | 5W29nB | 2.8066 | 288498 | 4066039 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6681 |
| 158 | Well emissions | 5W29nC | 2.8066 | 290498 | 4066039 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6796 |
| 159 | Well emissions | 5W28nA | 2.8066 | 289253 | 4057341 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6796 |
| 160 | Well emissions | 5W28nB | 2.8066 | 288253 | 4057341 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6665 |
| 161 | Well emissions | 5W27nA | 2.8066 | 288897 | 4047819 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6580 |
| 162 | Well emissions | 5W27nB | 2.8066 | 287897 | 4047819 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6560 |
| 163 | Well emissions | 5W26nA | 2.8066 | 288541 | 4038298 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6596 |
| 164 | Well emissions | 5W26nB | 2.8066 | 287541 | 4038298 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6596 |
| 165 | Well emissions | 5W25nA | 2.8066 | 288185 | 4028777 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6691 |
| 166 | Well emissions | 4W32nA | 2.8066 | 298997 | 4095137 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6921 |
| 167 | Well emissions | 4W32nB | 2.8066 | 297997 | 4095137 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 7200 |
| 168 | Well emissions | 4W31nA | 2.8066 | 298752 | 4085082 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6996 |
| 169 | Well emissions | 4W29nA | 2.8066 | 298329 | 4065794 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 7298 |
| 170 | Well emissions | 4W28nA | 2.8066 | 298107 | 4057074 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 7396 |
| 171 | Well emissions | 4W27nA | 2.8066 | 297929 | 4047330 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6996 |
| 172 | Well emissions | 4W27nB | 2.8066 | 296929 | 4047330 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 7029 |
| 173 | Well emissions | 4W26nA | 2.8066 | 297751 | 4037586 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 7072 |
| 174 | Well emissions | 4W26nB | 2.8066 | 296751 | 4037586 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 7196 |
| 175 | Well emissions | 4W25nA | 2.8066 | 297573 | 4027842 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 7196 |

Table F-8 Far Field Modeling Input Values (Assuming 9.6 g/hp-hr NOx Wellhead Engines)(continued)

| Source Count | Source Type | Location/ID | NOx Emission Rate (g/s) | UTM | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|--------------------|-------------|-------------------------|-------------|--------------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | | Easting (m) | Northing (m) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 176 | Well emissions | 4W24nA | 2.8066 | 298573 | 4027842 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 7196 |
| 177 | Well emissions | 3W31nA | 2.8066 | 308273 | 4084859 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 7396 |
| 178 | Well emissions | 3W30nA | 2.8066 | 308229 | 4075182 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 7596 |
| 179 | Well emissions | 3W29nA | 2.8066 | 308407 | 4065616 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6996 |
| 180 | Well emissions | 3W28nA | 2.8066 | 308451 | 4056651 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 7098 |
| 181 | Well emissions | 3W27nA | 2.8066 | 308518 | 4046774 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 7196 |
| 182 | Well emissions | 3W26nA | 2.8066 | 308585 | 4036896 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 7390 |
| 183 | Well emissions | 3W26nB | 2.8066 | 307585 | 4036896 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 7347 |
| 184 | Well emissions | 3W25nA | 2.8066 | 308652 | 4027019 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 7344 |
| 185 | Well emissions | 3W25nA | 2.8066 | 307652 | 4027019 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 7203 |
| 186 | Well emissions | 2W30nA | 2.8066 | 317194 | 4075026 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 7797 |
| 187 | Well emissions | 2W28nA | 2.8066 | 317817 | 4056317 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 7295 |
| 188 | Well emissions | 2W27nA | 2.8066 | 317995 | 4046195 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 7396 |
| 189 | Well emissions | 2W26nA | 2.8066 | 318173 | 4036073 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 7797 |
| 190 | Well emissions | 2W24nA | 2.8066 | 319173 | 4036073 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 7308 |
| 191 | Central Compressor | 13W32NA | 4.1721 | 215344 | 4095670 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 5973 |
| 192 | Central Compressor | 13W31NA | 4.1721 | 214525 | 4087566 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 5796 |
| 193 | Central Compressor | 13W30NA | 4.1721 | 214071 | 4077901 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 5596 |
| 194 | Central Compressor | 13W29NA | 4.1721 | 213627 | 4068389 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 5241 |
| 195 | Central Compressor | 13W28NA | 4.1721 | 213090 | 4059806 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 6016 |
| 196 | Central Compressor | 12W32NA | 4.1721 | 224108 | 4095578 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 6061 |
| 197 | Central Compressor | 12W31NA | 4.1721 | 223567 | 4086997 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 6143 |
| 198 | Central Compressor | 12W30NA | 4.1721 | 223122 | 4077486 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 5753 |
| 199 | Central Compressor | 12W28NA | 4.1721 | 222448 | 4059374 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 5720 |
| 200 | Central Compressor | 12W27NA | 4.1721 | 221949 | 4051405 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 5796 |
| 201 | Central Compressor | 11W31NA | 4.1721 | 234105 | 4086728 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 5960 |
| 202 | Central Compressor | 11W30NA | 4.1721 | 233971 | 4077162 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 5897 |
| 203 | Central Compressor | 11W27NA | 4.1721 | 233526 | 4050867 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 6229 |
| 204 | Central Compressor | 10W30NA | 4.1721 | 242380 | 4076917 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 6403 |
| 205 | Central Compressor | 10W29NA | 4.1721 | 241980 | 4067374 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 5796 |
| 206 | Central Compressor | 10W28NA | 4.1721 | 241646 | 4058942 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 6032 |
| 207 | Central Compressor | 10W27NA | 4.1721 | 241335 | 4050400 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 6196 |
| 208 | Central Compressor | 10W26NA | 4.1721 | 241023 | 4041857 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 6668 |
| 209 | Central Compressor | 9W32NA | 4.1721 | 253036 | 4096716 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 7000 |
| 210 | Central Compressor | 9W29NA | 4.1721 | 252369 | 4067062 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 5897 |

Table F-8 Far Field Modeling Input Values (Assuming 9.6 g/hp-hr NOx Wellhead Engines)(continued)

| Source Count | Source Type | Location/ID | NOx Emission Rate (g/s) | UTM | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|--------------------|-------------|-------------------------|-------------|--------------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | | Easting (m) | Northing (m) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 211 | Central Compressor | 9W28nA | 4.1721 | 252169 | 4058564 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 6799 |
| 212 | Central Compressor | 9W27nA | 4.1721 | 252013 | 4049799 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 6202 |
| 213 | Central Compressor | 9W26nA | 4.1721 | 251857 | 4041034 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 6389 |
| 214 | Central Compressor | 8W32nA | 4.1721 | 262246 | 4096383 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 6796 |
| 215 | Central Compressor | 8W29nA | 4.1721 | 261490 | 4066795 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 6596 |
| 216 | Central Compressor | 8W27nA | 4.1721 | 261023 | 4049288 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 6052 |
| 217 | Central Compressor | 7W32nA | 4.1721 | 271968 | 4096027 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 6796 |
| 218 | Central Compressor | 7W31nA | 4.1721 | 271678 | 4085794 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 6419 |
| 219 | Central Compressor | 7W29nA | 4.1721 | 271211 | 4066506 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 6596 |
| 220 | Central Compressor | 7W28nA | 4.1721 | 271033 | 4057986 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 6796 |
| 221 | Central Compressor | 7W27nA | 4.1721 | 270789 | 4048776 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 6603 |
| 222 | Central Compressor | 6W29nA | 4.1721 | 280244 | 4066328 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 6458 |
| 223 | Central Compressor | 6W28nA | 4.1721 | 279914 | 4057650 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 6530 |
| 224 | Central Compressor | 6W27nA | 4.1721 | 279602 | 4048184 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 6596 |
| 225 | Central Compressor | 5W30nA | 4.1721 | 290187 | 4086260 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 6652 |
| 226 | Central Compressor | 5W29nA | 4.1721 | 289498 | 4066039 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 6698 |

Table F-9 Far Field Modeling Input Values (Assuming 2.0 g/hp-hr NOx Wellhead Engines)

| Source Count | Source Type | Location/ID | NOx Emission Rate (g/s) | UTM | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|----------------|-------------|-------------------------|-------------|--------------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | | Easting (m) | Northing (m) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 1 | Well emissions | 14W32NA | 0.7547 | 203235 | 4096434 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6209 |
| 2 | Well emissions | 14W31NA | 0.7547 | 203173 | 4088127 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5796 |
| 3 | Well emissions | 14W29NA | 0.7547 | 203147 | 4068123 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5415 |
| 4 | Well emissions | 13W32NA | 0.7547 | 215344 | 4095670 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5973 |
| 5 | Well emissions | 13W32NB | 0.7547 | 214344 | 4095670 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6009 |
| 6 | Well emissions | 13W32NC | 0.7547 | 216344 | 4095670 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5989 |
| 7 | Well emissions | 13W31NA | 0.7547 | 214525 | 4087566 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5796 |
| 8 | Well emissions | 13W31NB | 0.7547 | 213525 | 4087566 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5796 |
| 9 | Well emissions | 13W31NC | 0.7547 | 215525 | 4087566 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5763 |
| 10 | Well emissions | 13W31ND | 0.7547 | 214525 | 4088566 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5796 |
| 11 | Well emissions | 13W30NA | 0.7547 | 214071 | 4077901 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5596 |
| 12 | Well emissions | 13W30NB | 0.7547 | 213071 | 4077901 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5494 |
| 13 | Well emissions | 13W30NC | 0.7547 | 215071 | 4077901 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5697 |
| 14 | Well emissions | 13W29NA | 0.7547 | 213627 | 4068389 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5241 |
| 15 | Well emissions | 13W29NB | 0.7547 | 212627 | 4068389 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5238 |
| 16 | Well emissions | 13W29NC | 0.7547 | 214627 | 4068389 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5278 |
| 17 | Well emissions | 13W29ND | 0.7547 | 213627 | 4069389 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5337 |
| 18 | Well emissions | 13W28NA | 0.7547 | 213090 | 4059806 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6016 |
| 19 | Well emissions | 13W28NB | 0.7547 | 212090 | 4059806 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6012 |
| 20 | Well emissions | 13W28NC | 0.7547 | 214090 | 4059806 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6012 |
| 21 | Well emissions | 13W27NA | 0.7547 | 212581 | 4051683 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6042 |
| 22 | Well emissions | 13W26NA | 0.7547 | 212073 | 4043560 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6291 |
| 23 | Well emissions | 12W32NA | 0.7547 | 224108 | 4095578 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6061 |
| 24 | Well emissions | 12W32NB | 0.7547 | 223108 | 4095578 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5996 |
| 25 | Well emissions | 12W31NA | 0.7547 | 223567 | 4086997 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6143 |
| 26 | Well emissions | 12W31NB | 0.7547 | 222567 | 4086997 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6173 |
| 27 | Well emissions | 12W31NC | 0.7547 | 224567 | 4086997 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6291 |
| 28 | Well emissions | 12W30NA | 0.7547 | 223122 | 4077486 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5753 |
| 29 | Well emissions | 12W30NB | 0.7547 | 222122 | 4077486 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5799 |
| 30 | Well emissions | 12W30NC | 0.7547 | 224122 | 4077486 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5717 |
| 31 | Well emissions | 12W29NA | 0.7547 | 222957 | 4067496 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5596 |
| 32 | Well emissions | 12W29NB | 0.7547 | 221957 | 4067496 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5596 |
| 33 | Well emissions | 12W29NC | 0.7547 | 223957 | 4067496 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5596 |
| 34 | Well emissions | 12W28NA | 0.7547 | 222448 | 4059374 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5720 |
| 35 | Well emissions | 12W28NB | 0.7547 | 221448 | 4059374 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5648 |

Table F-9 Far Field Modeling Input Values (Assuming 2.0 g/hp-hr NOx Wellhead Engines) (continued)

| Source Count | Source Type | Location/ID | NOx Emission Rate (g/s) | UTM | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|----------------|-------------|-------------------------|-------------|--------------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | | Easting (m) | Northing (m) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 36 | Well emissions | 12W28NC | 0.7547 | 223448 | 4059374 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5802 |
| 37 | Well emissions | 12W27NA | 0.7547 | 221949 | 4051405 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5796 |
| 38 | Well emissions | 12W27NB | 0.7547 | 220949 | 4051405 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5796 |
| 39 | Well emissions | 12W27NC | 0.7547 | 222949 | 4051405 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5930 |
| 40 | Well emissions | 12W27ND | 0.7547 | 221949 | 4052405 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5812 |
| 41 | Well emissions | 12W26NA | 0.7547 | 221451 | 4043437 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6101 |
| 42 | Well emissions | 12W25NA | 0.7547 | 220952 | 4035468 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6196 |
| 43 | Well emissions | 11W32NA | 0.7547 | 234283 | 4097339 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6580 |
| 44 | Well emissions | 11W32NB | 0.7547 | 233283 | 4097339 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6813 |
| 45 | Well emissions | 11W32NC | 0.7547 | 234283 | 4098339 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6580 |
| 46 | Well emissions | 11W31NA | 0.7547 | 234105 | 4086728 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5960 |
| 47 | Well emissions | 11W31NB | 0.7547 | 233105 | 4086728 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5996 |
| 48 | Well emissions | 11W30NA | 0.7547 | 233971 | 4077162 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5897 |
| 49 | Well emissions | 11W30NB | 0.7547 | 232971 | 4077162 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5796 |
| 50 | Well emissions | 11W30NC | 0.7547 | 234971 | 4077162 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5996 |
| 51 | Well emissions | 11W29NA | 0.7547 | 233815 | 4067574 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5524 |
| 52 | Well emissions | 11W29NB | 0.7547 | 232815 | 4067574 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5546 |
| 53 | Well emissions | 11W28NA | 0.7547 | 233660 | 4059187 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5648 |
| 54 | Well emissions | 11W28NB | 0.7547 | 232660 | 4059187 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5796 |
| 55 | Well emissions | 11W27NA | 0.7547 | 233526 | 4050867 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6229 |
| 56 | Well emissions | 11W27NB | 0.7547 | 232526 | 4050867 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6298 |
| 57 | Well emissions | 11W27NC | 0.7547 | 234526 | 4050867 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6048 |
| 58 | Well emissions | 11W26NA | 0.7547 | 233393 | 4042547 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6396 |
| 59 | Well emissions | 11W26NB | 0.7547 | 232393 | 4042547 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6376 |
| 60 | Well emissions | 11W25NA | 0.7547 | 233259 | 4034227 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6360 |
| 61 | Well emissions | 11W25NB | 0.7547 | 232259 | 4034227 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6317 |
| 62 | Well emissions | 10W32NA | 0.7547 | 243226 | 4097050 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6826 |
| 63 | Well emissions | 10W32NB | 0.7547 | 242226 | 4097050 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6826 |
| 64 | Well emissions | 10W31NA | 0.7547 | 242692 | 4086528 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6170 |
| 65 | Well emissions | 10W30NA | 0.7547 | 242380 | 4076917 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6403 |
| 66 | Well emissions | 10W30NB | 0.7547 | 241380 | 4076917 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6596 |
| 67 | Well emissions | 10W30NC | 0.7547 | 243380 | 4076917 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6396 |
| 68 | Well emissions | 10W29NA | 0.7547 | 241980 | 4067374 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5796 |
| 69 | Well emissions | 10W29NB | 0.7547 | 240980 | 4067374 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5602 |
| 70 | Well emissions | 10W29NC | 0.7547 | 242980 | 4067374 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5796 |

Table F-9 Far Field Modeling Input Values (Assuming 2.0 g/hp-hr NOx Wellhead Engines) (continued)

| Source Count | Source Type | Location/ID | NOx Emission Rate (g/s) | UTM | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|----------------|-------------|-------------------------|-------------|--------------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | | Easting (m) | Northing (m) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 71 | Well emissions | 10W28NA | 0.7547 | 241646 | 4058942 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6032 |
| 72 | Well emissions | 10W28NB | 0.7547 | 240646 | 4058942 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6170 |
| 73 | Well emissions | 10W27NA | 0.7547 | 241335 | 4050400 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6196 |
| 74 | Well emissions | 10W27NB | 0.7547 | 240335 | 4050400 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6193 |
| 75 | Well emissions | 10W27NC | 0.7547 | 242335 | 4050400 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6396 |
| 76 | Well emissions | 10W27ND | 0.7547 | 241335 | 4051400 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6396 |
| 77 | Well emissions | 10W26NA | 0.7547 | 241023 | 4041857 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6668 |
| 78 | Well emissions | 10W26NB | 0.7547 | 240023 | 4041857 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6632 |
| 79 | Well emissions | 10W26NC | 0.7547 | 242023 | 4041857 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6639 |
| 80 | Well emissions | 10W25NA | 0.7547 | 240712 | 4033315 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6596 |
| 81 | Well emissions | 10W25NB | 0.7547 | 239712 | 4033315 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6596 |
| 82 | Well emissions | 9W32NA | 0.7547 | 253036 | 4096716 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 7000 |
| 83 | Well emissions | 9W32NB | 0.7547 | 252036 | 4096716 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6983 |
| 84 | Well emissions | 9W32NC | 0.7547 | 254036 | 4096716 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 7019 |
| 85 | Well emissions | 9W31NA | 0.7547 | 252814 | 4086283 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6396 |
| 86 | Well emissions | 9W30NA | 0.7547 | 252613 | 4076584 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6091 |
| 87 | Well emissions | 9W30NB | 0.7547 | 251613 | 4076584 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6019 |
| 88 | Well emissions | 9W29NA | 0.7547 | 252369 | 4067062 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5897 |
| 89 | Well emissions | 9W29NB | 0.7547 | 251369 | 4067062 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5770 |
| 90 | Well emissions | 9W29NC | 0.7547 | 253369 | 4067062 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6019 |
| 91 | Well emissions | 9W28NA | 0.7547 | 252169 | 4058564 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6799 |
| 92 | Well emissions | 9W28NB | 0.7547 | 251169 | 4058564 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6996 |
| 93 | Well emissions | 9W28NC | 0.7547 | 253169 | 4058564 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6796 |
| 94 | Well emissions | 9W27NA | 0.7547 | 252013 | 4049799 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6202 |
| 95 | Well emissions | 9W27NB | 0.7547 | 251013 | 4049799 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6229 |
| 96 | Well emissions | 9W27NC | 0.7547 | 253013 | 4049799 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6196 |
| 97 | Well emissions | 9W26NA | 0.7547 | 251857 | 4041034 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6389 |
| 98 | Well emissions | 9W26NB | 0.7547 | 250857 | 4041034 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6396 |
| 99 | Well emissions | 9W26NC | 0.7547 | 252857 | 4041034 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6383 |
| 100 | Well emissions | 9W26ND | 0.7547 | 251857 | 4042034 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6330 |
| 101 | Well emissions | 9W25NA | 0.7547 | 251701 | 4032269 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6596 |
| 102 | Well emissions | 8W32nA | 0.7547 | 262246 | 4096383 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6796 |
| 103 | Well emissions | 8W32nB | 0.7547 | 261246 | 4096383 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6796 |
| 104 | Well emissions | 8W32nC | 0.7547 | 263246 | 4096383 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6813 |
| 105 | Well emissions | 8W31nA | 0.7547 | 261957 | 4086060 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6426 |

Table F-9 Far Field Modeling Input Values (Assuming 2.0 g/hp-hr NOx Wellhead Engines) (continued)

| Source Count | Source Type | Location/ID | NOx Emission Rate (g/s) | UTM | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|----------------|-------------|-------------------------|-------------|--------------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | | Easting (m) | Northing (m) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 106 | Well emissions | 8W30nA | 0.7547 | 261734 | 4076339 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6396 |
| 107 | Well emissions | 8W29nA | 0.7547 | 261490 | 4066795 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6596 |
| 108 | Well emissions | 8W29nB | 0.7547 | 260490 | 4066795 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6596 |
| 109 | Well emissions | 8W28nA | 0.7547 | 261267 | 4058275 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5996 |
| 110 | Well emissions | 8W28nB | 0.7547 | 260267 | 4058275 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 5973 |
| 111 | Well emissions | 8W27nA | 0.7547 | 261023 | 4049288 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6052 |
| 112 | Well emissions | 8W27nB | 0.7547 | 260023 | 4049288 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6596 |
| 113 | Well emissions | 8W27nC | 0.7547 | 262023 | 4049288 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6124 |
| 114 | Well emissions | 8W26nA | 0.7547 | 260778 | 4040300 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 7036 |
| 115 | Well emissions | 8W26nB | 0.7547 | 259778 | 4040300 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6888 |
| 116 | Well emissions | 8W26nC | 0.7547 | 261778 | 4040300 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6806 |
| 117 | Well emissions | 8W25nA | 0.7547 | 260533 | 4031313 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6612 |
| 118 | Well emissions | 7W32nA | 0.7547 | 271968 | 4096027 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6796 |
| 119 | Well emissions | 7W32nB | 0.7547 | 270968 | 4096027 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6396 |
| 120 | Well emissions | 7W32nC | 0.7547 | 272968 | 4096027 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6796 |
| 121 | Well emissions | 7W31nA | 0.7547 | 271678 | 4085794 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6419 |
| 122 | Well emissions | 7W31nB | 0.7547 | 270678 | 4085794 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6517 |
| 123 | Well emissions | 7W31nC | 0.7547 | 272678 | 4085794 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6399 |
| 124 | Well emissions | 7W30nA | 0.7547 | 271478 | 4076161 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6576 |
| 125 | Well emissions | 7W29nA | 0.7547 | 271211 | 4066506 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6596 |
| 126 | Well emissions | 7W29nB | 0.7547 | 270211 | 4066506 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6596 |
| 127 | Well emissions | 7W28nA | 0.7547 | 271033 | 4057986 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6796 |
| 128 | Well emissions | 7W28nB | 0.7547 | 270033 | 4057986 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6396 |
| 129 | Well emissions | 7W28nC | 0.7547 | 272033 | 4057986 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6678 |
| 130 | Well emissions | 7W27nA | 0.7547 | 270789 | 4048776 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6603 |
| 131 | Well emissions | 7W27nB | 0.7547 | 269789 | 4048776 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6596 |
| 132 | Well emissions | 7W27nC | 0.7547 | 271789 | 4048776 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6662 |
| 133 | Well emissions | 7W26nA | 0.7547 | 270544 | 4039566 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6796 |
| 134 | Well emissions | 7W25nA | 0.7547 | 270299 | 4030356 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6776 |
| 135 | Well emissions | 7W24nA | 0.7547 | 270055 | 4021146 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 7000 |
| 136 | Well emissions | 6W32nA | 0.7547 | 281436 | 4095756 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6016 |
| 137 | Well emissions | 6W32nB | 0.7547 | 280436 | 4095756 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6170 |
| 138 | Well emissions | 6W31nA | 0.7547 | 280978 | 4085519 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6196 |
| 139 | Well emissions | 6W30nA | 0.7547 | 280629 | 4075905 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6596 |
| 140 | Well emissions | 6W29nA | 0.7547 | 280244 | 4066328 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6458 |

Table F-9 Far Field Modeling Input Values (Assuming 2.0 g/hp-hr NOx Wellhead Engines) (continued)

| Source Count | Source Type | Location/ID | NOx Emission Rate (g/s) | UTM | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|----------------|-------------|-------------------------|-------------|--------------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | | Easting (m) | Northing (m) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 141 | Well emissions | 6W29nB | 0.7547 | 279244 | 4066328 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6485 |
| 142 | Well emissions | 6W28nA | 0.7547 | 279914 | 4057650 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6530 |
| 143 | Well emissions | 6W28nB | 0.7547 | 278914 | 4057650 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6396 |
| 144 | Well emissions | 6W28nC | 0.7547 | 280914 | 4057650 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6596 |
| 145 | Well emissions | 6W27nA | 0.7547 | 279602 | 4048184 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6596 |
| 146 | Well emissions | 6W27nB | 0.7547 | 278602 | 4048184 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6596 |
| 147 | Well emissions | 6W27nC | 0.7547 | 280602 | 4048184 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6560 |
| 148 | Well emissions | 6W26nA | 0.7547 | 279290 | 4038717 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6642 |
| 149 | Well emissions | 6W25nA | 0.7547 | 278978 | 4029250 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6596 |
| 150 | Well emissions | 6W24nA | 0.7547 | 279978 | 4029250 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6596 |
| 151 | Well emissions | 6W24nB | 0.7547 | 280978 | 4029250 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6596 |
| 152 | Well emissions | 5W32nA | 0.7547 | 290521 | 4095426 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6796 |
| 153 | Well emissions | 5W31nA | 0.7547 | 290187 | 4085260 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6416 |
| 154 | Well emissions | 5W30nA | 0.7547 | 290187 | 4086260 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6652 |
| 155 | Well emissions | 5W30nB | 0.7547 | 289187 | 4086260 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6639 |
| 156 | Well emissions | 5W29nA | 0.7547 | 289498 | 4066039 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6698 |
| 157 | Well emissions | 5W29nB | 0.7547 | 288498 | 4066039 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6681 |
| 158 | Well emissions | 5W29nC | 0.7547 | 290498 | 4066039 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6796 |
| 159 | Well emissions | 5W28nA | 0.7547 | 289253 | 4057341 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6796 |
| 160 | Well emissions | 5W28nB | 0.7547 | 288253 | 4057341 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6665 |
| 161 | Well emissions | 5W27nA | 0.7547 | 288897 | 4047819 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6580 |
| 162 | Well emissions | 5W27nB | 0.7547 | 287897 | 4047819 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6560 |
| 163 | Well emissions | 5W26nA | 0.7547 | 288541 | 4038298 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6596 |
| 164 | Well emissions | 5W26nB | 0.7547 | 287541 | 4038298 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6596 |
| 165 | Well emissions | 5W25nA | 0.7547 | 288185 | 4028777 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6691 |
| 166 | Well emissions | 4W32nA | 0.7547 | 298997 | 4095137 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6921 |
| 167 | Well emissions | 4W32nB | 0.7547 | 297997 | 4095137 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 7200 |
| 168 | Well emissions | 4W31nA | 0.7547 | 298752 | 4085082 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6996 |
| 169 | Well emissions | 4W29nA | 0.7547 | 298329 | 4065794 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 7298 |
| 170 | Well emissions | 4W28nA | 0.7547 | 298107 | 4057074 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 7396 |
| 171 | Well emissions | 4W27nA | 0.7547 | 297929 | 4047330 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6996 |
| 172 | Well emissions | 4W27nB | 0.7547 | 296929 | 4047330 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 7029 |
| 173 | Well emissions | 4W26nA | 0.7547 | 297751 | 4037586 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 7072 |
| 174 | Well emissions | 4W26nB | 0.7547 | 296751 | 4037586 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 7196 |
| 175 | Well emissions | 4W25nA | 0.7547 | 297573 | 4027842 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 7196 |

Table F-9 Far Field Modeling Input Values (Assuming 2.0 g/hp-hr NOx Wellhead Engines) (continued)

| Source Count | Source Type | Location/ID | NOx Emission Rate (g/s) | UTM | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|--------------------|-------------|-------------------------|-------------|--------------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | | Easting (m) | Northing (m) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 176 | Well emissions | 4W24nA | 0.7547 | 298573 | 4027842 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 7196 |
| 177 | Well emissions | 3W31nA | 0.7547 | 308273 | 4084859 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 7396 |
| 178 | Well emissions | 3W30nA | 0.7547 | 308229 | 4075182 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 7596 |
| 179 | Well emissions | 3W29nA | 0.7547 | 308407 | 4065616 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 6996 |
| 180 | Well emissions | 3W28nA | 0.7547 | 308451 | 4056651 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 7098 |
| 181 | Well emissions | 3W27nA | 0.7547 | 308518 | 4046774 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 7196 |
| 182 | Well emissions | 3W26nA | 0.7547 | 308585 | 4036896 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 7390 |
| 183 | Well emissions | 3W26nB | 0.7547 | 307585 | 4036896 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 7347 |
| 184 | Well emissions | 3W25nA | 0.7547 | 308652 | 4027019 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 7344 |
| 185 | Well emissions | 3W25nA | 0.7547 | 307652 | 4027019 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 7203 |
| 186 | Well emissions | 2W30nA | 0.7547 | 317194 | 4075026 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 7797 |
| 187 | Well emissions | 2W28nA | 0.7547 | 317817 | 4056317 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 7295 |
| 188 | Well emissions | 2W27nA | 0.7547 | 317995 | 4046195 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 7396 |
| 189 | Well emissions | 2W26nA | 0.7547 | 318173 | 4036073 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 7797 |
| 190 | Well emissions | 2W24nA | 0.7547 | 319173 | 4036073 | 1.5 | 0.2 | 5.5 | 477 | 1.0 | 1.1 | 7308 |
| 191 | Central Compressor | 13W32NA | 4.1721 | 215344 | 4095670 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 5973 |
| 192 | Central Compressor | 13W31NA | 4.1721 | 214525 | 4087566 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 5796 |
| 193 | Central Compressor | 13W30NA | 4.1721 | 214071 | 4077901 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 5596 |
| 194 | Central Compressor | 13W29NA | 4.1721 | 213627 | 4068389 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 5241 |
| 195 | Central Compressor | 13W28NA | 4.1721 | 213090 | 4059806 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 6016 |
| 196 | Central Compressor | 12W32NA | 4.1721 | 224108 | 4095578 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 6061 |
| 197 | Central Compressor | 12W31NA | 4.1721 | 223567 | 4086997 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 6143 |
| 198 | Central Compressor | 12W30NA | 4.1721 | 223122 | 4077486 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 5753 |
| 199 | Central Compressor | 12W28NA | 4.1721 | 222448 | 4059374 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 5720 |
| 200 | Central Compressor | 12W27NA | 4.1721 | 221949 | 4051405 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 5796 |
| 201 | Central Compressor | 11W31NA | 4.1721 | 234105 | 4086728 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 5960 |
| 202 | Central Compressor | 11W30NA | 4.1721 | 233971 | 4077162 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 5897 |
| 203 | Central Compressor | 11W27NA | 4.1721 | 233526 | 4050867 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 6229 |
| 204 | Central Compressor | 10W30NA | 4.1721 | 242380 | 4076917 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 6403 |
| 205 | Central Compressor | 10W29NA | 4.1721 | 241980 | 4067374 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 5796 |
| 206 | Central Compressor | 10W28NA | 4.1721 | 241646 | 4058942 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 6032 |
| 207 | Central Compressor | 10W27NA | 4.1721 | 241335 | 4050400 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 6196 |
| 208 | Central Compressor | 10W26NA | 4.1721 | 241023 | 4041857 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 6668 |
| 209 | Central Compressor | 9W32NA | 4.1721 | 253036 | 4096716 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 7000 |
| 210 | Central Compressor | 9W29NA | 4.1721 | 252369 | 4067062 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 5897 |

Table F-9 Far Field Modeling Input Values (Assuming 2.0 g/hp-hr NOx Wellhead Engines) (continued)

| Source Count | Source Type | Location/ID | NOx Emission Rate (g/s) | UTM | | Stack Parameters | | | | Building | | Elevation (ft) |
|--------------|--------------------|-------------|-------------------------|-------------|--------------|------------------|--------------|----------------|-----------|------------|-----------|----------------|
| | | | | Easting (m) | Northing (m) | Height (m) | Diameter (m) | Velocity (m/s) | Temp (°K) | Height (m) | Width (m) | |
| 211 | Central Compressor | 9W28nA | 4.1721 | 252169 | 4058564 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 6799 |
| 212 | Central Compressor | 9W27nA | 4.1721 | 252013 | 4049799 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 6202 |
| 213 | Central Compressor | 9W26nA | 4.1721 | 251857 | 4041034 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 6389 |
| 214 | Central Compressor | 8W32nA | 4.1721 | 262246 | 4096383 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 6796 |
| 215 | Central Compressor | 8W29nA | 4.1721 | 261490 | 4066795 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 6596 |
| 216 | Central Compressor | 8W27nA | 4.1721 | 261023 | 4049288 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 6052 |
| 217 | Central Compressor | 7W32nA | 4.1721 | 271968 | 4096027 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 6796 |
| 218 | Central Compressor | 7W31nA | 4.1721 | 271678 | 4085794 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 6419 |
| 219 | Central Compressor | 7W29nA | 4.1721 | 271211 | 4066506 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 6596 |
| 220 | Central Compressor | 7W28nA | 4.1721 | 271033 | 4057986 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 6796 |
| 221 | Central Compressor | 7W27nA | 4.1721 | 270789 | 4048776 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 6603 |
| 222 | Central Compressor | 6W29nA | 4.1721 | 280244 | 4066328 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 6458 |
| 223 | Central Compressor | 6W28nA | 4.1721 | 279914 | 4057650 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 6530 |
| 224 | Central Compressor | 6W27nA | 4.1721 | 279602 | 4048184 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 6596 |
| 225 | Central Compressor | 5W30nA | 4.1721 | 290187 | 4086260 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 6652 |
| 226 | Central Compressor | 5W29nA | 4.1721 | 289498 | 4066039 | 6.7 | 0.6 | 19 | 644 | 4.8 | 4.5 | 6698 |