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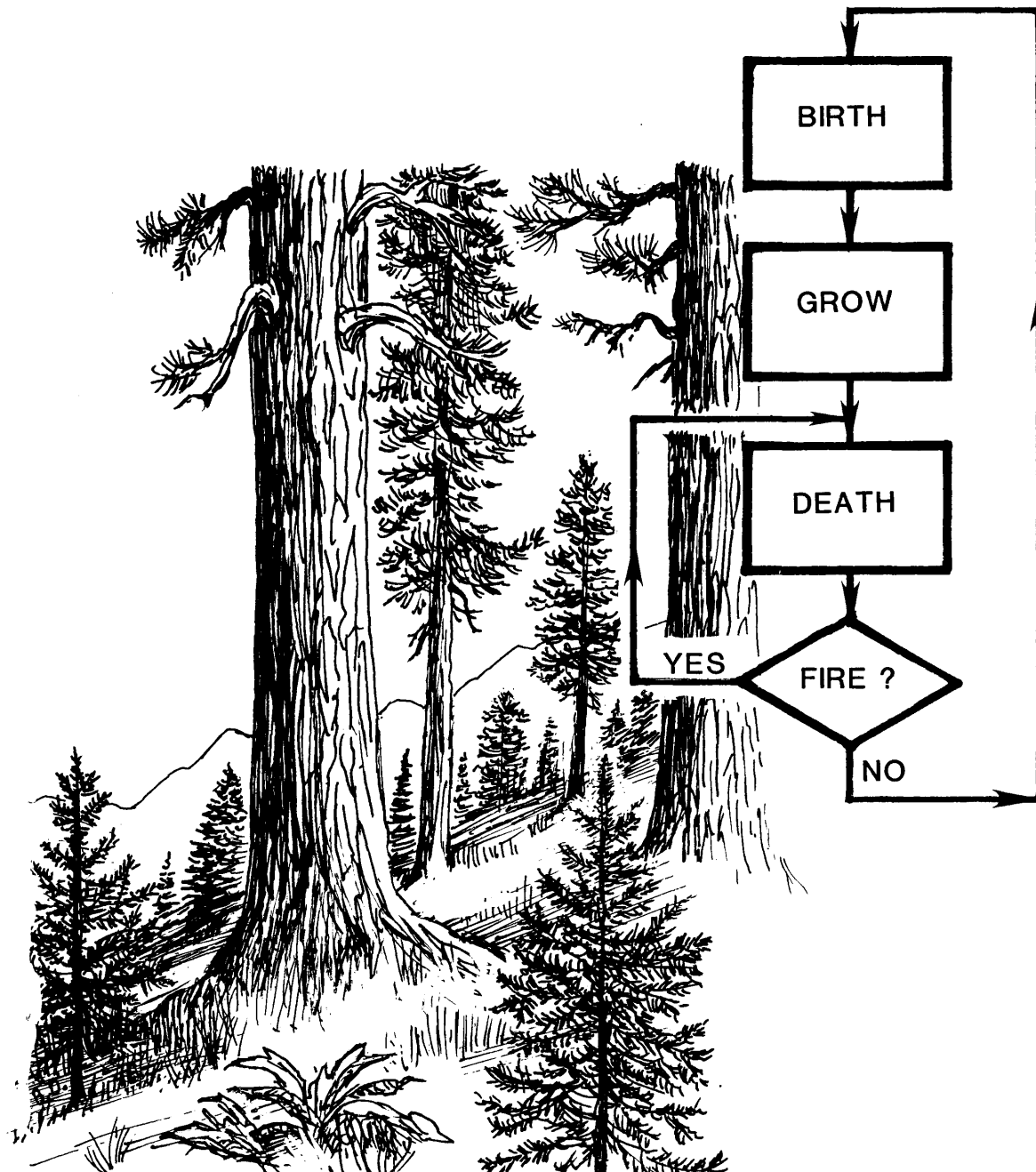
General Technical
Report INT-266

September 1989



FIRESUM—An Ecological Process Model for Fire Succession in Western Conifer Forests

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RESEARCH SUMMARY

A successional process model has been developed to simulate long-term stand dynamics in forests of the Northern Rockies. The model can be used to evaluate fire effects differences for various fire regimes, including prescribed burning at different intervals, complete fire exclusion (fire suppression), and pre-1900 fire frequencies. The model, **FIRESUM** (a **FIRE S**uccession **M**odel), simulates tree establishment, growth, and mortality, along with live and dead fuel accumulation, fire behavior, and fuel reduction on a 400-square-meter plot. The following influences on tree establishment and growth are included in the model: growing season warmth, water stress, light tolerance, and site

quality. The model predicts basal area by species, duff and fuel accumulation, and fire intensities. All model algorithms are discussed, and corresponding parameters for several tree species are presented. The model is continually being tested and verified. Recent test results show **FIRESUM** underpredicts basal area by an average of 10 to 20 percent. A sensitivity analysis of **FIRESUM** showed that parameters associated with the growth algorithm are most critical. The model was designed so that it could be applied to different forest types with minimal modification of the computer code.

ACKNOWLEDGMENTS

We thank the following individuals who participated in workshops that provided critical analysis during model development: James R. Habeck, Steven W. Running, Ronald H. Wakimoto, and Hans R. Zuuring of the University of Montana (Missoula); Patricia L. Andrews, Jim D. Chew, William H. Frandsen, Arnold I. Finklin, Roger G. Hungerford, David Pierce, Elizabeth D. Reinhardt, Kevin C. Ryan, and Raymond C. Shearer of the Forest Service, U.S. Department of Agriculture, in Missoula.

CONTENTS

	Page
Introduction	1
The Model	1
Model Description	1
Tree Growth	4
Tree Regeneration	7
Tree Mortality	8
Fuel Accumulation	10
Fire Characteristics	12
Fuel Consumption	13
Model Output	13
Model Testing and Analysis	14
Validation and Verification	14
Sensitivity Analysis	15
Summary and Conclusions	16
References	17
Appendix A: Program listing for FIRESUM	21
Appendix B: Example of the TREE.DAT file	73
Appendix C: Example of the SITE.DAT file	75
Appendix D: Example of the CONTRL.DAT file	76

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INTRODUCTION

The long-term effects on forest composition and structure of different fire management alternatives, such as complete suppression of all fires and prescribed fires of varying intervals and prescriptions, are often difficult to quantify. Although many researchers have studied successional communities arising after fire (Arno and others 1985; Kessell and Potter 1980; Steele and Geier-Hayes 1987; Stickney 1980; Means; 1981), investigations of the effects of successive fires—that is a “fire regime”—on vegetation are rare. The long time periods involved greatly complicate quantification of effects of successive fires based on field evidence. Computerized simulation models, however, offer an alternative means of comparing long-term effects of different fire regimes on forest vegetation. An additional benefit of developing such models is detection of areas where knowledge is deficient and future research is critically needed.

We developed a computer model, called FIRESUM (a **FIRE S**uccession Model), to simulate the effect of different fire regimes on tree composition, stand structure, and fuel loading in forests of the inland portion of the northwestern United States. Comparison of long-term fire effects predictions under different fire regimes could prove useful for developing fire management prescriptions to meet resource management objectives.

FIRESUM was created by extensively modifying the process model SILVA (Kercher and Axelrod 1981), which simulates forest succession involving fire in mixed conifer forests of the California Sierra Nevada. Parameters and algorithms within SILVA were revised, deleted, or added to reflect current knowledge of ecologic processes inherent in various types of forests. Currently, FIRESUM can be applied to ponderosa pine/Douglas-fir and whitebark pine/subalpine fir forests of the Inland Northwest and the Northern Rocky Mountains.

The purpose of this paper is to describe algorithms and routines used in FIRESUM along with related modeling assumptions. The parameters used to quantify each algorithm are also discussed.

THE MODEL

Model Description

FIRESUM is a deterministic model containing stochastic properties. Tree growth, woody fuel accumulation, and litterfall are simulated deterministically, whereas tree

establishment and mortality are stochastic algorithms. The model simulates all processes on an individual tree level in a 400-square-meter area called the simulation plot. Because the particular combination of stochastic events occurring within a given FIRESUM simulation represent only one case among the set of many possible simulation outcomes, the model repeats simulations many times to obtain an average of simulated results.

FIRESUM is a gap-replacement model (Shugart and West 1980) following the approach used for JABOWA (Botkin and others 1972) in which individual trees are grown deterministically using an annual time step, difference equation. Tree growth is affected by several site factors, including available light, water stress, and growing season warmth. Tree establishment and mortality are modeled stochastically using Monte Carlo techniques. Fuel loadings are calculated yearly. Fires are introduced at various intervals, and effects of each fire are simulated by reduction of litter, duff, and down woody fuels; and by tree mortality and postfire tree regeneration and growth.

FIRESUM was programmed in the FORTRAN 77 language and contains over 2000 lines of code, with 43 subroutines and a main driver (appendix A). A generalized flow chart for FIRESUM execution is presented in figure 1. FIRESUM execution starts with tree and site parameters read into the program from external data files (TREE.DAT and SITE.DAT as shown in appendixes B and C) in subroutines TREE and SITE.DAT. External files allow efficient modification of parameters and facilitate the execution of simultaneous runs. The tree parameter file (appendix B) consists of numbers describing each tree species in terms of the model's algorithms. For example, the maximum height of each tree species used in growth algorithm of FIRESUM (H_m in appendix B) is represented in the tree parameter file. The site file (appendix C) contains parameters that describe the simulation site. Initial tree data for a sample plot are read from data file CONTRL.DAT (appendix D) into subroutine CONTRL and then these input trees are distributed on the plot in DIST. These data represent the simulation stand at the start of simulation. Parameters used to summarize site conditions are read from subroutine SITE.DAT and used to compute growth reduction factors in CALC and SITE. Frequency of cone crops and fire years are computed in CYCLES and RINGS, respectively. Establishment of new trees is done in BIRTH, trees are then grown in subroutine GROW and subject to mortality in KILL, thereby completing a normal tree life cycle.

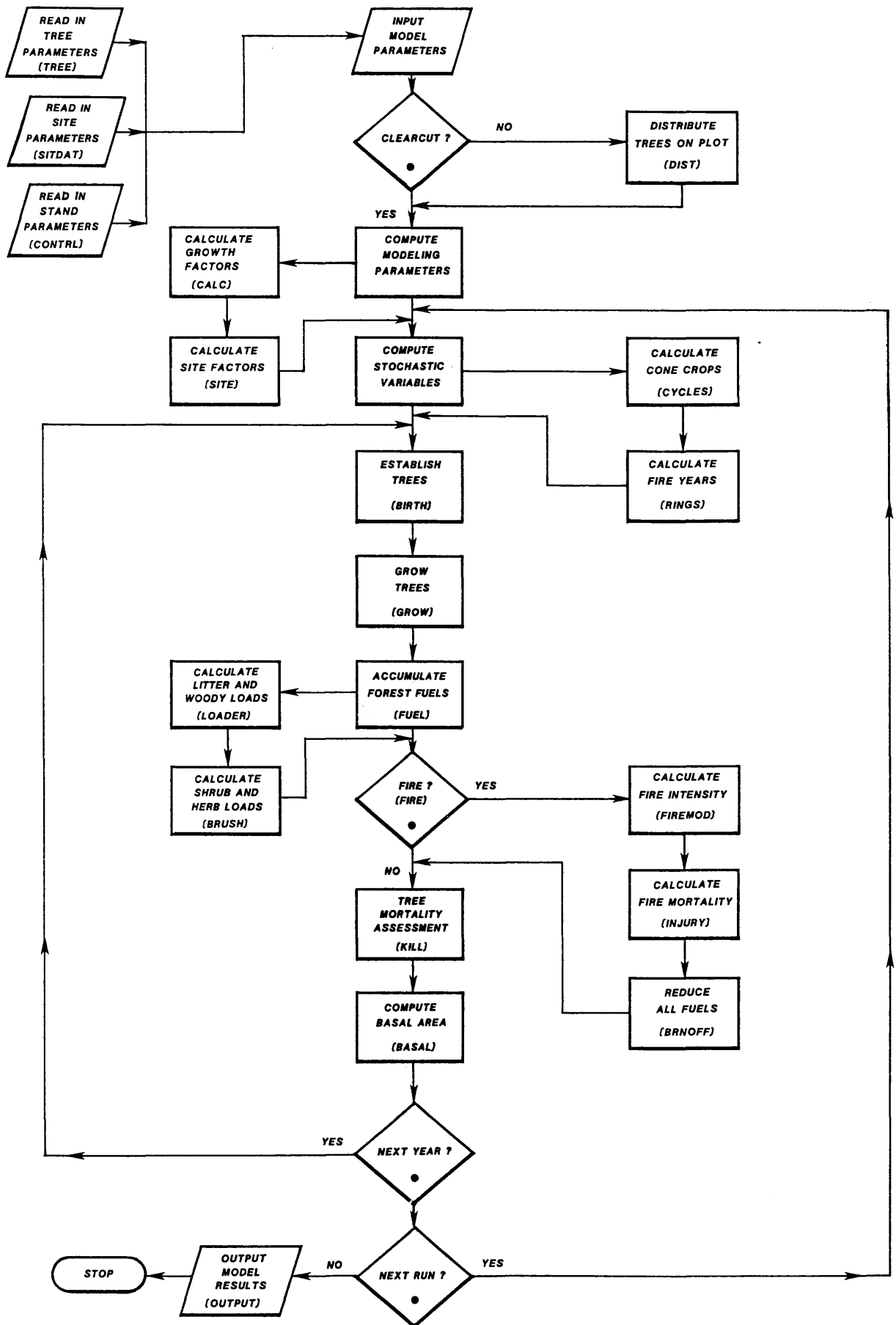


Figure 1—An instructional guide to program logic for the simulation process model FIRESUM. Program subroutines are noted in parentheses.

Fuel loadings are annually estimated in FUEL, LOADER, and BRUSH, and are passed to subroutine FIRE when a fire is initiated. Fire intensity is calculated in FIREMOD from these fuel loading predictions. Subsequent tree mortality from fire is estimated in INJURY using function RISK. Fuel reduction is performed in subroutine BRNOFF and the new loadings are passed back to FUEL. BASAL stores a running average annual basal area by species, which is then passed to subroutine OUTPUT at program termination. OUTPUT prints final results to external files.

Several subroutines not shown in figure 1 are also used in model execution. Subroutine SNAG estimates woody fuel contributed by recently dead trees and adds that amount to the fuel bed. FOLIAGE computes the leaf area

of each tree on the simulation plot. Subroutines BEETLE and RUST are used to compute mortality caused by the mountain pine beetle and white pine blister rust. Crown fires are modeled in subroutine CROWN, which predicts when a ground or surface fire becomes hot enough to ignite tree crowns. This submodel is in the developmental stage and needs additional testing before implementation into FIRESUM. Subroutine RANDX is the random number generator. The growth reduction factor for water stress is computed in WRSTRS. The degree of shading based on leaf area is computed in SHADE, and the flame length is computed in FLTEMP.

The following are detailed descriptions of major simulation algorithms in FIRESUM. Values for parameters in these algorithms are shown in table 1.

Table 1—A summary table of parameter values for all species currently implemented in FIRESUM

Parameter symbol ¹ (units)	Tree species ²									
	PIPO	ABGR	PSME	PICO	LAOC	ABLA	PIEN	PIAL	PICO	LALY
Hm (cm)	6,562.5	5,333.7	5,715.0	4,115.0	6,857.5	4,175.5	5,456.0	3,657.0	4,115.0	3,048.0
Dm (cm)	250.5	139.4	208.8	110.0	250.0	126.7	234.4	182.0	110.0	168.0
AGEMAX (years)	450.0	275.0	350.0	220.0	450.0	180.0	320.0	1,000.0	350.0	800.0
DMIN (deg-days)	2,249.9	2,496.6	1,810.4	1,215.3	1,817.4	801.8	801.4	800.0	1,500.0	800.0
DOPT (deg-days)	4,010.0	4,200.0	4,200.0	4,200.0	4,200.0	3,800.0	3,800.0	3,000.0	3,000.0	3,000.0
DMAX (deg-days)	8,608.0	7,194.0	7,194.0	7,194.0	7,194.0	6,200.0	6,200.0	5,200.0	6,500.0	5,200.0
Shade tolerance ³	I	T	M	I	I	T	M	M	I	I
SV (cm ² /cm ²)	57.6	72.9	69.1	64.7	184.0	70.0	54.2	57.6	64.7	184.0
PLA (m/m)	3.54	2.04	2.85	3.54	3.54	2.04	2.04	3.54	3.54	3.54
WSO (proportion)	.25	.47	.32	.38	.38	.65	.65	.33	.40	.75
Pc (probability)	.395	.333	.446	.318	.438	.333	.167	N/A	.318	.368
hc (years)	2.0	2.0	1.0	2.0	2.0	2.0	3.0	1.0	2.0	1.0
BC (proportion)	.070	.033	.065	.014	.069	.015	.022	.015	.014	.031
DKF (proportion)	.0575	.0339	.0339	.0460	.1310	.0339	.0339	.057	.044	.201
DKL (proportion)	.1116	.0667	.1167	.1186	.2000	.0667	.0667	.112	.112	.200
LTD (proportion)	.5500	.6500	.6500	.6600	.8500	.6500	.6500	.550	.660	.650
DKD (proportion)	.2280	.2210	.2210	.2210	.2210	.2210	.2210	.221	.221	.321
AINC (centimeters)	.012	.005	.007	.015	.016	.008	.008	.006	.016	.007
Lc (percent)	40.0	80.0	80.0	40.0	40.0	80.0	80.0	50.0	40.0	45.0
NYR (years)	4.0	7.0	5.0	3.0	1.0	7.0	6.0	7.0	3.0	1.0

- | | |
|---|--|
| ¹ Hm = Maximum attainable height | Pc = Probability of good cone crop |
| Dm = Maximum attainable diameter | hc = Years blocked after good cone crop |
| Agemax = Maximum attainable age | BC = Bark thickness conversion factor |
| DMIN = Minimum number degree-days | DKF = Decomposition loss from needlefall |
| DOPT = Optimum number of degree-days | DKL = Decomposition loss from litter |
| DMAX = Maximum number of degree-days | LTD = Decomposition loss from litter to duff |
| Shade tolerance = Shade tolerance class | DKD = Decomposition loss from duff |
| SV = Surface to volume ratio of foliage | AWC = Minimum diameter growth for mortality |
| PLA = Projected leaf area conversion factor | Lc = Live crown ratio |
| WSO = Minimum AET:PET ratio | NYR = Years needles remain on tree |

²Species codes are: PIPO = ponderosa pine, ABGR = grand fir, PSME = Douglas-fir, LAOC = western larch, ABLA = subalpine fir, PIEN = Engelmann spruce, PIAL = whitebark pine, PICO = lodgepole pine, LALY = subalpine larch.

³Shade tolerance categories are I-shade intolerant, M-moderately shade tolerant, and T-shade tolerant.

Tree Growth (Subroutine GROW)

Growth is modeled by an annual increase in tree diameter measured at breast height (d.b.h.) [1.37 meters above ground line] (Botkin and others 1972). Diameter increment growth (dD/dt) is calculated from the time step equation:

$$\frac{dD}{dt} = \frac{GD [1 - (DH)/(D_m H_m)]}{274 + 3b_2 D - 4b_3 D^2} [rAL rN rW rDEGD] \quad (1)$$

where D is the diameter (d.b.h. in centimeters) and H is the height of the tree (centimeters), D_m and H_m are maximum attainable d.b.h. and height (centimeters) for the tree species in the Northern Rocky Mountain region. Values for D_m and H_m (table 1) are taken from Patterson and others (1985), Fowells (1965), Pando (1973), Pfister and others (1977), Hunt (1986), and other studies of old-growth forests. Tree height (H) is computed from:

$$H = 137 + b_2 D - b_3 D^2 \quad (2)$$

where b_2 and b_3 are species-dependent constants. Constants G , b_2 , and b_3 are estimated using equations 3 and 5 in Botkin and others (1972), which have D_m , H_m , and maximum attainable age (AGEMAX in years) as independent variables.

The remaining variables in the equation are growth reduction factors (values between 0.0 and 1.2) that represent the total effect of surrounding environment on tree growth. These factors are modeled as tree growth response to available light (rAL), nutrient supply (rN), water relations (rW), and temperature regime ($rDEGD$). Optimal growth is only possible when all factors equal 1.0.

Available light (AL) for an individual tree is calculated according to Beer's Law (Kercher and Axelrod 1982) using the equation:

$$AL = AL_0 e^{-k_j \sum LAI} \quad (3)$$

where $\sum LAI$ is the sum of leaf area indexes for all trees taller than the tree under consideration and AL_0 is available light at full sunlight (standardized to 1.0). Variable k_j is the extinction coefficient per meter for canopy type j .

Because forest canopy characteristics differ by tree composition, that is forest community, it was necessary to stratify extinction coefficient (k) (and many other simulation parameters mentioned later in this paper) by a classification of fire groups (Davis and others 1980) synthesized from the Montana habitat types of Pfister and others (1977). In their classification, habitat types were grouped into similar categories based on vegetation composition, tree ecology and fire histories (table 2). Canopy extinction coefficients by fire group are presented in table 3.

Because utilization of available light by a tree depends on degree of shade tolerance for that species, light response equations were stratified by shade tolerance class (shade intolerant, moderately shade tolerant, and shade tolerant as shown in table 1). These equations, from Botkin and others (1972), are

$$\text{Shade tolerant: } rAL = 1 - e^{-4.84(AL-0.05)} \quad (4)$$

$$\text{Shade intolerant: } rAL = 2.24 [1 - e^{-1.136(AL-0.08)}] \quad (5)$$

where rAL is a dimensionless number between zero and 1.0 (1.2 for shade intolerant species), and AL expresses available light (also dimensionless). Shade-tolerant species are able to attain higher growth rates in heavily shaded conditions (fig. 2). But light saturation for tolerant species occurs at a much lower level of photosynthetic activity than for the shade intolerants. Although three tolerance classes are recognized in FIRESUM, the tolerant equation (4) includes species that are tolerant and moderately tolerant of shade.

Leaf area was difficult to calculate due to the absence of leaf area equations for Inland Northwest tree species. In FIRESUM we estimated leaf area (LA in square centimeters) from:

$$LA = \frac{[(CW * PFOL) / CD] * SV_i}{PLA_i} \quad (6)$$

where CW is crown weight in grams, $PFOL$ is proportion of crown that is foliar weight, CD is needle density in grams per cubic centimeter (assumed to be 0.5 for all species based on the authors' unpublished data), SV_i is

Table 2—Fire groups implemented in FIRESUM. Tree species prevalent in the ponderosa pine/Douglas-fir forests are capable of attaining dominance in any of these fire groups

Number	Fire group name ¹	Predominant overstory	Fire frequency
1	Warm, dry ponderosa pine	Pure ponderosa pine	3-8 year intervals
2	** Grand fir	Larch, Douglas-fir, ponderosa pine, grand fir	20-200 years
3	** Warm, dry Douglas-fir	Ponderosa pine, Douglas-fir	5-20+ years
4	Cool, dry Douglas-fir	Douglas-fir	35-40 years
5	** Moist Douglas-fir	Douglas-fir, lodgepole pine, ponderosa pine	around 40 years
6	Cool habitat types	Lodgepole pine	100-500 years
7	Dry, lower subalpine types	Douglas-fir, lodgepole pine, spruce	50-130 years

¹ Fire groups are from Davis and others (1980).

** Only these fire groups have ponderosa pine/Douglas-fir ecosystems. The other groups are included in FIRESUM for future research. All fire groups contain the seven species implemented in FIRESUM.

Table 3—FIRESUM parameter values stratified by fire group. Descriptions of the fire groups are provided in Table 2 (Davis and others 1980)

Parameter symbol ¹	Fire group number						
	1	2	3	4	5	6	7
k	0.426	0.525	0.426	0.426	0.426	0.426	0.525
BARMAX	.0071	.0149	.0074	.0091	.0107	.0083	.0111
SPM	1.0	6.0	2.0	4.0	3.0	5.0	5.0
PRO	.990	.717	.668	.768	.768	.985	.852
LBULK	15.8	41.6	21.9	25.3	36.0	43.3	38.1
DBULK	76.9	45.8	76.9	110.6	110.6	139.5	142.7

¹Parameter descriptions:

- k = Extinction coefficient (dimensionless)
- BARMAX = Maximum attainable basal area (m²/m²)
- SPM = Maximum seedling density (seedlings/m²)
- PRO = Dead shrubby fuel in shrub biomass (proportion)
- LBULK = Bulk density of litter (kg/m³)
- DBULK = Bulk density of duff (kg/m³)

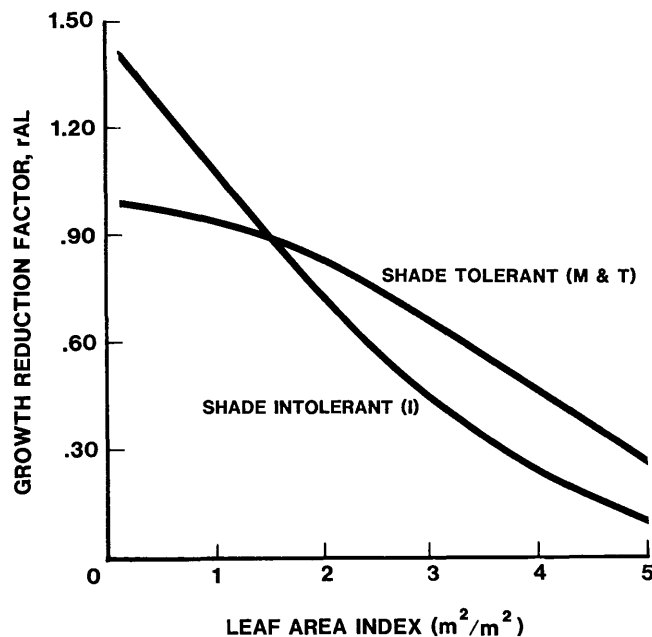


Figure 2—Relationship of the growth reduction factor for shading to leaf area index (equations 4, 5). This range of leaf area indexes is commonly found in ponderosa pine/Douglas-fir forests of the Inland Northwest. Shade tolerant categories *M* (moderately shade tolerant) and *T* (shade tolerant) are represented by the same function. Shade intolerant species (*I*) have a different function.

needle surface-to-volume ratio for species *i* (values are from Lopushinsky [1970], Brown [1970], and Minore [1979]), and PLA_i is a conversion factor to estimate projected leaf area from all-sided leaf area for species *i* (values calculated from Kaufmann and others [1982], Smith [1972], and unpublished data). Crown weight and proportion foliar weight are estimated from regression equations (Brown 1976, 1978; Moeur 1981) that use d.b.h. as the independent variable. All other variables are constants (table 1).

The effect of resource availability (tree crowding) on tree growth was indirectly modeled as a function of stand basal area with the equation:

$$rN = 1 - (BAR/BARMAX_j) \quad (7)$$

where BAR is basal area (square meters) of simulation stand and $BARMAX_j$ is maximum attainable basal area (square meters) for stands in fire group *j*. Values for $BARMAX_j$ (table 3) are estimated from Pfister and others (1977) and Arno and others (1985). The factor rN goes to zero as BAR approaches $BARMAX_j$ (fig. 3).

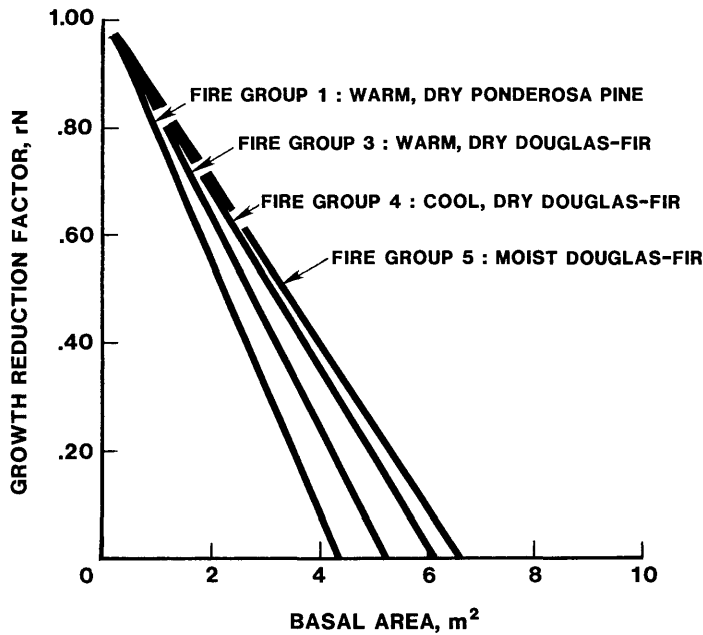


Figure 3—Growth reduction factor (rN) relationship to plot basal area in four fire groups.

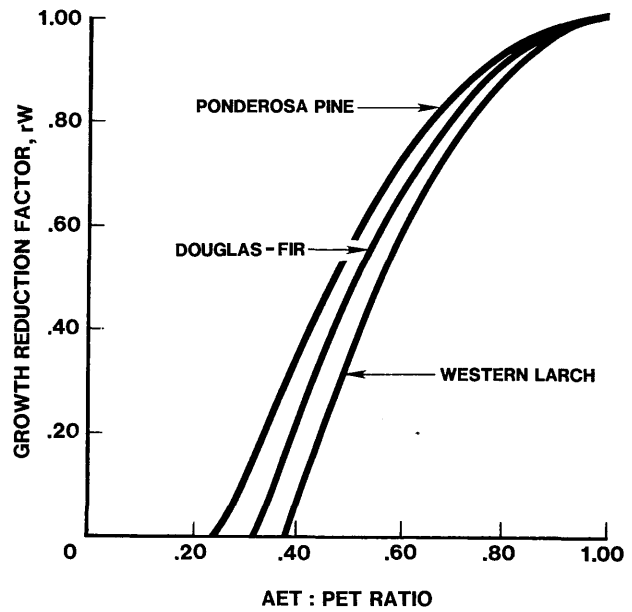


Figure 4—Relationship of the growth reduction factor rW to the simulation plot's actual to potential evapotranspiration ratio (AET:PET).

Modeling growth response to water stress (rW) in FIRESUM is taken from Reed (1980) and Reed and Clark (1979) where the ratio of actual to potential evapotranspiration (AET:PET) is the driving variable. This ratio indicates the relative aridity of the simulation climate. The water response (rW) equation is:

$$rW = 1 - [(1 - APR)/(1 - WSO_i)]^2 \quad (8)$$

where APR is the annual AET:PET ratio for the site and WSO is the lower limit of tolerance in APR for species i . This parabolic function (fig. 4) reaches maximum when APR equals 1.0, which assumes growth is not inhibited when annual AET exceeds annual PET. Values of WSO_i for each species were calculated from weather data collected at or near the edge of species i 's natural distribution where water becomes the limiting factor (Little 1971). Actual evapotranspiration is calculated using the water balance equations presented in Kercher and Axelrod (1981), which use monthly precipitation ($BASEP$), soil water-holding capacity ($TEXT$), soil depth ($TILL$), and a runoff constant ($EXCESS$) as variables (values shown in appendix C). Potential evapotranspiration is calculated from the Thornthwaite and Mather (1957) equations.

Climatic influence on diameter growth was modeled as a function of temperature expressed as growing degree-days (Botkin and others 1972; Shugart and Nobel 1981). The parabolic equation taken from Reed and Clark (1979) is given as

$$\text{when } DMIN_i < DEGD < DMAX_i: \\ rDEGD = \frac{[(DEGD - DMIN_i)(DMAX_i - DEGD)]^V}{[(DOPT_i - DMIN_i)(DMAX_i - DOPT_i)]^V} \quad (9)$$

where $V = (DMAX_i - DOPT_i)/(DOPT_i - DMIN_i)$

$$\text{when } DEGD < DMIN_i \text{ or } DEGD > DMAX_i: \\ rDEGD = 0.0 \quad (10)$$

where $rDEGD$ is a number between 0 and 1.0, $DEGD$ is number of degree-days calculated from weather data submitted as input for a simulation run; $DMIN_i$ and $DMAX_i$ are the maximum and minimum degree-days defining the geographic range of species i ; and $DOPT_i$ is number of degree-days for optimum growth of species i .

Figure 5 illustrates the ability of Douglas-fir to grow in colder environments (lower number of degree-days) as compared with ponderosa pine. Note the value $rDEGD$ equals 1.0 at $DOPT_i$. Growing degree-days are calculated using equation 9 in Botkin and others (1972). This equation employs a base temperature of 4 °C to define growing season and uses mean monthly temperatures for January and July as minimum and maximum yearly temperatures. $DMAX_i$ and $DMIN_i$ were estimated from weather data collected at extremes of species i 's geographical distribution in the Inland Northwest (Shugart 1984). $DOPT_i$ was calculated from weather data at stations that were at or near areas where site index values for species i were maximum. Additional information from Alexander and others (1984), Dale and Hemstrom (1984), Fowells (1965), Hellmers and others (1970), and Little (1971) was used to further quantify these three parameters (table 1).

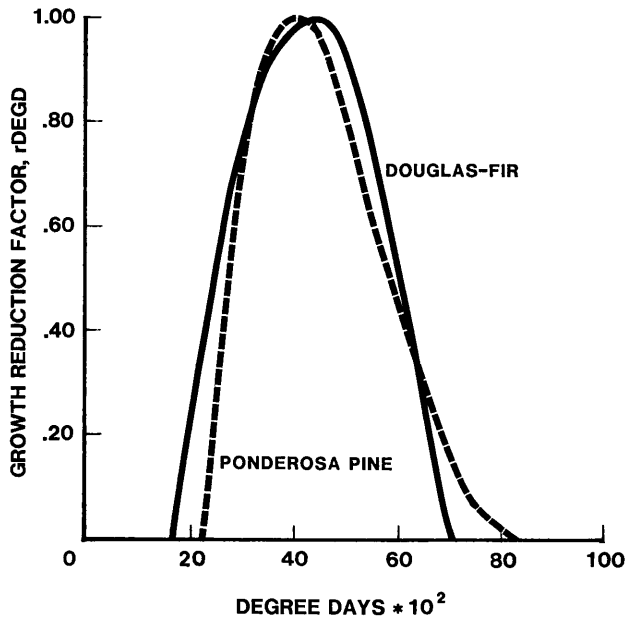


Figure 5—The relationship of degree-days for the simulation plot to the growth reduction factor representing growing season warmth and its effect on tree growth ($rDEGD$).

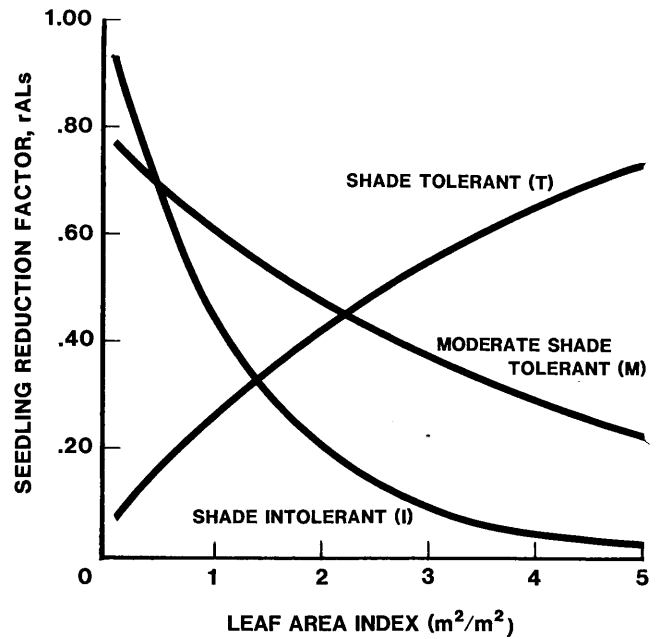


Figure 6—Effects of shading (leaf area index) on the seedling reduction factor $rALS$ for three shade tolerance categories.

Tree Regeneration (Subroutine BIRTH)

Trees were established on the simulation plot if two criteria were met. First, simulated growing degree-days ($DEGD$) had to exceed $DMIN_i$ for the species under consideration (Knapp and Smith 1982; Shugart 1984; Weinstein and others 1982); and second, the threshold AET:PET ratio (defined earlier as APR in subroutine $GROW$) had to be greater than WSO_i (Brix 1979; Kercher and Axelrod 1984; Lopushinsky and Klock 1974). If the above criteria were true, then size of cone crop was evaluated.

Each year a species can have a good or poor cone crop, but trees are established only in good seed years. The Monte Carlo method discussed in Kercher and Axelrod (1984) was used to determine good cone crop years. In this stochastic method, p_c is the probability of a good cone crop. Each year a random number is generated and, if it is less than p_c , a good cone crop is simulated. But this process is blocked for a number of years after a good cone crop (Kercher and Axelrod 1981). The number of blocked years ($h_c - 1$) is based on the assumption that trees must store sufficient energy reserves before generating another good cone crop. Good seed years are determined at the beginning of each simulation run and remain constant for each replicate run within a simulation. Values for parameters p_c and h_c (table 1) are from Boe (1954), Eis and Craigdallie (1983), Lotan and Perry (1983), Shearer (1985), and Shearer and Schmidt (1970).

The number of trees established on the simulation plot is calculated from the equation:

$$FNJ_i = SPM_j * PTREE_i * PSUR_i * rAL_s * rSRF_i \quad (11)$$

where FNJ_i is the number of seedlings established for species i , SPM_j is the maximum number of seedlings (includes all species) that can become established on 1.0 m^2 for fire group j , $PTREE_i$ is proportion of seed trees of species i , $PSUR_i$ is the probability of seedling survival considering the duff depth, rAL_s is a reduction factor accounting for effects of limited light on seedling establishment, and $rSRF$ is a reduction factor that models the effect of distance of seed source on tree establishment.

The factor rAL_s ranges from 0 to 1.0, depending on three levels of shade tolerance. The set of equations for calculating rAL_s are:

$$\text{Shade intolerant:} \quad rAL_s = e^{(-0.8*LAI)} \quad (12)$$

$$\text{Moderate shade tolerant:} \quad rAL_s = e^{(-0.25*LAI - 1.0)} \quad (13)$$

$$\text{Shade tolerant:} \quad rAL_s = 1 - e^{(-0.25*LAI - 0.2)} \quad (14)$$

where LAI is plot leaf area index (square meters of leaf area per square meter of plot area). The coefficients were derived by the authors, based on unpublished data about the dynamics of seedling establishment. Shade-tolerant species are able to establish the most seedlings at low light levels (fig. 6) (Grime and Jeffery 1965).

Values for SPM_j (table 3) were taken from Alexander (1984), Arno and others (1985), Knapp and Smith (1982), Pfister and Shearer (1977), Schimdt and others (1976), Shearer (1974), Shearer (1975), and Shearer (1985). Seed trees were defined as any tree greater than 10 cm d.b.h. or having an age greater than some minimum threshold (variable YSC , values shown in appendix B). This assumes only trees meeting these criterion are able to

produce appreciable quantities of seed. The variable $PTREE_i$ roughly estimates a species contribution to the seedbank; it is calculated by dividing the number of seed trees for species i by the total number seed trees. To account for off-site seed dispersion, tree species not represented on the plot were assigned a value of 0.05 for $PTREE_i$.

$PSUR_i$ was calculated using regression equations developed from a study on litter and duff depth reduction in north Idaho (Boyce 1985). The independent variable in these equations is depth of litter and duff in centimeters (DEPTH). These equations are:

$$\text{Ponderosa pine:} \\ PSUR = 1.0 - 0.164 * DEPTH \quad R^2 = 0.94 \quad (15)$$

$$\text{Grand fir:} \\ PSUR = 1.0 - 0.149 * DEPTH \quad R^2 = 0.90 \quad (16)$$

$$\text{Douglas-fir:} \\ PSUR = 1.0 - 0.160 * DEPTH \quad R^2 = 0.99 \quad (17)$$

$$\text{Lodgepole pine:} \\ PSUR = 1.0 - 0.161 * DEPTH \quad R^2 = 0.93 \quad (18)$$

$$\text{Western larch:} \\ PSUR = 1.0 - 0.177 * DEPTH \quad R^2 = 0.99 \quad (19)$$

In the absence of specific data for subalpine fir and Engelmann spruce, the grand fir equation was used to represent $PSUR$ for those species. Negative values for $PSUR$ were equated to zero.

The distance the simulation plot is from seed sources directly influences the number of trees established. Factor $rSRF$ attempts to simulate this relationship. Reduction equations are of the form:

$$Y_i = \frac{e^{(a+bX_i)}}{e^a} \quad (20)$$

where Y_i is the $rSRF$ for species i with values between 0 and 1, X_i is the distance from species i 's seed source, which is input into FIRESUM (value $DIST$ in appendix D); and a and b are species-derived constants based on data provided by McCauley and others (1985). These values (variable $DISEQU(1,i)$ for a , variable $DISEQU(2,i)$ for coefficient b) are shown in appendix B.

All new trees are established as saplings of 1.0 cm diameter at breast height (d.b.h.) and 1.37 m tall. These new trees are added to the simulation after a lag period of 25 to 50 years, depending on the site (value LAG in appendix B).

The absence of seed trees for a species on the plot presents a special case in FIRESUM. Distances to seed source from simulation plot by species are input into the model. The factor $rSRF$ and the number of seed trees are computed annually for each species. But the value of $rSRF$ only enters into the seedling equation(s) when all seed trees of that species are eliminated from the simulation plot, because of beetle epidemic or successional replacement, for example. It is assumed in FIRESUM that the seed source of eliminated species composes 5 percent of the total seed crop trees outside the simulation plot for all tree species but whitebark pine. If all trees are killed on the plot, such as after a crown fire, the seed source stand is assumed to be identical to the preburn simulation stand.

Whitebark pine regeneration is computed in subroutine PINALB (appendix A), which models the effects of seed crop, Clark's nutcrackers, and light on whitebark regenera-

tion (Keane and others 1989b). This routine is very different from that used for other species and shows how FIRESUM can be modified to simulate life cycles for any tree species. A complete discussion on the whitebark pine regeneration algorithm is presented in Keane and others (1989b).

Tree Mortality (Subroutine KILL)

Four types of tree mortality—random, stress, fire, and insects and disease—are recognized in FIRESUM and are modeled as stochastic functions. "Random mortality" is the chance of death, from endemic insect attack, wind-throw, or other local perturbations that a tree experiences throughout its lifetime. The probability of random mortality (P_r) is calculated by the equation:

$$P_r = 4/AGEMAX_i \quad (21)$$

where $AGEMAX_i$ is the maximum attainable age for species i . It was assumed that only 2 percent of the trees survive to $AGEMAX_i$ to derive equation 21 (Botkin and others 1972). Analysis of stand data from Montana, Idaho, and eastern Oregon (Arno and others 1985; Keen 1940; Seidel 1975) suggests that 2 percent is reasonable.

"Stress mortality" is tree death resulting from severe stress over periods of 2 to 50 years. Stress mortality can be caused by water scarcity, insufficient light, or tree crowding (Kercher and Axelrod 1984, Shugart and Noble 1981). The probability of stress mortality (P_s) is a function of growth increment. If a tree's annual growth increment ($DINC$) is less than a threshold value ($AINC$) for that species, the following equation is executed:

$$P_{s(n+1)} = P_{s(n)} + 0.2 - 0.2 P_{s(n)} \quad (22)$$

where n is the number of stressful years.

A new P_s is calculated each year $DINC$ is less than $AINC$. P_s will eventually equal 0.997 after 30 years in this stressed condition. Values for $AINC$ were estimated by examining the cross-sections of numerous severely suppressed trees.

Mortality due to fire is modeled as a function of fire intensity. When a fire spreads through an area it kills trees by scorching foliage and killing bole cambium. The degree of crown scorch and cambial kill depends on fire intensity and duration. Ryan and Reinhardt (1988) developed an empirical mortality equation that implicitly accounts for both causes of fire death (fig. 7). The equation is:

$$P_{fk} = \frac{1}{1 + \text{EXP}[-1.941 + 6.32(1 - \text{EXP}(BC_i D_k)) + 0.000535 CK_k^2]} \quad (23)$$

where P_{fk} is the probability of mortality from fire for tree k , BC_i is a bark conversion factor for species i , which multiplied by D_k (d.b.h. of tree k in centimeters) provides an estimate of bark thickness for tree k , and CK_k is percentage of scorched crown volume for tree k . Values for BC_i are taken from Faurot (1977), Lange (1971), Lynch (1959), Myers and Alexander (1972), and Ryan and Reinhardt (1988).

Assuming crown shape approximates a paraboloid (Peterson 1985; Ryan and Reinhardt 1988), scorched crown volume was estimated using:

$$CK_k = 100 [B(2L-b) / L^2] \quad (24)$$

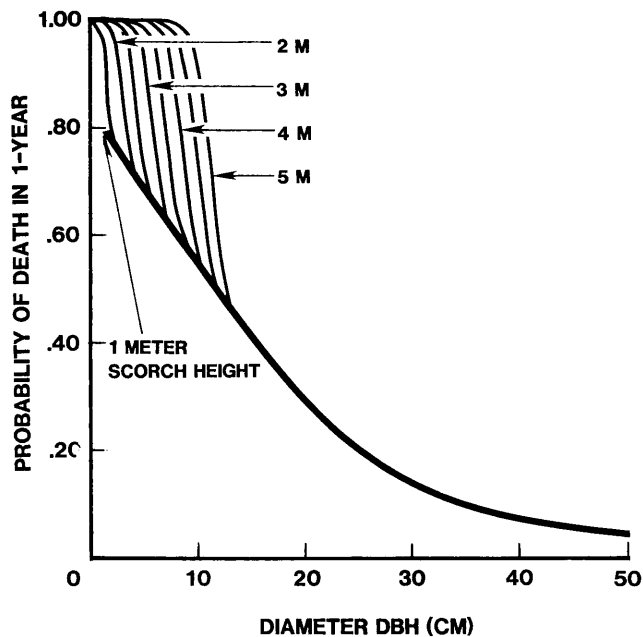


Figure 7—Mortality of ponderosa pine as related to tree diameter (d.b.h.) and crown scorch height. Taken from Ryan and Reinhardt (1988).

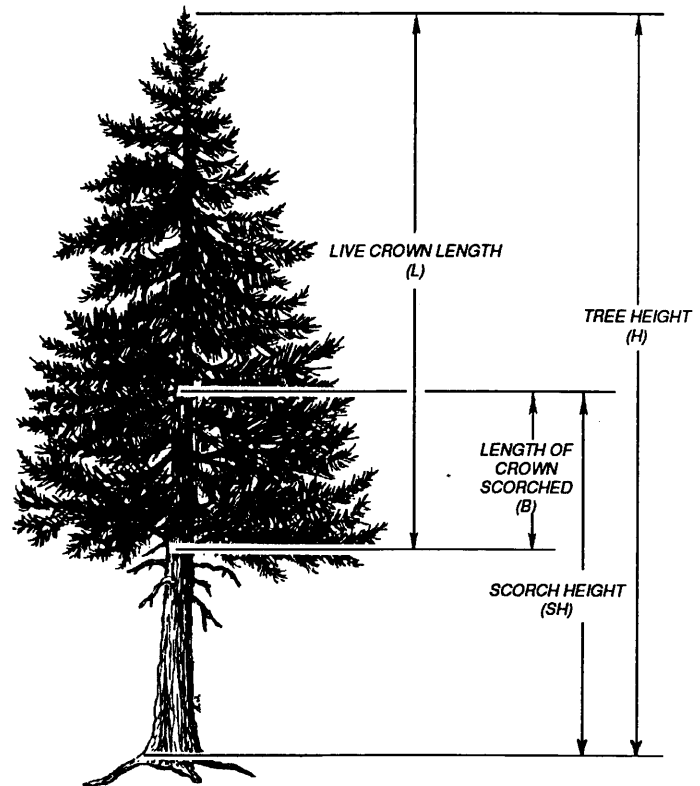


Figure 8—Diagram of important tree dimensions used in the calculation of percent crown scorched. This variable is used to compute tree mortality.

The dimensions B (length of scorched crown in centimeters) and L (length of crown in centimeters) are calculated from tree height and crown length (fig. 8). Tree height (H_k in centimeters) is calculated from the equation:

$$H_k = 137 + b_2 D_k - b_3 D_k^2 \quad (25)$$

where b_2 and b_3 are the species-dependent constants described in the Tree Growth section. The length of crown (L) is the product of live crown ratio (L_c) and tree height. The dimension B is solved by the equation:

$$B = SH - [H - L] \quad (26)$$

where SH is scorch height. Scorch height in meters is calculated from an empirical expression developed by Van Wagner (1973):

$$SH = \frac{C_1 (FI)^{7/6}}{[C_2 (FI) + (C_3 (WIND)^3)^{1/2} (TKILL - T)]} \quad (27)$$

where FI is fire intensity (kilowatts per meter of fireline), $WIND$ is wind speed (kilometers /hour) at midflame height, T is ambient temperature (degrees Celsius), and $TKILL$ is the lethal temperature for tree foliage (assumed as 60 °C). The constants C_1 , C_2 and C_3 were derived empirically and are 0.742 m³/C, 0.0256 (kW/m)^{4/3}, and 0.278 h/km (kW/m)^{7/3}, respectively. Fire intensity is discussed later. Ambient temperature (T) was assumed to be 20 °C, a typical temperature for prescribed fire. Kercher and Axelrod (1984) found equation (26) to be very sensitive to wind-speed at high fuel loadings and insensitive to windspeed at low loadings.

Although the mortality equation (23) includes a wide range of diameters and species, data for small diameter tree mortality were lacking. Because the majority of simulated trees are less than 10 cm d.b.h., additional validation

of the equation with small diameter tree mortality is needed.

Insect and disease mortality is the fourth type of tree mortality represented in FIRESUM. Each insect and disease mortality algorithm was developed from empirical data using regression analysis. In the regression equations, probability of mortality (Y -variable) is computed from many types of independent variables (X -variables) including tree diameter, tree densities, proportion of trees infested, and some site variables. Each type of insect or disease is represented by regression equations for each species it may affect. Also, these equations are stratified by fire group. Currently, FIRESUM models mountain pine beetle-caused mortality on lodgepole pine and whitebark pine, and white pine blister rust-caused mortality on whitebark pine in whitebark pine/subalpine fir forests (Keane and others 1989b). Additional insect and disease mortality equations will be included as they are needed.

Each tree that dies, regardless of the cause of mortality, contributes a portion of its woody branchwood and all of its needles to the fuel bed. Weight of branchwood less than 3 inches in diameter for dead trees is calculated from equations by Brown (1978) and divided equally into the three smallest fuel components (discussed in the next section). It is assumed scorched foliage is not consumed by the fire and is added to the fuel bed, unless the fire was a crown fire. It is assumed all foliage is consumed by a crown fire. Needle weight is computed from equations presented in Brown (1978).

Fuel Accumulation (Subroutine FUEL)

Six dead and two live fuel components are recognized in FIRESUM (table 4). Loadings for these eight fuel components are computed annually, and if a fire is simulated, all fuel loadings are passed to subroutine FIRE, where they are used to estimate fire intensity. Accumulation algorithms are used to represent annual fuel increments for (1) dead woody fuel components, (2) litter and duff components, and (3) live and dead shrub and herbaceous components.

The 1-, 10-, and 100-hour timelag dead woody fuel components are updated each year using the following equations:

$$\text{if } WOOD_{fy} < WOODMAX_{fj} \text{ then} \\ WOOD_{fy+1} = WOOD_{fy} + WOODMAX_{fj} / WYR_{fj} \quad (28)$$

$$\text{else if } WOOD_{fy} > WOODMAX_{fj} \text{ then} \\ WOOD_{fy+1} = WOODMAX_{fj} \quad (29)$$

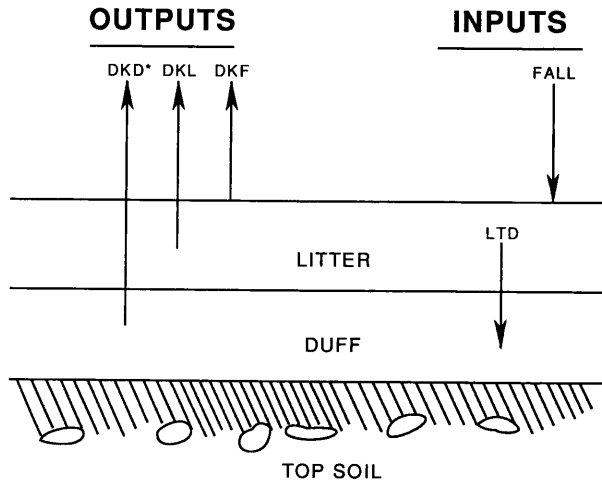
where $WOOD_{fy}$ is fuel loading (kilograms per square meter) for woody fuel component f at year y , $WOODMAX_{fj}$ is the maximum attainable fuel loading for component f in fire group j , and WYR_{fj} is the number of years to reach $WOODMAX_{fj}$ in an undisturbed forest for component f in fire group j . Parameter values (table 5) were taken from Bevins (1977), Brown and Bevins (1986), Brown and See (1981), Jeske and Bevins (1976), Mathews (1972), van Wagtenonk (1972). These equations operate under the assumption of constant accumulation and decomposition rates.

Table 4—Fuel components included in FIRESUM. Timelag woody branchwood categories are described in Fosberg (1970)

Number	Fuel component	Description
Dead Fuel		
<i>Litter Fuel</i>		
1	Litter	Downed tree foliage, no duff material contributes to fire
<i>Downed Woody Branchwood</i>		
2	1-hour time lag	Twigs and branches 0 to 1/4 inch in diameter
3	10-hour time lag	Twigs and branches 1/4 to 1 inch in diameter
4	100-hour time lag	Twigs and branches 1 to 3 inches in diameter
<i>Shrub and Herbaceous Fuel</i>		
5	Shrub	Shrub stemwood 0 to 1 inch diameter
6	Herbaceous	Grass and forbs
Live Fuel		
<i>Shrub and Herbaceous Fuel</i>		
7	Shrub	Foliage and small stemwood on live shrubs
8	Herbaceous	Grass and forbs living on forest floor

Table 5—Parameter values for woody fuel accumulation equations (28) and (29). $WOODMAX$ is the maximum fuel loading and WYR is the time required to reach maximum fuel loading

Parameter symbol	Fire group number						
	1	2	3	4	5	6	7
1-hour dead woody branchwood							
WYR (years)	40.0	40.0	40.0	30.0	30.0	40.0	50.0
WOODMAX (kg/m ²)	.0121	.2710	.0638	.0520	.0520	.1776	.075
10-hour dead wood branchwood							
WYR (years)	40.0	40.0	40.0	30.0	30.0	40.0	50.0
WOODMAX (kg/m ²)	.833	.1548	.2619	.1879	.1879	.4294	.196
100-hour dead woody branchwood							
WYR (years)	40.0	40.0	40.0	30.0	30.0	40.0	50.0
WOODMAX (kg/m ²)	.1546	.1055	.5484	.5365	.5365	.7022	.546



- * DKD - portion duff lost to microbial and faunal respiration
- DKL - portion litter lost from microbial and faunal respiration
- DKF - portion litter lost from overwinter decomposition
- LTD - portion litter incorporated into duff
- FALL - needlefall from conifer species on the plot

Figure 9—Diagram of litter and duff components. Inputs are noted by the downward-pointing arrows; outputs or losses are shown with upward-pointing arrows. This dynamic system is modeled using the coefficients DKD, DKL, DKF, FALL, and LTD.

Litter and duff loadings are calculated using annual dynamic equations in Kercher and Axelrod (1981). These equations are diagrammed in figure 9. The amount of annual needlefall ($FALL_i$) is calculated from the equation:

$$FALL_i = \sum(CW_i) * PFOL_i / NYR_i \quad (30)$$

where $\sum(CW_i)$ is the sum of crown weight over all trees of species i , $PFOL_i$ is the proportion of crown that is needles, and NYR_i is number of years needles remain on a tree of species i . Crown weight and $PFOL_i$ are estimated using regression equations provided by Brown (1976 and 1978). NYR values (table 1) are from Fowells (1965), Gottfried and Ffolliot (1983), Harlow and Harrar (1969), Smith (1972), Turner and Long (1975).

Needlefall (kilograms per square meter), the only input to litter-duff equations, is reduced by a species-dependent proportion (DKF_i) to account for overwinter decomposition (fig. 9). The remaining needlefall is added to the litter and subjected to further decomposition losses. A portion of the litter (DKL_i) is lost to the system while another portion (LTD_i) is added to the duff. Duff loading is then decreased by a decomposition proportion (DKD_i), and this decrement is also lost from the system. Decomposition losses in both litter and duff components are due to microbial and microfauna respiration. Each component is updated annually, and the total litter and duff loading for the stand is calculated by summing across all species. Values for DKF_i , DKL_i , LTD_i , and DKD_i for species i (table 1) are taken from Allison and Klein (1961), Edmonds (1979), Fahey (1983), Fogel and Cromack (1977), Jenny and others (1949), Kercher and Axelrod (1984), Klemmedson and others (1985), Gottfried and Ffolliot (1983), Maclean and Wein (1978), Means and others (1985), Meetenmeyer (1978), Piene and Van Cleve (1978), and Yoneda (1975).

Biomass for shrub and herbaceous fuel types are estimated separately using a function provided by Kercher and Axelrod (1984). The shrub and herbaceous equations are identical, except for internal parameters, and assume shrub and herb biomass on a site has an upper limit dependent on stand productivity. Annual change in biomass is a product of current biomass and a factor that limits growth as maximum biomass is approached. The equation is:

$$MASS_{m(y+1)} = MASS_{m(y)} + n * MASS_{m(y)} [1 - MASS_{m(y)} / BIOMAX_{m(j)}] * rAL \quad (31)$$

where $MASS_{m(y)}$ is biomass (kilograms per square meter) of fuel component m (shrub or herb) at year y , n is a growth constant for small biomass (per year), $BIOMAX_{m(j)}$ is maximum attainable biomass (kilograms per square meter) for fire group j in fuel component m , and rAL is the light response function presented in the tree growth section (equations 4 and 5). Values for n were taken as 1.44 per year for shrubs (Sampson 1944) and 10.842 per year for herbaceous fuel (from unpublished data collected by the authors). $BIOMAX_{m(j)}$ values (table 6) are from Brown and Bevins (1986), Irwin and Peek (1979), and Martin (1982).

Table 6—Parameter values for maximum biomass (BIOMAX) used to compute loadings of live and dead shrub and herbs in equation (31)

Component	Fire group number						
	1	2	3	4	5	6	7
Shrub (kg/m ²)	0.027	0.086	0.076	0.069	0.070	0.016	0.054
Herb (kg/m ²)	.029	.048	.043	.102	.101	.142	.197

Using light response functions (rAL) from the Growth section, shrub and herbaceous loadings are divided into tolerant and intolerant categories. For example, the value for shade intolerant rAL (number between 0 and 1) is multiplied by total shrub biomass to compute intolerant shrub biomass. Biomass estimates for the herbaceous shade tolerance categories are averaged, and then it is assumed that 90 percent of the average is dead at fire incidence. The remaining 10 percent is treated as live fuel. Shrubby biomass is also averaged across shade tolerance categories, but calculations of dead ($SDEAD$) and live ($SLIVE$) loadings (kilograms per square meter) are accomplished using these equations:

$$SDEAD = SAVE * (1 - PRO_j) / PLOTSIZ ;$$

dead shrubby fuels (kg/m²) (32)

$$SLIVE = SAVE * (PRO_j) / PLOTSIZ ;$$

live shrubby fuels (kg/m²) (33)

where $SAVE$ is the average loading (kilograms per square meter) for shade-tolerant and intolerant shrubs, PRO_j is the proportion of dead shrubby fuel in the total shrub biomass for fire group j , and $PLOTSIZ$ is the simulation plot size (square meters). Values for PRO_j (table 3) are from Brown and Bevins (1986).

Total depth of duff and litter (centimeters) is also calculated in subroutine FUEL using the equation:

$$DEPTH = 100 * [(LITT / LBULK_j) + (DUFF / DBULK_j)]$$

(34)

where $DEPTH$ is depth of duff and litter (centimeters), $LITT$ and $DUFF$ are the loadings (kilograms per square meter) of the litter and duff respectively, and $LBULK_j$ and $DBULK_j$ are the bulk densities of the litter and duff strata (respectively) for fire group j . Table 3 shows values of $LBULK_j$ and $DBULK_j$ taken from Brown (1981). This depth is then passed to subroutine BIRTH for use in the Boyce (1985) regression equations (equations 15 to 19).

Fire Characteristics (Subroutine FIRE)

Fire frequency is an input to FIRESUM. The user can specify number of years between fires (fire interval), an actual fire history for the stand consisting of variable fire intervals, or a stochastic function that computes fire interval as a dynamic variable using fire frequency probabilities (Kercher and Axelrod 1984). Fire year information is kept in a program array for reference during each

year of program execution, similar to the cone crop array mentioned in the Tree Regeneration section. This array remains unchanged between simulation runs. If the current simulation year is a fire year, fuel loadings and other input parameters are passed to subroutine FIREMOD and fire intensity is computed, then used to calculate scorch height for use in the fire mortality equation. Subroutine FIREMOD was developed by Albini (1976b) using Rothermel's (1972) model for predicting wildland fire spread. FIREMOD calculates Byram's fire line intensity (kilometers per hour) from a multivariate function comprised of the following user-specified parameters.

1. $WIND$ = windspeed at midflame height (kilometers per hour)
2. $SLOPE$ = slope of stand (degrees)
3. $MOIS_i$ = fractional moisture content of fuel type i
4. $RHOP_i$ = oven-dry particle density for fuel type i (grams per cubic centimeter)
5. $BULK_j$ = bulk density of fuel bed in fire group j (grams per cubic centimeter)
6. SVR_{ij} = mean surface to volume ratio for fuel type i in fire group j (per centimeter)
7. LHV_i = heat content of fuel type i (kilojoules per kilogram)
8. ST_i = mineral content fraction of fuel type i
9. SE_i = silica-free mineral content fraction of fuel type i
10. $MEXT_i$ = moisture of extinction for fuel type i (fraction of weight)
11. $FLOAD_i$ = loading of fuel type i (kilograms per square meter)

Parameters having constant values across fuel components are $WIND$ (kilometers per hour), $MEXT$, and $SLOPE$ (degrees) taken from actual stand and site data and input into the model (appendixes B and C), and LHV (= 18586.7 kJ/kg), ST (= 0.055), and SE (= 0.011) taken from Albini (1976a) and Anderson (1969). Other parameter values are in tables 7, 8, and 9. Variable $FLOAD_i$ is the only dynamic variable in the multivariate function, computed during program execution and passed to FIREMOD. Values for bulk densities and surface to volume ratios are taken from Brown (1970, 1981); particle densities from Brown (1970) and Anderson (1969); and moisture of extinction values from Frandsen and Andrews (1979) and Rothermel (1972). Values for moisture contents and windspeed are specified by the user and are usually taken from a typical fire prescription or fire weather prediction.

Table 7—Values for input parameters to subroutine FIREMOD stratified by fuel type component. $MOIS$ is the fuel moisture content and $RHOP$ is the surface to volume ratio

Parameter symbol	Fuel component number							
	1	2	3	4	5	6	7	8
$MOIS$ (proportion)	0.08	0.08	0.10	0.14	0.10	0.08	1.00	1.50
$RHOP$ (g/cm ²)	.51	.39	.39	.39	.51	.51	.51	.51

Table 8—Bulk densities (BULK) used in subroutine FIREMOD stratified by fire group

Parameter symbol	Fire group number						
	1	2	3	4	5	6	7
BULK (g/cm ³)	0.0158	0.0068	0.0080	0.0115	0.0071	0.0126	0.008

Table 9—Surface area to volume ratios (SVR) used in FIREMOD by fire group and fuel component

Fire group	Fuel component							
	1	2	3	4	5	6	7	8
1	57.41	8.89	3.48	0.95	3.156	91.86	49.20	91.86
2	57.41	11.76	2.88	.98	3.156	91.86	49.20	91.86
3	57.41	16.00	3.08	.98	3.156	91.86	49.20	91.86
4	57.41	16.00	3.08	.98	3.156	91.86	49.20	91.86
5	57.41	16.00	3.08	.98	3.156	91.86	49.20	91.86
6	57.41	16.00	3.08	.98	3.156	91.86	49.20	91.86
7	57.41	11.76	2.88	.98	3.156	91.86	49.20	91.86
8	57.41	11.76	2.88	.98	3.156	91.86	49.20	91.86

Fuel Consumption (Subroutine BRNOFF)

Fuel reduction by fire is computed using equations from Brown and others (1985), Norum (1974), and Sandberg (1980). The woody fuel reduction equations are:

$$1 \text{ and } 10 \text{ hour timelag: } WOOD_{\text{consumed}} = 0.890 (WOOD_{\text{pre}}) - 0.0060 \quad (34)$$

$$100 \text{ hour timelag: } WOOD_{\text{consumed}} = 0.845 (WOOD_{\text{pre}}) - 0.0150 \quad (35)$$

Woody fuel reduction equations use preburn fuel loadings ($WOOD_{\text{pre}}$ in kilograms per square meter) to estimate fuel consumption ($WOOD_{\text{consumed}}$ in kilograms per square meter) independent of fire intensity or moisture content. The proportion of duff reduction, however, is based on preburn duff moisture content ($DMOIST$ in percent). The equation for duff reduction is:

$$DUFF_{\text{post}} = DUFF_{\text{pre}} [(83.7 - 0.426 * DMOIST) / 100.0] \quad (36)$$

where $DUFF_{\text{post}}$ and $DUFF_{\text{pre}}$ are duff loadings (kilograms per square meter) postburn and preburn, respectively. A duff moisture content of 50 percent, typical of many fire prescriptions, was used in simulation runs. All litter, dead shrub, and herbaceous biomass is assumed to be consumed by fire, and the live shrub fuel loading was assumed to be reduced by 90 percent of preburn weight.

MODEL OUTPUT

FIRESUM stores average basal area for each tree species by simulation year in an external file. The program also stores fuel component loadings, duff depths, number of established seedlings, and fire behavior statistics. Any of these variables can be graphed against simulation time using various graphic software packages and related hardware (plotters). Figure 10 presents the graphed results of three contrasting simulation runs. The first run (10a and 10b) had fires occurring at 20-year fixed intervals, which could represent a typical prescribed burning scenario. The second run (10c and 10d) had fires occurring at an 8-year stochastic interval, which simulates pre-1900 fire frequency. And the last run (10e and 10f) is the result of a no-fire scenario (fire suppression). Tree species basal area, and fuel loadings are shown for the simulation plot.

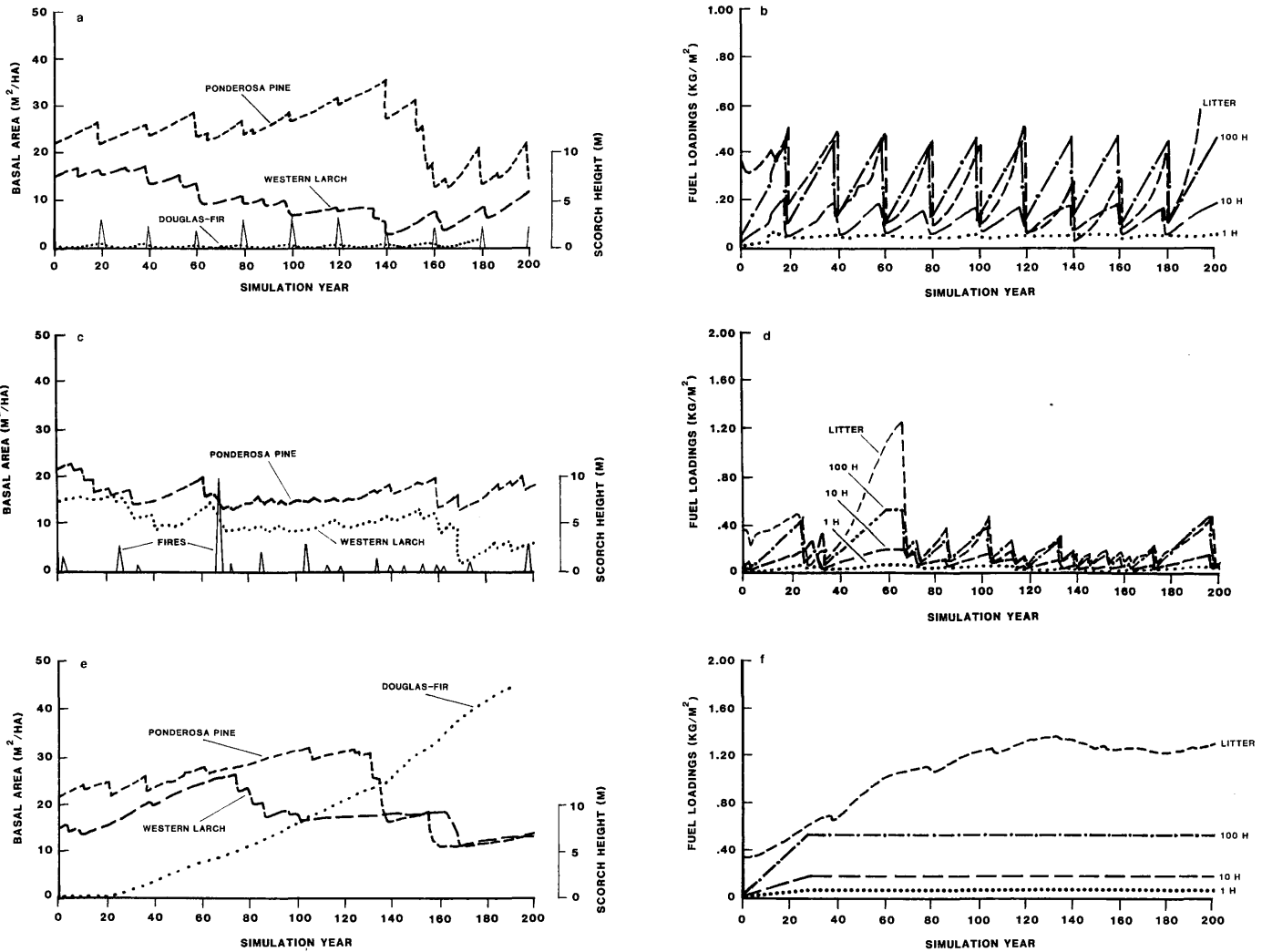


Figure 10 a-f—An example of FIRESUM outputs representing three possible fire scenarios. Graphs 10a and 10b show predicted basal areas and fuel loading for a 20-year fixed fire interval, respectively. Graphs 10c and 10d represent a stochastic fire interval having a mean of 8 years and graphs 10e and 10f predict basal areas and fuel loading in the absence of fires. All graphs are for the same simulation stand and simulate 200 years of ponderosa pine/Douglas-fir succession. Only four fuel components are graphed in 10b, 10d, and 10f: litter, 1-hour, 10-hour, and 100-hour timelag fuel classes. The scorch height of the fires in each scenario is illustrated by the spikes in graphs 10a, 10c, 10e with the corresponding scale located at the far right of these graphs.

MODEL TESTING AND ANALYSIS

Validation and Verification

Testing succession simulation models requires extensive stand data collected at one or more widely separated intervals during successional development. Acquiring these data can be difficult. To test or verify FIRESUM we employed a combination of two methods. The first method was to search the literature for long-term data compatible with the inputs and outputs of FIRESUM. Verification data must have density, age, and diameter (d.b.h.) measurements on trees by species by unit area. These data must have another set of measurements at least 25 to 30 years later, or age-diameter relationships

so that regression equations can be developed and used to project a present stand forward or backward in time (Habeck 1985, Keane and others 1989a). The model is then used to simulate conditions measured by these historic data.

The second method of verification involved sampling two adjacent stands on one site. One stand is a mature forest while the other has resulted from a wildfire (disturbance stand). Tree densities, ages, diameters (d.b.h.), and environmental variables (elevation, aspect, slope, soil depth, etc.) are recorded for each stand (example shown in table 10). The sampled values from the mature stand are used as inputs to FIRESUM. The model is then used to simulate effects of a wildfire on the input stand and grow a subsequent simulation stand of the same age as the

Table 10—Example site and environmental conditions for the ponderosa pine/ Douglas-fir stand used in a FIRESUM execution

Input parameter	Value
Site Description	
Elevation (m)	1,256.0
Slope (degrees)	8.0
Depth to bedrock (ft)	2.5
Water holding cap. (cm/m)	133.3
Fire group	6.0
Fire Weather	
Ambient temperature (°C)	20.0
Wind (km/hour)	3.2
Relative humidity (%)	40.0
Fuel Moisture Contents	
1-hour fuel moisture (%)	8.0
10-hour fuel moisture (%)	10.0
100-hour fuel moisture (%)	14.0
Litter moisture (%)	8.0
Duff moisture (%)	50.0
Dead shrub moisture (%)	10.0
Dead herbaceous moisture (%)	8.0
Live shrub moisture (%)	150.0
Live herbaceous moisture (%)	100.0

Table 11—Results of three tests on the fire succession model FIRESUM

Test	Ecosystem	Basal area	Fuel loading
		--- Percent inaccurate ¹ ---	
Test 1	Ponderosa pine/Douglas-fir	12.2	14.6
Test 2	Whitebark pine/subalpine fir	16.2	10.5
Test 3	Whitebark pine	15.5	11.2
Average percentage inaccurate		14.6	12.1

¹Variable basal area includes basal area for all species on simulation plot. Fuel loading is the total fuel loading (all six fuel components) for the plot. Percentage inaccurate indicates the difference in percentage of the observed from the predicted.

sampled disturbance stand. Results of the simulation are compared with the sampled values from the disturbance stand. The model can be refined or calibrated based on verification results.

Three verification tests have been administered to FIRESUM (table 11) (see Keane and others in press a, in press b). Test results indicated FIRESUM underpredicts basal areas and overpredicts fuel loadings. This is probably due to inaccurate quantification of the parameters involved in the algorithms. Also, site parameters measured for the sample stand could have been in error and model parameters might not have been adequate for these sample sites. These parameters were taken from the literature and may not be applicable to the area or to the site where the test plot was located.

Sensitivity Analysis

A sensitivity analysis of FIRESUM was performed by increasing a selected parameter by 10 percent of its original value and executing the model while holding all other parameters constant. Computer costs and time constraints limited basal area predictions to the average from 30 simulation runs Kelcher and Axelrod 1954). Standard deviations of basal area averaged from 30 runs were below 0.5 m²/ha; small enough to discern the relative sensitivity of various parameters.

Results of the sensitivity analysis (table 12) agreed closely with those found by Kercher and Axelrod (1984). Maximum age for a tree species (*AGEMAX*) was clearly

Table 12—Results of the sensitivity analysis¹

Parameter		Percent change in PIPO basal area	
Symbol	Description	50 years	100 years
AGEMAX	Maximum age of species	-17.50	-18.10
WOODMAX	Maximum woody fuel loading	-1.41	-.89
SPM	Maximum stocking of seedlings	-1.03	-2.33
DBULK	Bulk density of duff-litter	+1.61	+3.78
WSO	Minimum AET:PET of a species	-7.25	-5.11
DMIN	Minimum number degree-days	-11.34	-7.37
DMAX	Maximum number degree-days	-1.65	+3.34
BARMAX	Maximum basal area	+10.01	+11.24
Dm	Maximum diameter	+9.98	+8.86
Hm	Maximum height	+5.01	+2.00
NYR	Years needles stay on tree	+.96	-1.04
DKL	Proportion of decay in litter	+.23	+.36
AINC	Minimum growth rate for mortality	-1.06	-3.11

¹Values in table are percentage change in ponderosa pine basal area when parameter listed in first column is increased by 10 percent. Sensitivity is measured at the 50th and 100th year of simulation and is calculated from the average of thirty simulation runs.

the most sensitive parameter measured, due to its presence in both the growth and mortality algorithms. In general, parameters directly related to the theoretical growth equation seemed to be the most crucial in FIRE-SUM. Parameters involved in the calculation of tree regeneration were also important.

An additional, and more extensive, sensitivity analysis was performed for some parameters used in the fire module (FIREMOD). In this analysis, three sets of fuel moisture values for each of three size classes of woody fuel were entered into the model to evaluate overall effect on plot basal area. This process was repeated for three duff moisture values. Results show that dry fuels resulted in an increase in the basal area of ponderosa pine (table 13), presumably because fires ignited in dry fuels tend to be hotter than those ignited in moist fuels. These hotter

fires apparently eliminated competing conifers and shrubs, thus allowing greater pine productivity. When duff moisture content was high, very little duff was removed by fire; this adversely affected regeneration of ponderosa pine, and to a lesser degree, Douglas-fir.

SUMMARY AND CONCLUSIONS

FIRESUM is similar to SILVA and many other JABOWA-type models in concept, but it is unique in construction. Related environmental components were integrated in FIRESUM so they depend on each other. Additional ecological processes such as woody fuel accumulation and duff depth-regeneration interaction were added to more completely simulate growing conditions in ponderosa pine/Douglas-fir ecosystems. The fuel and fire sub-modules were refined to more accurately predict fire behavior, and the regeneration algorithm was extensively modified to account for the role of site conditions in seedling mortality. Because site parameters in FIRESUM were stratified by habitat type groups (fire groups), many stands of differing species and site conditions may be modeled. Lastly, the FIRESUM program was modified by making fuel moisture and other site variables inputs to the program.

FIRESUM could be further modified to more accurately simulate ecological processes. The regeneration algorithm could be reworked to account for additional stochastic elements contributing to seedling establishment (Keane and others in press a, in press b). Cone crop size, seed dissemination, seed germination, and seed lost to birds and animals could be linked to weather and soil conditions. The fuel accumulation and decomposition algorithm could be improved. Currently, FIRESUM does not simulate accumulation and decomposition in woody, shrubby, and herbaceous fuels, as it does for litter and duff. Quantification of decomposition rates in all fuel components and linking the decomposition rates to climatic processes (for example, AET:PET ratio) would enhance the model's predictive value.

Table 13—Sensitivity analysis of fuel moisture values in FIRESUM

Moisture class	Duff moisture content	Ponderosa pine basal area (m ² /ha) ²		
		25 yr	50 yr	100 yr
DRY	0.25	24.42	21.85	15.03
MOIST	.25	23.91	22.43	16.72
WET	.25	22.83	23.37	17.62
DRY	.75	19.68	17.34	13.08
MOIST	.75	21.75	18.68	15.30
WET	.75	22.44	22.44	17.50
DRY	1.50	22.91	20.32	15.34
MOIST	1.50	19.77	21.74	16.37
WET	1.50	19.34	22.88	17.24

¹Fuel moisture contents are for woody fuel components only. The 1-, 10-, and 100-hour timelag moisture contents for the three moisture classes are: DRY (0.05, 0.05, 0.08), MOIST (0.12, 0.12, 0.16), and WET (0.19, 0.19, 0.24).

²Values are averages of ponderosa pine basal area from 30 simulation runs. Basal area was recorded for the 25th, 50th, and 100th year of simulation.

Another possible modification would be to develop a more intensive growth equation. The use of growth reduction factors may not allow sufficient resolution to accurately predict subtle changes in tree growth. The fire subroutines could also be modified to account for tree mortality due to crown fires or to root damage, duration of fire and its effect on tree mortality, vertical fire propagation, contribution of large fuels to fire intensity and tree mortality, and reduction of shrub and herbaceous fuels. Other changes might be to more intensively model the effect of soil fertility and water stress on tree growth, develop more accurate leaf area equations, link tree establishment and growth to understory shrub and herbaceous cover, and include off-site seed sources in the regeneration subroutine. Lastly, a wide range of stands with long-term measurements are needed to more accurately estimate the variability of model predictions.

With the addition or modification of subroutines, FIRESUM could be applied to a broad range of ecological problems in the Inland Northwest. One possible application is to assess the effect of climatic change on tree growth and fire intensity and frequency. Climatic input parameters could be modified using current models that simulate changes in temperature and precipitation over time. Changes in photosynthetic activity due to the "greenhouse effect," increased carbon dioxide, increased temperature, and decreased water availability, could be simulated by introducing another reduction factor in the growth algorithm. Climatic effects on fire frequency would have to be stochastically linked to the vegetation complex and site environment. FIRESUM might enable us to predict shifts in species composition and structure if the global climate is indeed changing as many scientists contend.

Another important application of FIRESUM is in increasing understanding of ecological processes. Such an understanding could ultimately aid natural resource management. For example, a land manager might wish to use FIRESUM to evaluate cumulative effects of different prescribed burning schedules on tree composition and structure. Other potential uses include assessment of insect- and disease-caused tree mortality related to fire frequency, prediction of stand productivity at varying fire frequencies, and evaluation of wildlife habitat potential under different fire regimes.

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APPENDIX A: LISTING OF THE FORTRAN77 COMPUTER CODE FOR THE MODEL/PROGRAM FIRESUM

```

PROGRAM FIRESUM
C ::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::
C      Model for simulation of western conifeous forests.          *
C This version was coded by Bob Keane, Quantitative Ecologist.    *
C Modifications and alterations to original SILVA were accomplished by *
C      Bob Keane                                                  *
C please contact Bob Keane for information on its use              *
C      Keane:                                                     *
C      PO Box 8089                                                *
C      USFS Fed. Bldg.                                           *
C      Missoula, MT 59806                                        *
C      406-329-3390                                              *
C      fts: 585-3390 OR 584-4867                                  *
C      com: 406-329-4837 or 406-329-3390                          *
C *****
C *****      FIRESUM: Keane version June 6, 1989      *****
C *****      Fire effects in Ponderosa pine-Douglas-fir stands*****
C *****      Fire effects in Whitebark pine forests  *****
C *****
C      FIRESUM coding is an extensive modification of jabowa
C      botkin et. al. j. ecol. 60:849-872 (1972).
C      *****
C      *****notice to users*****
C      SUBROUTINEs birth,dist,kill,cycles, and rings use the
C      random number generator rgen. this is called as XRANDOM,
C      where x is a returned array of random numbers between
C      0 and 1 and n is the number of returned values of x.
C      rgen and the seed generator ranst are at the END of the
C      deck. ranst is called once at the beginning of the job
C      to set the seed for rgen. the user should replace these
C      SUBROUTINEs with his own random number generator.
C      Input files should have names:tredat,sitdat,and contrl.
C      Unit numbers are: 1-tredat.dat,2-sitdat.dat,3-contrl.dat.
C      *****
C Modification of FIRESUM
C      Value of nj in birth rounded instead of trun
C      Polar method used to generate gauss r.v. in birth
C Corrections to SUBROUTINE site and input of tree water response
C      in SUBROUTINE tree
C      SUBROUTINE grow and birth modified for water stress
C      still use botkins thornthwaite method
C      this version has option of suppression effects of water stress
C      nwtstr = 1 water stress exists
C      0 no water stress, optimum growth
C This version prints out results in units of sq. m./ha. orsq.cm/sq.m.
C This version uses three scratch arrays and uses them in shade also.
C This version sets limit of 3000 trees.
C This version has been cleaned for sending to fws
C This version has fortran random number generator XRANDM,only
C      for export.
C This version is now ansi compatible for export.
C This version replaces rnfl in dist with rgen
C
C Dynamic Variables:
C AGE(j) - vector of tree ages (years)
C DBH(j) - vector of tree diameters (cm)
C OCCUR(j) - binary vector of fire years (0 or 1)
C DEGD - number of degree days for simulation plot.
C SLA(j) - vector of tree leaf areas (m2/m2)
C NTREES(i) - species vector for number of trees per species.

```


C NTREES(i) - species vector for number of trees per species. *
 C TABLE(j) - table of possible seed years for every species. *
 C S1(j),S2(j),S3(j) - working arrays for program execution. *
 C NDEAD(i) - number of dead trees per species. *
 C DDBH(j) - working vector for tree dbh. *
 C ABAR(j) - vector of basal areas for trees (m2/ha) *
 C PD(j) - probability of survival for each i tree. *
 C Input Variables: *
 C ASIDE(i) - allsided to projected leaf area conversion factor. *
 C C(7) - Coefficient in crown weight equations. *
 C ALPHA(7) - Coefficient in crown weight equations. *
 C B2(7) - calculated coefficient for height equation. *
 C B3(7) - calculated coefficient for height and growth equation. *
 C CEXT(8) - extinction factor for each fire group canopy. *
 C GRAT(7) - live crown ratio for each species. *
 C SIGMA(7) - parameter for converting crown weight to leaf area. *
 C AP(7) - alpha regression coefficient for *
 C BETAP(7) - beta regression coefficient for *
 C G(7) - calculated growth parameter for diameter increment. *
 C AGEMX(7) - maximum attainable age by species. *
 C DM(7) - maximum attainable diameter by species. *
 C HM(7) - maximum attainable height by species. *
 C SPM(8) - maximum attainable seedling stocking by fire group. *
 C XMBAR(8) - maximum attainable basal area by fire group. *
 C PHI - maximum relativized available light (=1.0) *
 C DMIN(7) - minimum number of degree days by species. *
 C DMAX(7) - maximum number of degree days by species. *
 C DOPT(7) - optimal number of degree days by species. *
 C BASET(12) - temperature by month (oC). *
 C BASEP(12) - precipitation by month (cm). *
 C BASEH - base elevation or elevational difference from w.s. to plot.*
 C ROCK - percent of exposed rock on plot. *
 C TILL - depth of soil in meters. *
 C TEXT - soil water holding capacity in mm/m. *
 C EXCESS - prop of precip that is runoff. *
 C PLTSIZ - area of simulation plot (m2). *
 C IFG - fire group number. *
 C SURA(7) - alpha coefficient for seedling survival equations. *
 C SURB(7) - beta coefficient for seedling survival equations. *
 C DBULK(8,2) - bulk density of litter and duff by fire group. *
 C ISHADE(7) - shade tolerance by species. *
 C IMOIST(7) - moisture tolerance by species. *
 C MEXT(2) - moisture of extinction by live or dead fuel class. *
 C RHOP(7) - fuel particle density for each fuel component. *
 C BULK(2,8) - bulk densities for live and dead fuel by fire group. *
 C MOIS(2,7) - moisture content of live and dead fuel components. *
 C MPS(2,7) - surface area to volume ratio for live and dead comp. *
 C LHV(2,7) - latent heat content of each fuel component. *
 C ST(2,7) - fraction mineral content of dead fuel. *
 C SE(2,7) - fraction mineral content of fuel excluding silica. *
 C DKD(7),DKL(7),DKF(7),LTD(7) - decomposition proportions for litter.*
 C ABM(7),FFL(7) - parameters quantifying litterfall loadings. *
 C DMOIST - duff moisture content. *
 C NS - number of species. *
 C NSPAN - time span (in years) to simulate. *
 C NRUNS - number of times to repeat each simulation time span. *
 C CLRCUT - flag indicating if stand originated as a clearcut. *
 C NWRSTR - flag indicating if water stress factors are included. *
 C IFIRE - number of years between fires (fire interval). *
 C SBURN - proportion of burnable live shrubs. *

```

C BC(7) - bark thickness conversion factor by species. *
C D1(7),D2(7),D3(7) - coefficients in fire mortality equation. *
C FWG(2,7) - working array for fuel loadings by component. *
C WOOD(3) - woody fuel loading by size class 1,10,100 hr. *
C NDYR(7) - number years needles stay on tree of species i. *
C CROP(7) - number of years between good cone crops. *
C CBLOCK(7) - number of years before a good cone crop can occur. *
C GRWS(7) - growth reduction from water stress. *
C GRF(7) - growth reduction from pollution. *
C This program calls 45 subroutines and 3 functions, consists of about *
C 3000 lines of code, and is written in FORTRAN 77. *
C *****
common/leaf/aside(7),c(7),alpha(7),b2(7),b3(7),cext(8),crat(7),
&
sigma(7),ap(7),betap(7)
common/trunk/g(7),agemx(7),dm(7),hm(7),spm(8),ysc(7)
common/hdata/phi,xmbar(8),degd,ainc(7),binfest(8),ibcycle(8),brr
common/climat/ dmin(7),dopt(7),dmax(7),baset(12),basep(12),baseh
common/water/grws(7),ws0(7),wsm(7),nws(7),wr,grdd(7),grbar(7)
common/plotq/elev,rock,till,soilm,text,excess,pltsiz,ifg
common/birthk/sura(7),surb(7),dbulk(8,2),disequ(2,7),rdelay(8)
common/types/ishade(7),imoist(7),spp(7)
common/wbark/ cmax,agecon,dbhmin,birds,spc,spcac,cyr(4),fmax,cpt,
&
pfind,ssc
common/fuel1/ mext(2),rhop(2,7),bulk(2,8),mois(2,7)
common/fuel2/ mps(2,7),lhv(2,7),st(2,7),se(2,7)
common/fuel3/ dkl(7),dkd(7),dkf(7),ltd(7)
common/fuel4/ abm(7),ffl(7),fyr(3,8),fload(3,8)
common/fuel5/ amc(7),bmc(7),cmc(7),dmc(7),mmc(7),tmc,emc(7)
common/cfire/cbd(7),vfl(7),cfmc(7),vfmc(7),cflm(7),csvr(7),
&
vsvr(7),bl(7)
common/sites/ occur(500),rh,wind,ttheta,t
common/mort/ dl(7),d2(7),d3(7),bc(7)
common/polut/ndyr(7),dmoist
common/oper/ ns,nspan,nruns,clrcut,nwrstr,ifire,sburn,ibr,impb
common/init/ ntrees0(7),dbh0(4000),ncount(20,7),nbins,width,
&
age0(4000),agein(20,7)
common/limits/ mxtrs,maxspc,mxdd,mxyrs,maxbin
real mext,lhv,mmc,mps,ltd,mois,emc,cyr
real dbh(4000),sla(4000),pd(4000),fwg(2,7),wood(3),ptree(7),
&
dsw(7),dsize(7)
real sl(4000),s2(4000),s3(4000),crop(7)
real grf(7),area(4500),abar(4500),age(4000)
integer table(4500),ntrees(7),ndead(7),cblock(7),clrcut,occur
integer fyr,itop(4000)
character*1 ishade,imoist,spp*4

open(unit=5,file='OUTFILE.DAT',form='formatted',recl=150,
&
pad='yes')

nl = 2
npine = 0
lag = 0
branch = 0.0
iseed = 0
icwf = 0

C ..... Call to initialize random number generator user should
C ..... introduces his own random number generator
xran = rrand()

```

```

call sitdta
call tree(nl,crop,cblock)
call calcnt
call cntrl(dsize,dimax,dimin)
call dist(s1,itop)
nyears= nspan
nsp= ns
do 5 i = 1,ns
    dsw(i) = 0.0
    if(dsize(i) .lt. 0.0) dsw(i) = abs(dsize(i))
    if(dsize(i) .gt. 0.0) dsw(i) = sqrt(5000.0*dsize(i)*3.14159)
5 continue

call site

close(5)

open(unit=8,file='WOOD.DAT',pad='yes',recl=80)
open(unit=9,file='BRUSH.DAT',pad='yes',recl=80)
open(unit=11,file='FIRE.DAT',pad='yes',recl=80)
open(unit=12,file='DUFF.DAT',pad='yes',recl=100)

do 10 i = 1,nruns
    irun = i
    if(irun .eq. 2) then
        close(8)
        close(9)
        close(11)
        close(12)
    endif
    print *, 'FIRESUM run number: ', i
    iseed = 0
    call cycles(table,nyears,nsp,s1,crop,cblock)
    call rings(nyears,s1)
    call starter(ntrees,dbh,age)
    do 20 k = 1,nspan
        kyr = k
        call birth(ntrees,dbh,age,s1,s2,table,nyears,kyr,duff,
&                irun,itop,dsw,ccrop,lag,iseed,ptree)
        call pollut(grf,kyr)
        call grow(dbh,pd,ntrees,sla,grf,s1,s2,s3,age,kyr,itop,
&                inend,npine)
        call fire(ntrees,dbh,fwg,nl,pd,kyr,duff,branch,wood,
&                irun,icwf,dimax,dimin)
        if(icwf .eq. 1) iseed = 1
        call kill(ntrees,ndead,dbh,pd,s1,age,branch,itop,
&                icwf)
        call basal(ntrees,dbh,kyr,nyears,area)
        if(icwf .eq. 1) then
            lag = kyr + ifix(rdelay(iffg))
        endif
20    continue
        nm= nspan*ns
        call avg(area,abar,nm)
10 continue

C ..... printing annual basal area projections
call output(abar,nyears)

stop

```

```

END
BLOCKDATA
C *****
C BLOCK DATA FOR SIMULATION RUN SPECIFICS
C   These numbers set operating limits on model:
C   mxtrs..... maximum number of trees allowed on the stand
C   mxysr..... max number of years in one "run" of the model
C   maxbin..... max num of diam cohorts in initial dist of tree sizes
C   maxspc..... max number of tree species
C   mxysr..... maximum number of years the model may run
C *****
   common/limits/ mxtrs,maxspc,mxdd,mxysr,maxbin

   data mxtrs/4000/
   data mxdd/4000/
   data mxysr/500/
   data maxbin/20/
   data maxspc/7/

END
SUBROUTINE add(x,nx,xnew,new,k)
C *****
C This subroutine adds new trees to the DBH array (x(i,j)) in the
C appropriate species and DBH slots. This subroutine is called from
C BIRTH and adds seedlings 137 cm tall and 1.0 cm diameter.
C *****
   common/oper/ ns,nspan,nruns,clrcut,nwrstr,ifire,sburn,ibr,impb
   integer clrcut
   dimension x(1),nx(1),xnew(1)

C ..... Add the elements of xnew to x after species k
C ..... nx array is not updated
   if (new.eq.0) return
   n= isum(nx,ns)
   kk= isum(nx,k)
   nkk= n-kk
   if (nkk.eq.0) go to 15
   do 10 j= 1,nkk
       x(n+new-j+1)= x(n-j+1)
10 continue
15 continue
   do 20 j= 1,new
       x(kk+j)= xnew(j)
20 continue

   return
END
SUBROUTINE avg(x,xbar,n)
C *****
C This subroutine averages the annual estimates of basal area for
C every run. This is a running average and variance is not computed.
C *****
   dimension x(1),xbar(1)
   integer count
   data count/0/

   count= count+1
   w1= float(count-1)/float(count)
   w2= 1./float(count)

```

```

C ..... Estimate the average and include in array
  do 10 i= 1,n
    xbar(i)= w1*xbar(i)+w2*x(i)
  10 continue
  return
  END
  SUBROUTINE basal(ntrees,dbh,kyr,nyears,area)
C *****
C * Subroutine basal keeps a continous account of species basal *
C * area by simulation year. These values are stored in working *
C * array AREA(i,j) to be printed in subroutine OUTPUT. *
C *****
  common/plotq/elev,rock,till,soilm,text,excess,pltsiz,ifg
  common/oper/ ns,nspan,nruns,clrcut,nwrstr,ifire,sburn,ibr,impb
  integer clrcut
  dimension ntrees(1),dbh(1),area(nyears,1)
  data pi/3.141592654/

  do 10 k= 1,ns
    nk= ntrees(k)
    area(kyr,k)= 0.
    if (nk.eq.0) go to 10
    if(k .eq. 1) then
      jj = 0
    else
      jj= isum(ntrees,k-1)
    endif
    do 20 j= 1,nk
      area(kyr,k)= area(kyr,k)+dbh(j+jj)**2.0
    20 continue

C ..... Compute the basal area for the plot in meters square
  area(kyr,k)=area(kyr,k)*pi/(4.*pltsiz)
  10 continue
  return
  END
  SUBROUTINE beetle(SPP,DIA,AGE,PROB)
C *****
C This subroutine simulates tree mortality if tree is infested with *
C bark beetles. The current functions are from data collected from *
C the gallatin by Region 1 personnel - contact Ammens Ogden *
C *****
  character spp*4

C ..... Compute the probability of mortality by species
  if(spp .eq. 'pial') then
    prob = ((0.7664 * dia) - 0.2222) / 100.0
    if(prob .lt. 0.0) prob = 0.0
    if(prob .gt. 1.0) prob = 1.0
  elseif(spp .eq. 'pico') then
    if(dia .lt. 46.0 .and. age .lt. 150.0) then
      prob = (0.555 * dia) / 100.0
    else
      prob = 0.10
    endif
  elseif(spp .eq. 'pipo' .or. spp .eq. 'pimo') then
    if(dia .lt. 46.0) then
      prob = (0.555 * dia) / 100.0
    else
      prob = 0.10
  
```

```

        endif
    else
        prob = 1.0
    endif
    return
END
SUBROUTINE birth(ntrees,dbh,age,ds,agnw,table,nyears,kyr,duff,
&             irun,itop,dsw,ccrop,lag,iseed,ptree)
C ::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::
C This subroutine adds new trees to plot based on climatic constraints
C (degree-days,available water,cone crop) and site factors (shading and
C duff depth). Tree incursion is at 8 years and 1 cm dbh.
C
C   spm(j) ..... max number of new seedlings per meter for all species
C   fnj(j) ..... number of seedlings established onsite.
C   psur ..... percent survival calculated from duff depth (Boyce 86)
C   dsw ..... distance to seed wall in meters
C ::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::
    real dbh(1),ds(1),agnw(1),age(1),ptree(7)
    real u(2),dsbar(7),sigds(7),sregen(7),dsw(7)
    integer clrcut,table(nyears,1),ntrees(1),itop(1)
    character*1 ishade,imoist,spp*4
    common/oper/ ns,nspan,nruns,clrcut,nwrstr,ifire,sburn,ibr,impb
    common/limits/ mxtrs,maxspc,mxdd,mxyrs,maxbin
    common/water/grws(7),ws0(7),wsm(7),nws(7),wr,grdd(7),grbar(7)
    common/leaf/aside(7),c(7),alpha(7),b2(7),b3(7),cext(8),crat(7),
&             sigma(7),ap(7),betap(7)
    common/trunk/g(7),agemx(7),dm(7),hm(7),spm(8),ysc(7)
    common/climat/ dmin(7),dopt(7),dmax(7),baset(12),basep(12),baseh
    common/hdata/phi,xmbar(8),degd,ainc(7),binfest(8),ibcycle(8),brr
    common/birthk/sura(7),surb(7),dbulk(8,2),disequ(2,7),rdelay(8)
    common/plotq/elev,rock,till,soilm,text,excess,pltsiz,ifg
    common/types/ishade(7),imoist(7),spp(7)
    data dsbar/7*.5/,sigds/7*0.1/,no/0/

C ..... Initialize important variables
    if(kyr .eq. 1) duff = 1.5
    do 5 i = 1,ns
        sregen(i) = 0.0
    5 continue
    cones = 0.0
    seedlng = spm(ifg)
    fnjsum = 0.0
    dred = 1.0

C ..... Delay regeneration for interval based on fire group
    if(lag .gt. kyr) then
        go to 200
    endif

C ..... Start the regeneration process for each species
    do 100 j= 1,ns
        nj= 0
        sla= 0.

C ..... Climatic and cone crop tests
        if (table(kyr,j) .eq. no) go to 100
        if (degd .lt. dmin(j)) go to 100
        if (degd .gt. dmax(j)) go to 100
        if (grws(j) .le. 0.0) go to 100

```

```

        if (wr .lt. ws0(j))          go to 100
C .....Seedlings to be established. Reduction factors now calculated
    psur = (sura(j) - surb(j) * duff) / sura(j)
    if(psur .lt. 0.0) psur = 0.0
    totsla = 0.0
    totree = 0.0
    do 10 ii = 1,ns
        if(lag+ysc(ii) .lt. kyr) iseed = 0
        if(iseed .eq. 0) ptree(ii) = 0.0
10    continue
    do 20 kk= 1, ns
        nkk= ntrees(kk)
        if (nkk.eq.0) go to 20
        kkkk = kk - 1
        kkk = kk
        if(kk .eq. 1) then
            ikk = 0
        else
            ikk= isum(ntrees, kkkk)
        endif
        call needle(sla, ikk, nkk, dbh, kkk, wgt, pltsiz)
        totsla = totsla + sla
C ..... Calculation of proportion of seed trees
    do 15 ii = 1, nkk
        if((dbh(ii+ikk) .gt. 10.0 .or. age(ii+ikk) .ge.
&        ysc(kk)) .and. iseed .eq. 0) then
            ptree(kk) = ptree(kk) + 1.0
            totree = totree + 1.0
        endif
15    continue
20    continue
C ..... Adjustment for off-site seeding, and then the seedling equation
    if(iseed .eq. 0) then
        if(totree .gt. 0.0)    ptree(j) = ptree(j) / totree
        if(totree .le. 0.0)    ptree(j) = 0.05
        if(ptree(j) .lt. 0.05) ptree(j) = 0.05
    endif
C ..... Calculation of whitebark pine seedlings if species present
    if(spp(j) .eq. 'pial') then
        call pinalb(fnj, totsla, dbh, age, ntrees, itop, ccrop, cones)
        seedlng = seedlng - (fnj / pltsiz)
        if(seedlng .le. 0.0) seedlng = 0.1
    endif
C ..... Reduction of seedling due to distance from seed source
30    dred = 1.0
    if(dsw(j) .gt. 20) then
        if(ptree(j) .le. 0.01) then
            if(spp(j) .eq. 'pial') then
                xdists = dsw(j) - 20.0
                if(xdists .le. 0.0) xdists = 0.0
                dred = 10.0**(-0.8062-(0.000454*xdists)) /
&                0.1563
            else
                if(dred .lt. 0.0001) dred = 0.0001
            endif
            xdists = (dsw(j) - 20.0) * 3.2808

```

```

                                xmax = abs(disequ(1,j) / disequ(2,j)) / 3.28
                                if(xdist .le. 0.0) xdist = 0.0
                                if(xmax .gt. xdist) then
&                                  dred = exp(disequ(1,j) + disequ(2,j)
                                              * xdist) / exp(disequ(1,j))
                                              if(dred .lt. 0.00001) dred = 0.00001
                                else
                                  dred = 0.00001
                                endif
                                endif
                                endif
                                endif
                                endif
                                endif
C ..... Calculation of number of seedlings for species j
                                if(spp(j) .ne. 'pial') then
                                  fnj = seedlng * pltsiz * psur * ptree(j) * dred
                                else
                                  fnj = seedlng * dred
                                endif
C ..... Reduction for shading effects by tolerance class
                                if(ishade(j) .eq. 'I') fnj=fnj * exp(-0.8*totsla)
                                if(ishade(j) .eq. 'M') fnj=fnj * exp(-0.25*(totsla+1.0))
                                if(ishade(j) .eq. 'T') fnj=fnj * (1.0-exp(-0.25*(totsla+0.2)))
C ..... Final calculation of number established seedlings
                                ntot= isum(ntrees,ns)
                                xred = (1.0 - (float(ntot) / float(mxtrs)))
                                if(fnj .gt. 100.0) fnj = 100.0
                                fnj = fnj * xred
                                sregen(j) = fnj
                                fnjsum = fnjsum + fnj
                                nj= int(fnj+.5)
                                if(nj.eq.0) go to 100
C ..... Check to see if number of trees has not exceeded maximum
                                if (ntot+nj.gt.mxtrs) call error(9)
C ..... Calculate a random diameter for each of the nj seedlings
                                do 40 i= 1,nj
                                  hsbar= b2(j)*dsbar(j)-b3(j)*dsbar(j)**2-b3(j)*sigds(j)**2
                                  sighs= (b2(j)-2.*b3(j)*dsbar(j))*sigds(j)
45                                  call rgen(u,2)
                                  u(1)= 2.*u(1)-1.
                                  u(2)= 2.*u(2)-1.
                                  s= u(1)**2+u(2)**2
                                  if (s.ge.1) go to 45
                                  z= u(1)*sqrt(-2.*alog(s)/s)
                                  hs= sighs*z+hsbar
                                  if (hs.lt.0.) go to 45
                                  ds(i)= (b2(j)/(2.*b3(j)))*
&                                     (1.-sqrt(1.-4.*(b3(j)/b2(j)**2)*hs))
                                40 continue
C ..... Place the seedling in appropriate cell in DBH and AGE array.
                                ij = j
                                call add(dbh,ntrees,ds,nj,ij)
                                do 50 k= 1,nj
                                  agnw(k)= rdelay(ifg)
                                50 continue

```



```

        call add(age,ntrees,agnw,nj,ijj)
C ..... Put zero into the blister rust array ITOP
        n= isum(ntrees,ns)
        kk= isum(ntrees,ijj)
        nkk= n-kk
        if (nkk.eq.0) go to 65
        do 60 i= 1,nkk
            itop(n+nj-i+1)= itop(n-i+1)
60         continue
65         do 70 i= 1,nj
            itop(kk+i)= 0
            if(spp(j) .eq. 'pial' .or. spp(j) .eq. 'pimo') then
                rnum = rnd()
                if(rnum .lt. brr) itop(kk+i) = 2
            endif
70         continue
            ntrees(j)= ntrees(j)+nj
100        continue

C ..... Writing important regeneration variable values to external file
200        if(irun .eq. 1) then
            write(12,1000) duff,totsla,fnjsum,(sregen(i),i=1,ns),cones
1000        format(20f8.2)
            endif
            return
            END
            SUBROUTINE brnoff(ln,dn,wood)
C .....
C      compute litter and duff and woody fuel burnoff on stand
C      based on equations in Brown and others (1985).
C      All litter is burned off and then fractions of duff, and the
C      three fuel types are also burned off.
C      all loadings in units of kilograms per square meters
C      wood(3)..... kg/m2 for each fuel type 1,10,100 hr.
C      dn(k) ..... biomass loading of k'th duff component
C      ln(k) ..... biomass loading of k'th litter component
C      pduff..... fract by which amount of duff decreases
C .....
        common/oper/ ns,nspan,nruns,clrcut,nwrstr,ifire,sburn,ibr,impb
        common/polut/ndyr(7),dmoist
        real ln(1),dn(1),pduff,wood(3)
        integer clrcut
        data da/83.70/,db/-0.426/

C.....
C      compute total loading and average moisture content
C.....
        pduff = (da+db*dmoist*100.0)/100.0
        if(pduff .lt. 0.0) pduff = 0.0
        do 10 i = 1,ns
            ln(i) = 0.0
            dn(i) = dn(i)*pduff
10        continue

C.....
C      calculation of woody fuel reductions from brown et al equations
C.....
        do 20 i = 1,3
            if(i .le. 2) then
                conwood = 0.890 * wood(i)

```

```

        else
            conwood = 0.845 * wood(i)
        endif
        if(conwood .lt. 0.0) conwood = 0.0
        wood(i) = wood(i) - conwood
20 continue
return
END
SUBROUTINE brush(dbh,ntrees,bbm1,bbm2,init)
C ::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::
C This subroutine computes shrub and herbaceous fuel loadings :
C for the simulation plot. The carrying capacity formula uses: :
C x01,x1,x02,x2 indicate live brushy fuel both tol and intol :
C g01,g1,g02,g2 indicate live grass and forb fuel both tol-intol :
C b,dd,a,cc are coefficients to the biomass equation.
C ::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::
common/leaf/aside(7),c(7),alpha(7),b2(7),b3(7),cext(8),crat(7),
&      sigma(7),ap(7),betap(7)
common/plotq/elev,rock,till,soilm,text,excess,pltsiz,ifg
common/trunk/g(7),agemx(7),dm(7),hm(7),spm(8),ysc(7)
common/hdata/phi,xmbar(8),degd,ainc(7),binfest(8),ibcycle(8),brr
common/oper/ ns,nspan,nruns,clrcut,nwrstr,ifire,sburn,ibr,impb
integer clrcut
dimension ntrees(1),dbh(1),b(8),dd(8)
integer yes,no
data yes/1/,no/0/
data b /0.02700,0.04600,0.08605,0.07600,0.06900,0.07000,
&      0.01598,0.05437/
data dd /0.02934,0.1190,0.04816,0.04300,0.10125,0.10143,
&      0.14224,0.19690/
data x01,x02,g01,g02 /0.0137,0.0137,0.0010,0.0010/
data a/1.1398/,cc/10.8644/

C ..... Inline function statements for the carrying capacity formula
r1(y)= 1.-exp(-2.32*(y-.05+abs(y-.05)))
r2(y)= 2.24*(1.-exp(-.568*(y-.08+abs(y-.08))))
delta(y)= y * a * (1.0 - (y/b(ifg)))
gdelta(y) = y * cc * (1.0 - (y/dd(ifg)))

C ..... Setting initial conditions after a fire of any intensity
if (init.eq.yes) then
    x1= x1 * (1.0 - sburn)
    x2= x2 * (1.0 - sburn)
    if(x1 .eq. 0.0) x1 = x01
    if(x2 .eq. 0.0) x2 = x02
    g1 = g01
    g2 = g02
endif
if (ns.eq.0) return

C ..... Summing up all trees and calculating leaf area index for stand
sla= 0.
do 10 k= 1,ns
    kk = k
    nk= ntrees(k)
    if (nk.eq.0) go to 10
    if(kk .eq. 1) then
        jj = 0
    else
        jj= isum(ntrees,kk-1)

```

```

endif
    call needle(tla,jj,nk,dbh,kk,wgt,pltsiz)
    sla = sla + tla
10 continue

C ..... Calculating all biomass reduction factors for shading effects
al= phi*exp(-cext(ifg)*sla)

C ..... Calculating current biomass on the simulation plot
x1 = x1 + r1(al) * delta(x1)
x2 = x2 + r2(al) * delta(x2)
g1 = g1 + r1(al) * gdelta(g1)
g2 = g2 + r2(al) * gdelta(g2)
if(g1 .gt. dd(ifg)) g1 = dd(ifg)
if(g2 .gt. dd(ifg)) g2 = dd(ifg)
bbm1= (x1+x2)/2.
bbm2= (g1+g2)/2.
init= no
return
END
SUBROUTINE calcnt
C *****
C * Subroutine calcnt calculates all parameters for growth equation *
C * from data in external file TREE.DAT. Intermediate values are *
C * first calculated based on maximum height, age, and diameter. *
C * Calculated parameters are then printed in external file OUTPUT. *
C *****

    common/leaf/aside(7),c(7),alpha(7),b2(7),b3(7),cext(8),crat(7),
&      sigma(7),ap(7),betap(7)
    common/trunk/g(7),agemx(7),dm(7),hm(7),spm(8),ysc(7)
    common/plotq/elev,rock,till,soilm,text,excess,pltsiz,ifg
    common/oper/ ns,nspan,nruns,clrcut,nwrstr,ifire,sburn,ibr,impb
    integer clrcut
    character name*10

C ..... Calculation of intermediate terms in growth equation
do 10 j=1,ns
    a= 1.-137./hm(j)
    term1= alog(2.*(2.*dm(j)-1.))
    term2= (a/2.)*alog((9./4.+a/2.)/(4.*dm(j)**2+2.*a*dm(j)-a))
    term3= (a+a**2/2.)/sqrt(a**2+4.*a)
    term4= 3.+a-sqrt(a**2+4.*a)
    term5= 4.*dm(j)+a+sqrt(a**2+4.*a)
    term6= 4.*dm(j)+a-sqrt(a**2+4.*a)
    term7= 4.*hm(j)/agemx(j)
    term8= 3.+a+sqrt(a**2+4.*a)
    g(j)= term7*(term1+term2-term3*alog((term4*term5)/
1      (term6*term8)))
    b2(j)= 2.*(hm(j)-137.)/dm(j)
    b3(j)= (hm(j)-137.)/dm(j)**2
10 continue

C ..... Writing intermediate results to external files
write(5,1000)
name= 'g'
write(5,2000) name, (g(j),j=1,ns)
name= 'b2'
write(5,2000) name, (b2(j),j=1,ns)
name= 'b3'

```

```

        write(5,2000) name, (b3(j),j=1,ns)
        name= 'c
        write(5,3000) name, (c(j),j=1,ns)
        return

C ##### FORMATS #####
1000 format(/lh ,32x,'*derived constants*',/)
2000 format(lh ,a10,7f10.3)
3000 format(lh ,a10,7f10.7)
      END
      SUBROUTINE cntrl(dsize,dimax,dimin)
C *****
C This subroutine: *
C   reads operating parameters and initial distribution of tree diameters. *
C Variables are: *
C   nsum..... total number of trees initially on the stand *
C   nspan..... number of years per run of the model *
C   nruns..... number of runs of the model *
C   nbins..... number of diameter cohorts for initial state *
C   width..... width in cm for each diameter cohort *
C   dbh0(j)..... vector of initial tree diameters in cm *
C   ntrees0(j).. number of trees initially in the j'th species *
C   ncount(i,j).. number trees init in i'th diam cohort for j'th species *
C *****
      common/oper/ ns,nspan,nruns,clrcut,nwrstr,ifire,sburn,ibr,impb
      common/init/ ntrees0(7),dbh0(4000),ncount(20,7),nbins,width
      l ,age0(4000),agein(20,7)
      common/limits/ mxtrs,maxspc,mxdd,mxyrs,maxbin
      real dsize(7)
      integer clrcut,yes,agein
      character*10 name
      data yes/l/

      open(unit=4,file='CONTRL.DAT',form='formatted',recl=150,
&        pad='yes')

C ..... Reading in simulation specifics, then writing the input to file
      read(4,1000) name,nspan
      write(5,1000) name,nspan
      read(4,1000) name,nruns
      write(5,1000) name,nruns
      read(4,1000) name,clrcut,dimax,dimin
      write(5,1000) name,clrcut,dimax,dimin
      read(4,1000) name,ifire
      write(5,1000) name,ifire
      read(4,1000) name,ibr
      write(5,1000) name,ibr
      read(4,1000) name,impb
      write(5,1000) name,impb
      read(4,4000) name,(dsize(j),j=1,ns)
      write(5,4000) name,(dsize(j),j=1,ns)
      read(4,1000) name,nwrstr
      write(5,1000) name,nwrstr
      read(4,1000) name,nbins
      write(5,1000) name,nbins
      read(4,2000) name,width
      write(5,2000) name,width
C   if (nbins.gt.maxbin) call error(4)
C   if (nspan.gt.mxyrs) call error(5)
      do 10 i= 1,nbins

```

```

        read(4,3000) name,(ncount(i,j),j=1,ns)
        write(5,3000) name,(ncount(i,j),j=1,ns)
10 continue
    do 20 i=1,nbins
        read(4,3000) name, (agein(i,j),j=1,ns)
        write(5,3000)name, (agein(i,j),j=1,ns)
20 continue
    nsum= 0
    do 30 i= 1,nbins
        do 40 j= 1,ns
            nsum= nsum+ncount(i,j)
40 continue
30 continue
    if (nsum.gt.mxtrs) call error(6)
    rewind 4
    close(4)
    return

C ##### Formats #####
1000 format(a10,i6,f10.2,f10.2)
2000 format(a10,f6.1)
3000 format(a10,7i6)
4000 format(a10,7f7.1)
END
SUBROUTINE crown(ntrees,dbh,ros,byram,flame,fzone,icwf)
dimension dbh(1),ntrees(1)
    icwf = 0
    return
END
SUBROUTINE cycles(x,n,m,u,p,r)
C *****
C This subroutine assigns cone crop years from species-specific prob- *
C abilities for having a good cone crop. A uniform random number gen- *
C erator is used (XRANDOM) and is called from subroutine RGEN. *
C Variables used: *
C X(i,j): binary array storing appropriate classes of cone crops *
C P(i): probability of a good cone crop for species i. *
C R(i): number of years to block after a good cone crop for spp i. *
C U(i): temporary storage array. *
C *****
    integer x(n,m),r(7)
    real u(1),ul(1),p(7)
    if (n.eq.0.or.m.eq.0) return

C ..... Initializing cone crop array
    do 10 i= 1,n
        do 20 j= 1,m
            x(i,j)= 0
20 continue
10 continue

C ..... Calculating probabilities for blocked and unblocked states
    do 50 j= 1,m
        i= 0
        if (r(j).eq.1) go to 30

C ..... Calculate pnb, prob of an unblocked state
    pnb= 1./(p(j)*float(r(j)-1))
    call rgen(ul,1)
    if (ul(1).le.pnb) go to 30

```

```

C ..... Select an integer b at random from 1,2,3,... r-1
      call rgen(u1,1)
      i= int(float(r(j)-1)*u1(1))+1
30    call rgen(u,n)
40    i= i+1
      if (i.gt.n) go to 50
      if (u(i).gt.p(j)) go to 40
      x(i,j)= 1
      i= i+r(j)-1
      go to 40
50  continue
      return
      END
      SUBROUTINE dist(u,itop)
C *****
C This subroutine calculates initial distribution of tree diameters.      *
C - if clearcut option is specified set initial diameter vector to zero. *
C Trees are distributed randomly (ie. uniform pdf) within a diam cohort *
C Variables are: *
C nbins..... number of diameter cohorts for initial state *
C width..... width in cm for each diameter cohort *
C dbh0(j)..... vector of initial tree diameters in cm *
C ntrees0(j)... number of trees initially in the j'th species *
C ncount(i,j).. number trees init in i'th diam cohort, j'th species *
C clrcut..... flag to specify clear cut option *
C *****
      common/oper/ ns,nspan,nruns,clrcut,nwrstr,ifire,sburn,ibr,impb
      common/init/ ntrees0(7),dbh0(4000),ncount(20,7),nbins,width,
      & age0(4000),agein(20,7)
      common/limits/ mxtrs,maxspc,mxdd,mxyrs,maxbin
      integer clrcut,yes,agein
      dimension u(1),itop(1)
      data yes/1/

C ..... Initialize appropriate arrays
      do 5 i= 1,ns
          ntrees0(i)= 0
5      continue

      do 8 i= 1,mxtrs
          dbh0(i)= 0.0
          age0(i)= 0.0
          itop(i) = 0
8      continue

C ..... Assign each tree diameter and age to appropriate cell in each
C ..... array (DBH and AGE)
      kk= 0
      do 10 j= 1,ns
          do 20 i= 1,nbins
              n= ncount(i,j)
              ntrees0(j)= ntrees0(j)+n
              if (n.eq.0) go to 20
              call rgen(u,n)
              do 30 k= 1,n
                  dbh0(kk+k)= width*(u(k)+i-1)
                  age0(kk+k)= float(agein(i,j))
30          continue
              kk= kk+n
          
```

```

20  continue
10  continue
    return
    END
    SUBROUTINE error(fmt)
C *****
C This subroutine terminates program and send message to terminal. *
C *****
    integer fmt
    character*50 msg(12)
    data msg /' N1 is greater than N2 .           ',
1      ' N1 is greater than MID.                 ',
2      ' MID is greater than N2.                 ',
3      ' Too many diameter cohorts.              ',
4      ' Time span is too large, redo control file. ',
5      ' Initial distribution has too many trees. ',
6      ' Too many species in TREDAT, redo file.   ',
7      ' No end-of-species marker, fix TREDAT file. ',
8      ' Too many trees in BIRTH.                ',
9      ' Too many dead trees in KILL.            ',
1     ' DINC is greater than 5.0 cm, abnormal.   ',
2     '                                           '/

C ..... Print appropriate error message
    write(5,1000) msg(fmt)
1000 format(/1H ,a50)
    stop
    END
    SUBROUTINE fire(ntrees,dbh,fwg,nl,p,yr,duff,branch,wood,
&      irun,icwf,dimax,dimin)
C *****
C This subroutine is a sub-driver for all components used to calculate fire *
C intensity. Subroutine logic is as follows: *
C 1. Update fuel loadings: call subroutine FUEL *
C 2. Compute if current simulation year is a fire year, if not RETURN *
C 3. Assign fuel loadings into appropriate array TFWG(i,j). *
C 4. Compute fire intensity: call FIREMOD. *
C 5. Compute scorch height and resultant tree mortality: call INJURY *
C 6. Compute fuel consumption: call BRNOFF *
C 7. Compute duff and litter depth. *
C Important variables are: *
C TFWG(i,j)- fuel loadings for live and dead fuel components, *
C DUFF- duff and litter depth in cms, *
C Computed intensity and scorch height are written to external file. *
C *****
    common/oper/ ns,nspan,nruns,clrcut,nwrstr,ifire,sburn,ibr,impb
    common/leaf/aside(7),c(7),alpha(7),b2(7),b3(7),cext(8),crat(7),
&      sigma(7),ap(7),betap(7)
    common/plotq/elev,rock,till,soilm,text,excess,pltsiz,ifg
    common/polut/ndyr(7),dmoist
    common/birthk/sura(7),surb(7),dbulk(8,2),disequ(2,7),rdelay(8)
    common/sites/ occur(500),rh,wind,ttheta,t
    common/fuel1/ mext(2),rhop(2,7),tbulk(2,8),mois(2,7)
    common/fuel2/ mps(2,7),lhv(2,7),st(2,7),se(2,7)
    common/fuel5/ amc(7),bmc(7),cmc(7),dmc(7),mmc(7),tmc,emc(7)
    common/mort/ d1(7),d2(7),d3(7),bc(7)
    dimension ntrees(1),dbh(1),p(1),fwg(2,7),tfwg(2,7)
    real ln(7),ln1(7),dn(7),dnl(7),wood(3),lw,mois,hs
    integer flag(3),yr,yes,no,occur,clrcut
    data yes/1/,no/0/

```

```

data ln1/7*0./,dnl/7*0./
data init/1/

C ..... Initialization of parameters
icwf = 0
duff1 = 0.0
duff2 = 0.0
lw = 0.0
n= isum(ntrees,ns)
if (n.eq.0) return

C ..... Decide if current year is a clearcut year
if(clrcut .eq. yr) then
  do 10 i = 1,n
    if(dbh(i) .ge. dmin .and. dbh(i) .le. dmax) then
      p(i) = 0.99999
    endif
  10 continue
  go to 30
endif

C ..... Update fuel components, including litter and duff.
call fuel(ntrees,dbh,fwg,ln,ln1,dn,dnl,wood,yr,init,irun,
&         branch,icwf)

C ..... Decide if current year is a fire year.
if (occur(yr).eq.no) go to 30

C ..... Putting the five dead fuel types into temporary array
C ..... tfwg(i,j) types are litter, 1 hour, 10, and 100 hour woody,
C ..... and cured grass and last dead shrub.
do 15 i = 1,ns
  lw = lw + ln(i)
  tfwg(1,i) = 0.0
15 continue
  tfwg(1,1) = lw
do 16 i = 1,3
  tfwg(1,i+1) = wood(i)
16 continue
  tfwg(1,5) = fwg(1,5)
  tfwg(1,6) = fwg(1,6)
  tfwg(1,7) = 0.0
do 17 i = 1,2
  tfwg(2,i) = fwg(2,i)
17 continue

C ..... Simulating a fire by calling FIREMOD
call firemd(nl,tfwg,byram,flag,ifg,rate,flame,fzone)

C ..... Computing crown fire initiation
call crown(ntrees,dbh,rate,byram,flame,fzone,icwf)

C ..... Calculating scorch height and tree mortality
call injury(ntrees,dbh,byram,p,hs,icwf)

C ..... Computing fuel reduction or consumption
call brnoff(ln,dn,wood)
init= yes

C ..... Writing fire intensity and scorch height to file

```



```

    if(irun .eq. 1) then
      write(11,1000) yr,byram,hs,flame,rate
1000   format(I4,7f10.4)
    endif

C ..... Calculating the depth of the duff layer from duff and litter
C ..... components LN and DN.

    30 do 40 i=1,ns
      duff1 = duff1 + ln(i)
      duff2 = duff2 + dn(i)
    40 continue
C ..... Computation of duff depth from duff bulk density
    duff1 = (duff1/dbulk(ifg,1))*100.0
    duff2 = (duff2/dbulk(ifg,2))*100.0
    duff = duff1 + duff2
    return
  END
  SUBROUTINE firemd(nl,fwg,byram,flag,ifg,rate,flame,fzone)
  *****
C *
C * metric version of original (nov. 1973) SUBROUTINE firemd *
C * -- units are converted on input and reconverted on output *
C * but internal computation is expressed in british units -- *
C *
C * conversion factors are stored in array named * cio * *
C * factor value converts from to *
C * ..... *
C * cio(1) .032808 sigma 1/ft 1/cm *
C * cio(2) .18915 xir,ir,xio btu/sqft/min kw/sqm *
C * cio(3) 37.259 rhobqig btu/cuft kj/cu m *
C * cio(4) 1.60934 wind.... mi/h km/h *
C * cio(5) .3048 ratex,rate ft/min m/min *
C * cio(6) 3.4592 byramx,byram btu/ft/s kw/m *
C * cio(7) 4.8824 fwg lb/sq ft kg/sq m *
C * cio(8) 2.3244 lhv btu/lb kj/kg *
C * cio(9) .016018 rhop lb/cu ft g/cc *
C *
C *
C * variables used in this SUBROUTINE (written in fortran - iv) *
C * are identified below. the rate-of-spread model employed is *
C * documented in usda forest service research paper int-115, *
C * a mathematical model for predicting fire spread in wildland *
C * fuels, r. rothermel (northern forest fire lab., missoula), *
C * but excluding the **effective heating number** revision of *
C * w.h. frandsen suggested in usda forest service general tech- *
C * nical report int-10, 1973. the calculation of byrams inten- *
C * sity (btu/min/ft of fireline length) is based on the crude *
C * approximation that the burning zone produces a uniform rate *
C * of heat output from front to back and that the depth of the *
C * flame is determined by the burning time of the gross descrip- *
C * tive mean particle diameter 4/sigma. *
C * significant revisions include..... *
C * a new way of computing the moisture of extinction of *
C * live fuels, including 1) exponential weighting of size *
C * classes to get fine dead/live ratio and 2) using mext(1) *
C * in place of the constant 0.3 in the equation for mext(2) *
C * use of a new weighting factor, g(i,j), in place of *
C * f(i,j) in computing net effective loading by size class *

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```

C * use of a power law formula for the reaction velocity *
C * correlation parameter *a* *
C * elimination of weighting factors on reaction intensity *
C * of categories (eff. heating no. or f(i) ) *
C * programmed nov. 1973 by f. albin, nffl, missoula. *
C *
C * input variables...first the physical variables *
C *
C * symbol pg.no./eq.no. definition *
C * in int-115 *
C * next(1)...31/65 moisture of extinction of dead fuel *
C * ttheta....33/80 tangent of local slope *
C * mois(i,j).31/66 moisture content of fuel type (i,j) *
C * mps(i,j)..30/53,32/72 mean surf/vol, 1/ft, of fuel (i,j) *
C * fwg(i,j)..31/60,32/73,74 surface loading, lb/sqft fuel (i,j) *
C * lhv(i,j)..31/61 low heat value, btu/lb, fuel (i,j) *
C * rhop(i,j).30/53,32/73 oven-dry particle density, lb/cuft *
C * st(i,j)...31/60 mineral content of fuel type (i,j) *
C * se(i,j)...31/63 mineral content excluding silica *
C * wind.... wind speed at mid flame height (mph)*
C *
C * input variables...program control and specification variables*
C *
C * symbol size range description *
C *
C * nd..... 0 - 7 number of dead fuel size classes to be *
C * considered (specifies largest class if *
C * there are more classes than nd) *
C * nl..... 0 - 7 same as nd, but for live fuels *
C * ifines(1). 1 - nd ordinal number of smallest-size dead fuel*
C * to be used in computation *
C * ifines(2). 1 - nl same as ifines(1) but for live fuels *
C * largel largest dead fuel size class to be included *
C * large2 largest live fuel size class to be included *
C *
C *
C * .....output variables.....
C *
C * symbol definition *
C *
C * flag( ) . array of error flags, set to 1 for error *
C * flag(1) dead fuel too moist too spread flame *
C * flag(2) wind speed exceeds reliable extrapolation *
C * flag(3) gross surf/vol too small (sigma.lt.175) *
C * betal.....mean packing ratio (pg 32/eq 73) *
C * sigma.....characteristic surface area to volume ratio of the *
C * fuel complex, 1/ft (pg 32/eq 71) *
C * gamma.....reaction velocity, 1/min (pg 31/eq 67) *
C * xir.....reaction intensity, btu/min/sqft, calculated from *
C * eq 58, pg 31, but with area-weighting factor, f-sub*
C * -i replaced by unity...no category weighting *
C * rhobqig...heat sink term -product of bulk density, effective *
C * heating number, and heat of preignition- btu/cuft *
C * (pg 32/eq 77) *
C * phis.....slope factor modifying spread rate (pg 33/eq 80) *
C * windx.....wind speed which produces maximum spread rate, mph *
C * (pg 33/eq 86) *
C * phiwx.....maximum value of wind factor (pg 33/eq 80,87) *
C * ratex.....maximum wind-driven rate of spread, ft/min (pg 32/ *

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C      *          eq 75, with phi-sub-w of eq 79 at u=0.9*i-sub-r) *
C      * byramx....byrams intensity, btu/min/ft of fireline length, *
C      *          at the rate of spread = ratex (near statement 30) *
C      * ir(i)....reaction intensity, btu/min/sqft, for dead (i=1) *
C      *          or live (i=2) fuel type -components of xir *
C      * next(2)...moisture of extinction of live fuel (pg 35/eq 88) *
C      * **n.b.- next(1), for dead fuel, is an input parameter *
C      * byram....byrams intensity, btu/min/ft of fireline length, *
C      *          for wind speed corresponding to index j (near 33) *
C      * rate.....spread rate, ft/min, for wind speed (pg 32/eq 75) *
C      * flame ....flame length in meters p86, eq 17 *
C      * * * * *
C      * working variables...internal to SUBROUTINE *
C      * -index i refers to fuel category (1=dead, 2=live) *
C      * -index j refers to (size) class within category (j.le.100)*
C      * * * * *
C      * symbol                definition *
C      * * * * *
C      * ai(i)....fuel surface area/sqft of ground (pg 30/eq 54) *
C      * a(i,j)...fuel surface area/sqft of ground (pg 30/eq 53) *
C      * wo(i,j)...net dry fuel loading, lb/sqft (pg 31/eq 60) *
C      * f(i,j)...weighting factor (pg 30/eq 56) *
C      * g(i,j)...weighting factor for computing net effective load- *
C      *          ing for each category...replaces weighting factor *
C      *          f(i,j) used for intrinsic properties (pg 30/eq 56) *
C      *          for loading calculation, size classes are grouped *
C      *          and weighted uniformly according to contribution to *
C      *          total area by group as a whole...g = aa(n)/ai(i).. *
C      * aa1.....area of size class 1 (mps.ge.1200) *
C      * aa2.....area of size class 2 (1200.gt.mps.ge.192) *
C      * aa3.....area of size class 3 (192.gt.mps.ge.96) *
C      * aa4.....area of size class 4 (96.gt.mps.ge.48) *
C      * aa5.....area of size class 5 (48.gt.mps.ge.16) *
C      *          .....note - fuels with mps .lt. 16 are not used *
C      * gs(i,j)...shorthand for exp(-138./mps(i,j)) *
C      * at.....total fuel surface area/sqft of ground (pg 30/eq55)*
C      * fx(i)....weighting factor (pg 30/eq 57) *
C      * noclas(i).noclas(1)=nd, noclas(2)=nl. see inputs *
C      * isize(i,j)=place no. of jth finest fuel, category i *
C      * fined....dry loading of dead fines, lb/sqft *
C      * finel....dry loading of live fines, lb/sqft *
C      * wdfmn....total moisture loading of dead fines, lb/sqft *
C      * findm....average moisture of dead fines (wdfmn/fined) *
C      * xmoisl...computed live moisture of extinction (pg 35/eq 88) *
C      * ax.....=f(i,j) *
C      * qig(i,j)..heat of preignition, btu/lb (pg 32/eq 78) *
C      * mcsa(i)...weighted average moisture content (pg 31/eq 66) *
C      * bse(i)....weighted average mineral content (pg 31/eq 63) *
C      * sigmal(i).characteristic surf/vol ratio (pg 32/eq 72) *
C      * lhvl(i)...weighted average low heat value, btu/lb (pg31/eq61)*
C      * sum1.....total dry loading, lb/sqft -(see pg 32/eq 74) *
C      * sum2.....total volumetric loading, ft (see pg 32/eq 73) *
C      * wol(i)....weighted average fuel loading, lb/sqft (pg 31/eq59)*
C      * sum3.....sum in heat sink equation, btu/cuft (pg 32/eq 77) *
C      * beta.....moisture content/moisture of extinction...redefined*
C      *          for each category (pg 31/eq 65) *
C      * mdcsa(i)..moisture damping coefficient (pg 31/eq 64) *
C      * barns(i)..mineral damping coefficient (pg 31/eq 64) *
C      * sigma....gross characteristic surf/vol ratio (pg 32/eq 71) *
C      * rhopl....bulk density of fuel complex, lb/cuft (pg 32/eq 74)*

```

```

C * best.....computed optimum packing ratio (pg 32/eq 69) *
C * rat.....ratio of packing ratio to best (used in eq 67/pg31)*
C * al.....empirical fit parameter a of eq 70/pg 32 *
C * but nondivergent power law used, not eq 70/pg 32 *
C * v.....sigma**1.5 used in eq 68/pg 32 *
C * b.....exponent in eqn for propagating flux/reaction in- *
C * tensity, xsi, (pg 32/eq 76) *
C * xnl.....parameter b of eq 83/pg 33 *
C * xnl.....parameter e of eq 84/pg 33 *
C * cl.....parameter c of eq 82/pg 33 *
C * wmax.....maximum effective wind speed, ft/min (pg 33/eq 86) *
C * r.....rate of spread, ft/min (pg 32/eq 75) *
C * rmax.....maximum wind-driven rate of spread, ft/min *
C * *
C ***** firemd ***** firemd *****
common/fuell/ mext(2), rhop(2,7), tbulk(2,8), mois(2,7)
common/fuel2/ mps(2,7), lhv(2,7), st(2,7), se(2,7)
common/sites/ occur(500), rh, wind, ttheta, t
common/oper/ ns, nspan, nruns, clrcut, nwrstr, ifire, sburn, ibr, impb
real rhop, mext, mois, mps, lhv, st, se, wind, ttheta
dimension ai(2), bse(2), sigmal(2), wol(2),
& a(2,7), f(2,7), fx(2), wo(2,7), qig(2,7), barns(2)
real betal, sigma, gamma, xir, rhobqig, phis, windx, phiwx, ratex,
& lhv1(2)
real byramx, byram, rate, xio, fwg(2,7), mcsa(2), mdcsa(2), ir(2)
integer isize(2,7), ifines(2), largel, large2, n1, nd, flag(3), clrcut
dimension g(2,7), gs(2,7), gn(2), noclas(2), cio(9),
& bulk(2,7)
data cio/.032808, .18915, 37.259, 1.60934, .3048, 3.4592, 4.8824,
& 2.3244, 0.016018/

nd = 6
largel= nd
large2= n1
ifines(1)= 1
ifines(2)= 1
do 651 i=1,n1
do 650 j=1,nd
mps(i,j)=mps(i,j)/cio(1)
fwg(i,j)=fwg(i,j)/cio(7)
lhv(i,j)=lhv(i,j)/cio(8)
rhop(i,j)=rhop(i,j)/cio(9)
if(i .eq. 1) bulk(i,j)= tbulk(i,j)/cio(9)
if(i .eq. 2) bulk(i,j) = tbulk(i,j)/cio(9)
650 continue
651 continue
wind = wind/cio(4)
noclas(1) = nd
noclas(2) = n1
C.... zero all working arrays and initialize variables
gamma=0.
xir=0.
windx=0.
phiwx=0.
ratex=0.
byramx=0.
xio=0.
flag(1)= 0
flag(2)= 0
flag(3)= 0

```

```

next(2)= 0.
do 1 i=1,2
  ai(i)=0.
  mcsa(i)=0.
  bse(i)=0.
  sigmal(i)=0.
  lhvl(i)=0.
  wol(i)=0.
  sum4= 0.
  sum1= 0.
  sum2= 0.
  sum3= 0.
  ir(i)= 0.
  barns(i)= 0.
  fx(i)= 0.
  sigma= 0.
  at= 0.
  gn(i) = 0.
  do 1 j=1,7
    isize(i,j)=j
    g(i,j) =0.
    gs(i,j) = 0.
    a(i,j)=0.
    f(i,j)=0.
    wo(i,j)=0.
    qig(i,j)=0.
    byram=0.
    rate =0.
1 continue
C sort fuel components by size, finest fuels first
C isize(i,j) = place no. of jth finest fuel of category i
do 4 i=1,2
  jmax = noclas(i)
  if(jmax.le.1) go to 4
  jmm = jmax -1
  do 3 j = 1,jmm
    km = jmax - j
    do 2 k=1,km
      ida=isize(i,k)
      idb=isize(i,k+1)
      siza=mps(i,ida)
      sizb=mps(i,idb)
      if(siza.ge.sizb) go to 2
      isize(i,k+1)=ida
      isize(i,k)=idb
2 continue
3 continue
4 continue
C delete large logs from firespread considerations
do 205 i = 1,2
  kmax = noclas(i)
  if(kmax.lt.1) go to 205
  do 202 k = 1,kmax
    j = isize(i,k)
    if((mps(i,j)).ge.16.) go to 202
    noclas(i) = k-1
    go to 205
202 continue
205 continue
C calculate weighting factors

```

```

C   first, for dead fuels....
C   then for live fuels....
n1 = noclas(1)
n2 = noclas(2)
noclas(1) = min0(large1,n1)
noclas(2) = min0(large2,n2)
do 7 i = 1,2
    kmin = ifines(i)
    kmax = noclas(i)
    if((kmax.eq.0).or.(kmin.gt.kmax)) go to 7
    do 5 k = kmin,kmax
        j = isize(i,k)
        gs(i,j) = mps(i,j)/rhop(i,j)
        a(i,j) = fwg(i,j)*gs(i,j)
        gs(i,j) = exp(-138./mps(i,j))
        ai(i) = ai(i) + a(i,j)
        wo(i,j) = fwg(i,j)*(1. - st(i,j))
5       continue
        do 6 k = kmin,kmax
            j = isize(i,k)
            f(i,j) = a(i,j)/ai(i)
6       continue
7       continue
    at = ai(1) + ai(2)
    fx(1) = ai(1)/at
    fx(2) = 1. - fx(1)
C.... find weight loading of dead and live fines, moisture extinct. live
C.... note dead and live fuels wtd by exp(-c/sigma) -- c=138 or 500
fined= 0.0
finel= 0.0
wdfmn= 0.0
findm= 0.0
do 18 i=1,2
    n=ifines(i)
    jm=noclas(i)
    if((jm.le.0).or.(n.gt.jm)) go to 18
    if(i.eq.2) go to 15
    do 13 j=n,jm
        jj=isize(i,j)
        sa=mps(i,jj)
        ep =exp(-138./sa)
        wtfac= fwg(i,jj)*ep
        wmfac= wtfac*mois(i,jj)
        fined =fined + wtfac
        wdfmn = wdfmn + wmfac
13      continue
        if(fined.eq.0.) go to 18
        findm = wdfmn/fined
15      if(i.eq.1) go to 18
        do 16 j=n,jm
            jj = isize(i,j)
            sa = mps(i,jj)
            ep = exp(-500./sa)
16      continue
            finel = finel + fwg(i,jj)*ep
18      continue
        if(finel.eq.0.) go to 19
        factor = fined/finel
        xmois1=2.9*factor*(1.-findm/mext(1))-0.226
        if(xmois1.lt.mext(1)) xmois1=mext(1)
        go to 20

```

```

19 xmois1=100.
20 mext(2)=xmois1
C.... intermediate computations for each category of fuel (live + dead)
do 22 i=1,2
  aal = 0.0
  aa2 = 0.0
  aa3 = 0.0
  aa4 = 0.0
  aa5 = 0.0
  jm=noclas(i)
  n=ifines(i)
  if((jm.eq.0).or.(n.gt.jm)) go to 22
  do 21 k=n,jm
    j=isize(i,k)
    ax=f(i,j)
    sigm = mps(i,j)
    if(sigm.ge.1200.) aal = aal + a(i,j)
    if((sigm.lt.1200.).and.(sigm.ge.192.)) aa2 = aa2 + a(i,j)
    if((sigm.lt.192.).and.(sigm.ge.96.)) aa3 = aa3 + a(i,j)
    if((sigm.lt.96.).and.(sigm.ge.48.)) aa4 = aa4 + a(i,j)
    if(sigm.lt.48.) aa5 = aa5 + a(i,j)
    qig(i,j)=250. + 1116.*mois(i,j)
    mcsa(i)=mcsa(i) + ax*mois(i,j)
    bse(i)=bse(i) + ax*se(i,j)
    signal(i)=signal(i) + ax*mps(i,j)
    lhvl(i)=lhvl(i) + ax*lhv(i,j)
    sum4= sum4+bulk(i,j)*fwg(i,j)
    sum1=sum1 + fwg(i,j)
    sum2=sum2 + fwg(i,j)/rhop(i,j)
21 sum3 = sum3 + fx(i)*f(i,j)*qig(i,j)*gs(i,j)
    do 221 k = n, jm
      j = isize(i,k)
      sigm = mps(i,j)
      if(sigm.ge.1200.) g(i,j) = aal/ai(i)
      if((sigm.lt.1200.).and.(sigm.ge.192.)) g(i,j) = aa2/ai(i)
      if((sigm.lt.192.).and.(sigm.ge.96.)) g(i,j) = aa3/ai(i)
      if((sigm.lt.96.).and.(sigm.ge.48.)) g(i,j) = aa4/ai(i)
      if(sigm.lt.48.) g(i,j) = aa5/ai(i)
      wol(i) = wol(i) + g(i,j)*wo(i,j)
221 continue
    beta = mcsa(i)/mext(i)
    mdcsa(i)=1. - beta*(2.59 - beta*(5.11 - beta*3.52))
    if(mext(i).lt.mcsa(i)) mdcsa(i)=0.
    barns(i)=0.174/(bse(i)**0.19)
    if(barns(i).gt.1.) barns(i)=1.
    sigma=sigma + fx(i)*signal(i)
    ir(i) = wol(i)*lhvl(i)*mdcsa(i)*barns(i)
22 continue
    if (mdcsa(1).le.0) flag(1)= 1
    if (mdcsa(1).le.0.) go to 3777

C.... begin final computations
C.... bulk density....
  rhop1= sum4/sum1

C.... packing ratio
  betal= sum2*rhop1/sum1

C.... optimum packing ratio
  best=3.348/(sigma**.8189)

```

```

    rat=beta1/best

C.... new exponent a equation used here
    al=133./(sigma**.7913)

C.... reaction intensity weighted by surface area fraction
    v=sigma**1.5
    gamma=(v*(rat**al)*exp(al*(1.-rat)))/(495. + .0594*v)
    ir(1)=gamma*ir(1)
    ir(2)=gamma*ir(2)
    xir=ir(1)+ir(2)

C.... heat sink terms
    rhobqig=rhop1*sum3

C.... propagating intensity
    b= (.792+.681*sqrt(sigma))*(.1+beta1)
    xio =(xir*exp(b))/(192. + .2595*sigma)

C.... slope factor phis
    phis=5.275*ttheta*ttheta/(beta1**0.3)

C.... parameters for determining wind factor phiw
    xml=0.02526*(sigma**.54)
    xnl=0.715*exp(-0.000359*sigma)
    cl =7.47*exp(-0.133*(sigma**.55))
    cl = cl/(rat**xnl)
    wmax=0.9*xir
    windx=wmax/88.
    phiwx=cl*(wmax**xml)
    rmax=xio*(1.0 + phis + phiwx)/rhobqig
    ratex=rmax
    byramx=xir*ratex*384./sigma
    w=wind*88.
    phiw=cl*(w**xml)
    r=xio*(1.+phis+phiw)/rhobqig
    rate= r
    byram= xir*r*384./sigma
    fzone = (byram/xir)
    if((w.ne.0.).and.(sigma.lt.175.)) flag(3)=1.0
    if (w.gt.wmax) flag(2)= 1

C    before return to calling program
C    must convert everything to metric here

3777 continue
    sigma=sigma*cio(1)
    xir=xir*cio(2)
    rhobqig=rhobqig*cio(3)
    windx=windx*cio(4)
    ratex=ratex*cio(5)
    byramx=byramx*cio(6)/60.
    ir(1)=ir(1)*cio(2)
    ir(2)=ir(2)*cio(2)
    do 3778 i=1,n1
    do 3778 j=1,nd
        mps(i,j)=mps(i,j)*cio(1)
        fwg(i,j)=fwg(i,j)*cio(7)
        lhv(i,j)=lhv(i,j)*cio(8)
        rhop(i,j)=rhop(i,j)*cio(9)
        bulk(i,j)= bulk(i,j)*cio(9)
3778 continue
    flame = 0.45 * (byram/60.0)**(0.46)
    wind= wind*cio(4)

```



```

bcio=cio(6)/60.
rcio=cio(5)
byram=bcio * byram
rate= rate * rcio
flame = flame * cio(5)
fzone = fzone * cio(5)
xio=xio*cio(2)
return
END
SUBROUTINE FLTEMP(flame,ftmp)
C ::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::
C This subroutine calculates the average flame temperature of a
C fire with a specified intensity and rate of spread. This temp
C is used in the calculation of heat needed to ignite crown.
C ::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::

trate = 1500.0 / flame
if(trate .gt. 1500.0) trate = 1500.0
ftmp = 2000.0 - (trate)
return
END
SUBROUTINE foil(pfoil,dbh,kk)
C *****
C * Subroutine foil calculates the proportion foliage in the live *
C * crown using regression equations from Brown (1976). Equations *
C * are exponential form except for grand fir and lodgepole pine *
C * crown portion regression equations. *
C * pfoil - proportion of live foliage in crown. *
C *****
common/types/ishade(7),imoist(7),spp(7)
common/leaf/aside(7),c(7),alpha(7),b2(7),b3(7),cext(8),crat(7),
& sigma(7),ap(7),betap(7)
character*1 ishade,imoist,spp*4

C ..... Calculate the pro. foilage for each individual species
if(spp(kk) .eq. 'abgr') then
pfoil = 1.0 / (ap(kk) + betap(kk)*dbh)
elseif(spp(kk) .eq. 'pico') then
pfoil = ap(kk) + betap(kk)*dbh
else
pfoil = ap(kk)*exp(betap(kk)*dbh)
endif
return
END
SUBROUTINE fuel(ntrees,dbh,fwg,ln,lnl,dn,dnl,wood,yr,init,irun,
& branch,icwf)
C ::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::
C This subroutine:
C calculates moisture content and loading for each fuel component
C mois(1,k) ... fraction moist content of fuel component k
C fwg(1,k) .... biomass loading of fuel component k kg/sq m
C emc(k) ..... equilibrium moisture content in percent
C bbm ..... brush biomass loading, kg/sq m
C rh ..... relative humidity in percent
C t ..... ambient temperature in deg c
C ::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::
common/fuel1/ mext(2),rhop(2,7),bulk(2,8),mois(2,7)
common/fuel5/ amc(7),bmc(7),cmc(7),dmc(7),mmc(7),tmc,emc(7)
common/sites/ occur(500),rh,wind,ttheta,t
common/plotq/elev,rock,till,soilm,text,excess,pltsiz,ifg

```

```

common/oper/ ns,nspan,nruns,clrcut,nwrstr,ifire,sburn,ibr,impb
common/polut/ndyr(7),dmoist
integer clrcut,yr
dimension ntrees(1),dbh(1),fwg(2,7),sfuel(8)
real ln(1),lnl(1),dn(1),dnl(1),wood(3)
real mois,mext,branch,amc,bmc,cmc,dmc,mmc,tmc,rh,emc
data sfuel/1.000,1.000,0.717,0.668,0.768,0.768,0.985,0.852/

flit = 0.0
if (ns.le.0) return

C ..... Update fuel loadings
call loader(ntrees,dbh,lnl,ln,dnl,dn,wood,yr,branch,icwf)

C ..... Calculation of moisture content of fuel - defined as EMC
do 20 k= 1,ns
  if(emc(k) .eq. 0.0) then
    emc(k) = amc(k)*rh**bmc(k)+cmc(k)*exp((rh-100.)/
&          dmc(k))+mmc(k)*(tmc-t)
  endif
  flit = flit + ln(k)
  mois(1,k)= emc(k)
20 continue

C ..... Update fuel loadings for shrubby and herbaceous fuels
call brush(dbh,ntrees,bbml,bbm2,init)

C #####
C Putting shrub and grass fuel in appropriate element of fuel
C array (fwg). Proportions sfuel(i) for shrubs go into live
C fuel, and 0.90 for herbaceous go into dead fuels and vice
C versa.
C #####

fwg(1,1) = flit
do 30 i = 1,3
  fwg(1,i+1) = wood(i)
30 continue
fwg(1,5) = (1.0 - sfuel(ifg))*bbml
fwg(1,6) = (bbm2*0.80)
fwg(2,1)= sfuel(ifg)*bbml
fwg(2,2)= (bbm2*0.20)

C ..... Writing current fuel values to external files
if(irun .eq. 1) then
  write(8,1000) (fwg(1,1),l=1,4)
  write(9,1000) (fwg(1,1),l=5,6),(fwg(2,m),m=1,2)
endif
C ##### FORMATS #####
1000 format(7f10.3)
return
END
SUBROUTINE grow(dbh,pd,ntrees,sla,grf,s1,s2,s3,age,kyr,itop,
& inend,npine)
C *****
C This subroutines calculates the annual growth increment for each species. *
C Program logic is: *
C 1. Compute basal area of stand and subsequent reduction factor. *
C 2. Compute reduction factor for climatic effects - DEGD. *
C 3. Compute leaf area and subsequent reduction factor for shading. *

```

```

C 4. Calculate growth increment and reduce by each computed factor.      *
C 5. Compute tree mortality from random and stress factors.              *
C 6. Remove tree if computed to be dead.                                  *
C Important variables include:                                           *
C BAR - Basal area of stand in cm**2                                     *
C DEGD - number of degree days for simulation stand.                     *
C T - growth reduction factor for climatic effects.                     *
C S - reduction factor for soil fertility effects.                      *
C AL - proportion of available light to a given tree.                   *
C H - tree height in cm                                                 *
C DINC - diameter growth increment for current simulation year in cm    *
C ISHADE(i) - shade tolerance category for species i.                  *
C GRF(i) - growth reduction factor for pollution for species i.        *
C GRWS(i) - growth reduction factor for water stress for species i.     *
C AGEMX(i) - maximum attainable age for species i.                     *
C PP(i) - probability of random mortality.                              *
C MORT,B1,B2,B3,CEXT - equation coefficients.                          *
C AINC(i) - minimum possible diameter growth for species i.           *
C Subroutines called:                                                  *
C SHADE - computes leaf area index by height class.                    *
C ERROR - prints error messages if run bounds are violated.           *
C *****
dimension dbh(1),ntrees(1),sla(1),pd(1),grf(1),sl(1),s2(1),
&          s3(1),age(1),itop(1)
character*1 ishade,imoist,spp*4,spec*4
common/leaf/aside(7),c(7),alpha(7),b2(7),b3(7),cext(8),crat(7),
&          sigma(7),ap(7),betap(7)
common/oper/ ns,nspan,nruns,clrcut,nwrstr,ifire,sburn,ibr,impb
common/trunk/g(7),agemx(7),dm(7),hm(7),spm(8),ysc(7)
common/water/grws(7),ws0(7),wsm(7),nws(7),wr,grdd(7),grbar(7)
common/hdata/phi,xmbar(8),degd,ainc(7),binfest(8),ibcycle(8),br
common/climat/dmin(7),dopt(7),dmax(7),baset(12),basep(12),baseh
common/types/ishade(7),imoist(7),spp(7)
common/plotq/elev,rock,till,soilm,text,excess,pltsiz,ifg
integer clrcut
real mort(2)
data pi/3.14159265/,mort/0.328,0.100/

nlive = 0
n= isum(ntrees,ns)
if(n.eq.0)return
if(kyr .lt. impb) then
  inend = 0
elseif(kyr .eq. impb) then
  inend = kyr + ibcycle(ifg)
endif

C ..... Compute total basal area of entire stand
bar= 0.
do 5 j= 1,n
  bar= bar+(pi/4.)*dbh(j)**2
5 continue

C ..... Compute shading leaf area for each tree
call shade(ntrees,dbh,sla,sl,s2,s3,pltsiz)
do 10 i=1,ns

C ..... Calculate soil fertility reduction factor from basal area
grbar(i) = 1.0 - bar / (xmbar(ifg) * 10000.0 * pltsiz)

```

```

ni= ntrees(i)
if (ni.eq.0) go to 10
if(i .eq. 1) then
  jj = 0
else
  jj= isum(ntrees,i-1)
endif
do 20 j= 1,ni

C ..... Compute standardized available light, then calculated growth
C ..... increment (maximum)
  al= phi*exp(-cext(ifg)*sla(j+jj))
  h= 137.+b2(i)*dbh(j+jj)-b3(i)*dbh(j+jj)**2.0
  dinc= g(i)*dbh(j+jj)*(1.-h*dbh(j+jj)/(hm(i)*dm(i)))
  dinc=dinc/(274.+3.*b2(i)*dbh(j+jj)-4.*b3(i)*dbh(j+jj)**2.0)

C ..... Reduce diameter increment for shading effects
  if(ishade(i).eq.'i' .or. ishade(i) .eq. 'I') then
    dinc = 2.24*(1.-exp(-1.136*(al-.08)))*dinc
  elseif(ishade(i) .eq. 't' .or. ishade(i) .eq. 'T' .or.
    & ishade(i) .eq. 'm' .or. ishade(i) .eq. 'M') then
    dinc = (1.-exp(-4.64*(al-.05)))*dinc
  endif

C ..... Reduce diameter increment using environmental growth reduction factors

  dinc= dinc * grf(i) * grws(i) * grdd(i) * grbar(i)
  if (dinc .gt. 5.0) call error(11)

C ..... Calculate tree mortality for random and stress factors
  if(spp(i) .eq. 'pial') then
    pd(j+jj) = 3.0 / agemx(i)
  else
    pd(j+jj) = 4.0 / agemx(i)
  endif
  if (dinc .lt. ainc(i)) then
    if(ishade(i) .eq. 'I' .or. ishade(i) .eq. 'i') then
      pd(j+jj) = pd(j+jj) + mort(1) - (mort(1)*pd(j+jj))
    else
      pd(j+jj) = pd(j+jj) + mort(2) - (mort(2)*pd(j+jj))
    endif
  endif

C ..... Calculate tree mortality if blister rust infection
  if(kyr .ge. ibr) then
    if(spp(i) .eq. 'pial' .or. spp(i) .eq. 'pimo') then
      dia = dbh(j+jj)
      tage = age(j+jj)
      infec = itop(j+jj)
      if(infec .eq. 0) then
        rnum = rnd()
        if(rnum .lt. pinfec) itop(j+jj) = 1
      endif
      call rust(dia,tage,prob,pinfec,infec)
      pd(j+jj) = pd(j+jj) + prob
    endif
  endif

C ..... Calculate tree mortality if mountain pine beetle infestation
  if(kyr .eq. impb) then

```

```

        if(spp(i) .eq. 'pial' .or. spp(i) .eq. 'pico'
&      .or. spp(i) .eq. 'pipo' .or. spp(i) .eq.
&      'pimo') then
            if(dbh(j+jj) .gt. 10.0) then
                npine = npine + 1
                nlive = nlive + 1
            endif
        endif
    endif
endif
if(kyr .gt. impb .and. kyr .le. inend) then
    if(spp(i) .eq. 'pial' .or. spp(i) .eq. 'pico' .or.
&      spp(i) .eq. 'pipo' .or. spp(i) .eq. 'pimo') then
        dia = dbh(j+jj)
        tage = age(j+jj)
        spec = spp(i)
        call beetle(spec,dia,tage,prob)
        pd(j+jj) = pd(j+jj) + prob
        if(dbh(j+jj) .gt. 10.0) then
            nlive = nlive + 1
        endif
    endif
endif
endif
endif

C ..... Incrementing individual tree diameter
        dbh(j+jj) = dbh(j+jj) + dinc
20    continue
10    continue
    if(npine .gt. 0) then
        pinfest = 1.0 - float(nlive) / float(npine)
    else
        pinfest = 1.0
    endif
    if(kyr .gt. inend .or. pinfest .ge. binfest(ifg)) inend = 0
    return
END
SUBROUTINE injury(ntrees,dbh,byram,p,hs,icwf)
C ::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::
C This subroutine calculates scorch height then estimates tree mort- :
C ality from scorch height using the function RISK. Parameters for :
C RISK include percent crown scorched, DBH, and scorch height. :
C Variables are: :
C   cl,c2,c3 ... coefficients for byrams equation :
C   byram ..... byrams fire intensity (kw/m) :
C   wind..... wind speed (km/hr) :
C   tkill ..... lethal foliage temperature (deg cent) :
C   bc ..... ratio of bark thickness to diameter at breast height:
C   hs ..... crown scorch height in meters :
C   p ..... prob tree dies within one year :
C   t ..... ambient air temperature (deg cent) :
C ::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::
common/oper/ ns,nspan,nruns,clrcut,nwrstr,ifire,sburn,ibr,impb
common/leaf/aside(7),c(7),alpha(7),b2(7),b3(7),cext(8),crat(7),
&      sigma(7),ap(7),betap(7)
common/sites/ occur(500),rh,wind,ttheta,t
common/mort/ dl(7),d2(7),d3(7),bc(7)
integer clrcut
dimension ntrees(1),dbh(1),p(1)
data cl/.7422/,c2/.02559/,c3/.2778/,tkill/60./,hsmin/.1/

n= isum(ntrees,ns)

```

```

        if (n.eq.0) return

C ..... Byrams equation for crown scorch height
      hs= c1*byram**1.1667/(sqrt(c2*byram+(c3*wind)**3)*(tkill-t))
      if (hs.lt.hsmin) return
      do 10 k= 1,ns
        kkk = k
        nk= ntrees(k)
        if (nk.eq.0) go to 10
        if(kkk .eq. 1) then
          jj = 0
        else
          jj= isum(ntrees, kkk-1)
        endif
        do 20 j= 1,nk

C ..... Calculation of crown scorch volume (Ryan Rheinhardt)
          ht = (137.+b2(k)*dbh(j+jj)-b3(k)*dbh(j+jj)**2)/100.0
          hcr = crat(k)*ht
          b = hs - (ht - hcr)
          if(b .le. 0.0) b = 0.0
          if(b .ge. hcr) b = hcr
          ck = 100.0 * (b*(2*hcr-b)/(hcr**2.0))
          dia = dbh(j+jj)

C ..... Estimation of probability of tree mortality from fire
          if(icwf .eq. 1) then
            p(j+jj) = 1.00
          else
            p(j+jj)= risk(ck,dia, kkk)
          endif
        20 continue
      10 continue
      return
      END
      SUBROUTINE kill(nalive, ndead, dbh, pd, u, age, branch, itop, icwf)
C ::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::
C : Subroutine kill eliminates trees from simulation plot by first :
C : generating a random number (u(k)) and comparing it with current :
C : probability of death for a given tree (p(i)). If u(k) less than :
C : p(i) the tree is removed and the standing woody fuel is distrib- :
C : uted on plot with subroutine SNAG. :
C ::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::
      common/limits/ mxtrs, maxspc, mxdd, mxyrs, maxbin
      common/leaf/ aside(7), c(7), alpha(7), b2(7), b3(7), cext(8), crat(7),
&          sigma(7), ap(7), betap(7)
      common/oper/ ns, nspan, nruns, clrcut, nwrstr, ifire, sburn, ibr, impb
      integer clrcut
      dimension nalive(1), ndead(1), dbh(1), pd(1), u(1), age(1),
&          itop(1)

      n= isum(nalive, ns)
      if (n.eq.0) return

C ..... Call the random number generator and initialize
      call rgen(u, n)
      indxl= 0
      ksp= 0
      ksum= 0

```

```

C ..... Calculate mortality by tree and species
  do 10 k= 1,n
    5   if (k.le.ksum) go to 6
        ksp= ksp+1
        ksum= ksum+nalive(ksp)
        go to 5

C ..... If a tree lives:
  6   if (u(k).gt.pd(k)) then
        indxl= indxl+1
        dbh(indxl)= dbh(k)
        age(indxl)=age(k)+1.0
        pd(indxl)= pd(k)
        itop(indxl) = itop(k)
      else

C ..... If a tree dies:
        dia = dbh(k)
        if(icwf .eq. 0) call snag(dia,branch,ksp)
        nalive(ksp)= nalive(ksp)-1
        ndead(ksp)= ndead(ksp)+1
      endif
  10 continue
  return
  END
  SUBROUTINE loader(ntrees,dbh,lnl,ln,dnl,dn,wood,yr,branch,icwf)
C :::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::
C This subroutine adds woody fuel, duff and litter to the forest floor. :
C Woody fuel is collected in WOOD(i) while litter is stored in LN(i).  :
C The duff weight is also calculated and stored in DN(i).              :
C The output variables:                                               :
C   fyr .... number of years to reach maximum fuel loadings          :
C   fload .. maximum fuel loading for woody fuel in a fire group      :
C   lnl .... previous year's litter loading for 100 sq meters stand   :
C   ln .... current year litter loading for 100 sq meters             :
C   fuel properties                                                    :
C   dkl .... litter decay constants                                   :
C   ltd .... litter to duff conversion constants                       :
C   dkf .... fresh litter fall decay constants                         :
C   dkd .... duff decay constants                                     :
C   leaf properties                                                    :
C   ffl .... fraction of leaf biomass which falls in one year        :
C :::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::
  dimension ntrees(1),dbh(1)
  common/oper/ ns,nspan,nruns,clrcut,nwrstr,ifire,sburn,ibr,impb
  common/plotq/elev,rock,till,soilm,text,excess,pltsiz,ifg
  common/polut/ndyr(7),dmoist
  common/fuel3/ dkl(7),dkd(7),dkf(7),ltd(7)
  common/fuel4/ abm(7),ffl(7),fyr(3,8),fload(3,8)
  real ln(1),lnl(1),dn(1),dnl(1),wood(3)
  real dkl,dkd,dkf,ltd,abm,ffl,fnl(7),litduff
  integer clrcut,yr,fyr
  data litduff/0.100/

C ..... Initializing fuel loadings for start of simulation
  if(yr .eq. 1 .or. icwf .eq. 1) then
    do 5 i = 1,3

C ..... If the stand has been clearcut
  if(clrcut .eq. 1) then

```

```

        wood(i) = fload(i,ifg)/float(fyr(i,ifg))
        do 1 j = 1,ns
            ln(j) = litduff * 0.25
            dn(j) = litduff * 0.75
1            continue
        elseif(icwf .eq. 1) then
C ..... if stand has had a crown fire
        wood(i) = (fload(i,ifg)/float(fyr(i,ifg)))*0.1
        do 2 j = 1,ns
            ln(j) = litduff * 0.25
            dn(j) = litduff * 0.75
2            continue
        else
C ..... If the stand is mature
        wood(i) = fload(i,ifg)/(float(fyr(i,ifg))/2.0)
        do 3 j = 1,ns
            ln(j) = litduff * 0.25
            dn(j) = litduff * 0.75
3            continue
        endif
5        continue
        branch = 0.0
        return
    endif

C ..... Calculating needlefall then litter accumulation
do 10 k= 1,ns
    kkk = k
    dnl(k)= dn(k)
    lnl(k)= ln(k)
    nk= ntrees(k)
    if (nk.eq.0) go to 10
    if(kkk .eq. 1) then
        jj = 0
    else
        jj= isum(ntrees,kkk-1)
    endif
    call needle(sla,jj,nk,dbh,kkk,wgt,pltsiz)
    if(clrcut .eq. yr) then
        fnl(k)= wgt/(1000.0*pltsiz)
    else
        fnl(k)= wgt/(1000.0*float(ndyr(k))*pltsiz)
    endif

C ..... The dynamic loading equations for litter and duff components
    ln(k)= lnl(k)*(1.-dkl(k)-ltd(k))+fnl(k)*(1.-dkf(k))
    dn(k)= dnl(k)*(1.-dkd(k))+lnl(k)*ltd(k)
10 continue

C ..... Calculation of woody fuel components - 1,10,100 hour fuels
do 30 i = 1,3
    if(wood(i) .lt. fload(i,ifg)) then
        wood(i) = wood(i) + fload(i,ifg)/float(fyr(i,ifg))
        & + ((branch * 0.333) / pltsiz)
    else
        wood(i) = fload(i,ifg)
    endif
30 continue

```



```

branch = 0.0
return
END
SUBROUTINE needle(sla,ikk,nkk,dbh,kk,wgt,pltsiz)
C *****
C This subroutine calculates the crown weight from equations in Brown *
C (1984) then gets the percentage of the weight that is foliage from *
C subroutine PFOIL. Using these and other species-specific parameters *
C the leaf area index SLA of the stand is estimated. *
C *****
character*1 imoist,ishade,spp*4
common/leaf/aside(7),c(7),alpha(7),b2(7),b3(7),cext(8),crat(7),
&      sigma(7),ap(7),betap(7)
common/types/ishade(7),imoist(7),spp(7)
dimension dbh(1)

sla = 0.0
wgt = 0.0

C ..... Calculate the weight of live crown by species
do 10 ii = 1,nkk
  dia = dbh(ii+ikk) * 0.3937
  call foil(pfoil,dia,kk)
  if(spp(kk) .eq. 'abla') then
    wt = (alpha(kk) + c(kk)*dia**(2.0))*453.59
  else
    wt = 453.59 * exp(alpha(kk) + c(kk)*alog(dia))
  endif
  wgt = wgt + wt * pfoil

C ..... Calculate the leaf area for this species
  sla = sla + ((wt / 0.5)*sigma(kk)/aside(kk))/(100000.0*
&      pltsiz)
10 continue
return
END
SUBROUTINE output(x,nyears)
C *****
C This subroutine writes the average basal area of each tree for *
C each year of simulation. X(i,j) contains species' basal area. *
C *****
common/oper/ ns,nspan,nruns,clrcut,nwrstr,ifire,sburn,ibr,impb
integer clrcut
dimension x(nyears,1)

open(unit=7,file='BASAL.DAT',pad='yes',recl=100)

C ..... Print the average basal area over nspan years to unit 7
do 10 j= 1,nspan
  write(7,2000) (x(j,k),k=1,ns)
10 continue
close(7)
return
1000 format(13,1x,13)
2000 format(7f10.3)
END
SUBROUTINE pinalb(fnj,sla,dbh,age,ntrees,itop,ccrop,cones)
C *****
C *      - subroutine pinalb -
C * This subroutine calculates the number of whitebark pine seedlings *

```

```

C * to establish on the simulation plot. The algorithm is based on *
C * a cone:bird ratio which indicates availability of cones to the *
C * Clark's nutcracker. Excess cones are then available for bears *
C * and squirrels. In addition, the number of seedlings (or caches) *
C * depends on density of foliage modeled as a function of leaf area *
C * index. *
C *****
dimension dbh(1),age(1),itop(1)
common/leaf/aside(7),c(7),alpha(7),b2(7),b3(7),cext(8),crat(7),
&
sigma(7),ap(7),betap(7)
common/hdata/phi,xmbar(8),degd,ainc(7),binfest(8),ibcycle(8),brr
common/wbark/ cmax,agecon,dbhmin,birds,spc,spcac,cyr(4),fmax,cpt,
&
pfind,ssc
common/plotq/elev,rock,till,soilm,text,excess,pltsiz,ifg
common/types/ishade(7),imoist(7),spp(7)
common/oper/ ns,nspan,nruns,clrcut,nwrstr,ifire,sburn,ibr,impb
integer ntrees(1),clrcut
character*1 ishade,imoist,spp*4
data pw1,pw2,pw3,a1,a2,a3/5.0,5.0,5.5,0.6,0.6,0.8/
data amin,aopt,amax/40.0,250.0,850.0/

C ..... Line functions for cacheability etc..
pref(y) = 1.00 - ((exp(-((y / fmax) - 1.0) / (a1 - 1.0))**pw1)
&
- exp(-(-1.0 / (a1 - 1.0))**pw1)) /
&
(1.0 - exp(-(-1.0 / (a1 - 1.0))**pw1)))
frac(y) = 1.0 - ((exp(-((y / cmax) - 1.0) / (a2 - 1.0))**pw2)
&
- exp(-(-1.0 / (a2 - 1.0))**pw2)) /
&
(1.0 - exp(-(-1.0 / (a2 - 1.0))**pw2)))
cac(y) = exp((y / cmax)**(pw3) - (1.0 + 0.5 * ((cmax-y)/cmax)))

C ..... Initialize appropriate variables
v = (amax - aopt) / (aopt - amin)
cones = 0.0

C ..... Search to find if whitebark species is present
do 20 i = 1,ns
if(spp(i) .eq. 'pial') then
ntrs = ntrees(i)

C ..... Calculation of cone bearing trees on plot
ictree = 0
if(i .eq. 1) then
ii = 0
else
ii = isum(ntrees,i-1)
endif
do 1 j = 1,ntrs
if(dbh(j+ii) .gt. dbhmin .and. age(j+ii) .gt.
&
amin .and. age(j+ii) .le. amax) then
ictree = ictree + 1
endif
1 continue

C ..... Calculation of relative size of cone crop
rnum = rnd()
do 5 j = 1,4
if(rnum .le. cyr(j)) then
confac = float(j-1) / 3.0
go to 6
endif

```

```

5         continue

6         if(ictree .le. 1) then
            cones = ccrop * confac
            go to 30
        endif

C ..... Calculation of number of cones per tree and then the summation
        if(i .eq. 1) then
            ii = 0
        else
            ii = isum(ntrees,i-1)
        endif
        do 10 j = 1,ntrs
            if(dbh(j+ii) .gt. dbhmin .and. age(j+ii) .gt.
&          amin .and. age(j+ii) .le. amax) then
                t = ((age(j+ii) - amin) *
&          (amax-age(j+ii))**v) /
&          (((amax-aopt)**v) *
&          (aopt - amin))
                cones = (cpt * t) + cones
                if(itop(j+ii) .eq. 1) cones = cones * 0.1
            endif
10        continue
            ccrop = cones
            if(cones .gt. 0.0) then
                cones = cones * confac
            else
                cones = cmax * 0.1 * confac
            endif
            go to 30
        endif
20 continue
return

C ..... Calculation of the number of caches on the plot
30 caches = ((cones * spc) / spcac) * (1.0 - (pfind + ssc))
    if(caches .le. 0.0) caches = 0.0

C ..... Calculation of the cones per bird ratio
cpb = ((cones / birds) / pltsiz) * 4046.849
    if(cpb .gt. cmax) cpb = cmax

C ..... Calculation of the fraction of cones available to griz
fcone = frac(cpb)
    if(fcone .le. 0.2) fcone = 0.2
    if(fcone .gt. 0.9) fcone = 0.9

C ..... Calculation of the reduction factor for cacheability
cabil = cac(cpb)

C ..... Calculation of the reduction factor for preferability (LAI)
    if(sla .gt. fmax) sla = fmax
    pleaf = pref(sla)
    if(pleaf .le. 0.1) pleaf = 0.1
    if(pleaf .gt. 1.0) pleaf = 1.0

C ..... Final calculation of seedlings started in current year FNJ
fnj = caches * cabil * pleaf

```

```

        return
        END
        SUBROUTINE pollut(grf,kyr)
C *****
C This subroutine calculated growth reduction effects from air pollutants *
C However, since air pollution effects are minimal in the Inland North- *
C west, the growth reduction factor for pollution was set equal to 1.0. *
C Important Variables: *
C   grf(i).... growth reduction factor for species i *
C   cr(i).... threshold of pollution damage for species i *
C   sen(i).... sensitivity coefficient for species i *
C   ndyr(i)... number of years needles are retained for species i *
C   cbar..... seasonal average so2 concentration ppm *
C   kyr..... current year *
C   ns..... number of tree species *
C *****
        common/polut/ndyr(7),dmoist
        common/oper/ ns,nspan,nruns,clrcut,nwrstr,ifire,sburn,ibr,impb
        integer clrcut
        dimension grf(1)
        if (ns.le.0) return
        if (kyr.eq.0) return

C ..... Set pollution growth reduction factor to 1.0 for Montana
        do 10 i= 1,ns
            grf(i)= 1.000
        10 continue
        return
        END
        SUBROUTINE rgen(x,i)
C *****
C Subroutines RGEN and RANST and function RAN are random number *
C generators for the model. Users should use their own random number *
C generators which return n random numbers u between 0 and 1 with *
C uniform distribution. XRANDOM is a Perkin-Elmer generator. *
C *****
        dimension x(i)

C ..... Fill array x(i) with random numbers from XRANDOM
        do 10 j=1,i
            xx = rnd()
            x(j) = xx
        10 continue
        return
        END
        SUBROUTINE rings(n,u)
C *****
C Subroutine RINGS produces an array containing the simulation years that *
C are fire years. This is a stochastic function where a random number is *
C generated (U(i)) and if less than p (set in the data statement) then *
C a fire is to be simulated for that year. The calculation is abandoned *
C if IFYR is greater than zero (user specified fire years). *
C Variables are: *
C   X(k) - fire year array containing 0 (no fire) or 1 (fire) *
C   U(i) - random number array *
C   R - number of years to block fires after a fire has been generated *
C   PNB - probability of fire in a blocked year. *
C   IFYR - user specified fire interval *
C *****
        common/oper/ ns,nspan,nruns,clrcut,nwrstr,ifire,sburn,ibr,impb

```

```

common/sites/ x(500),rh,wind,ttheta,t
integer x,r,yes,no,clrcut
real u(1),ul(1)
data r/3/,p/.0125/,yes/1/,no/0/
if (n.eq.0) return

C ..... Initializing fire array
do 10 i= 1,n
    x(i)= no
10 continue

C ..... Assign fire years if user specified
if(ifire .gt. 0) then
    ifyr = ifire
    do 20 k = 1,n
        if(k .eq. ifyr) then
            x(k) = yes
            ifyr = ifyr + ifire
        endif
    20    continue

C ..... Assign only one fire year if number is negative
elseif(ifire .lt. 0) then
    ifyr = iabs(ifire)
    x(ifyr) = yes
    return

C ..... Calculate fire years using stochastic function
else
    i= 0
    if (r.eq.1) go to 35

C ..... Calculate pnb, prob of an unblocked state
pnb= 1./(p*float(r-1))
call rgen(ul,1)
if (ul(1).le.pnb) go to 35

C ..... Select an integer b at random from 1,2,3,... r-1
call rgen(ul,1)
i= int(float(r-1)*ul(1))+1
35    call rgen(u,n)
40    i= i+1
    if (i.gt.n) return
    if (u(i).gt.p) go to 40

C ..... Assign fire years
    x(i)= yes
    i= i+r-1
    go to 40
endif

return
END
SUBROUTINE rust(dia,age,prob,pinfec,infec)
C *****
C This subroutine simulates individual tree mortality in the event *
C of a blister rust infection. Mortality functions are from *
C *
C *****

```

```

    prob = 0.0
    if(infec .eq. 0) then
        pinfec = 0.50
    elseif(infec .eq. 1) then

C ..... Calculate prob mortality for 5 needle pine from equation
        prob = exp(-0.10*dia)
        if(age .gt. 850.0) prob = 0.99
    endif

    return
    END
    SUBROUTINE shade(ntrees,dbh,sla,h,temp,indx,pltsiz)
C *****
C This subroutine calculates the effective leaf area index by tree *
C height to estimate shading effects for individual trees. Logic is: *
C 1. Calculated leaf areas for every tree. *
C 2. Sort leaf areas according to height. *
C 3. Sum leaf areas by height. *
C 4. Reorder the cumulative leaf areas by DBH. *
C Variables are: *
C TEMP(i) - temporary array containing leaf areas *
C SLA(i) - working array for leaf areas *
C DBH(i) - array containing dbh for each tree on plot *
C ALPHA,SIGMA,ASIDE,PLTSIZ - conversion factors for crown weight to *
C leaf area *
C Subroutines called: *
C SORTP - sorts leaf area according to height *
C *****
    common/oper/ ns,nspan,nruns,clrcut,nwrstr,ifire,sburn,ibr,impb
    integer clrcut
    character*1 imoist,ishade,spp*4
    common/types/ishade(7),imoist(7),spp(7)
    common/leaf/aside(7),c(7),alpha(7),b2(7),b3(7),cext(8),crat(7),
    & sigma(7),ap(7),betap(7)
    common/trunk/g(7),agemx(7),dm(7),hm(7),spm(8),ysc(7)
    common/hdata/phi,xmbar(8),degd,ainc(7),binfest(8),ibcycle(8),brr
    dimension ntrees(1),dbh(1),sla(1),indx(1),temp(1),h(1)

C ..... Calculation of leaf area for each tree
    n= isum(ntrees,ns)
    if (n.eq.0) return
    do 10 k= 1,ns
        nk= ntrees(k)
        if (nk.eq.0) go to 10
        if(k .eq. 1) then
            kk = 0
        else
            kk= isum(ntrees,k-1)
        endif
        do 20 i= 1,nk
            h(i+kk)= 137.+b2(k)*dbh(i+kk)-b3(k)*dbh(i+kk)**2.0
            if(spp(k) .ne. 'abla') then
                temp(i+kk) = ((exp(alpha(k)+c(k)*alog(dbh(i+kk)
                & /2.54))**453.59)/0.5)*
                & sigma(k)/aside(k)
            else
                temp(i+kk) = (((alpha(k) + c(k)*(dbh(i+kk)/2.54)
                & **2.0)**453.59)/0.5)*
                & sigma(k)/aside(k)
            endif
        enddo
    enddo

```

```

        endif
        temp(i+kk) = temp(i+kk)/(100000.0*pltsiz)
        indx(i+kk)= i+kk
20      continue
10     continue

C ..... Sort sla according to h
      call sortp(h,n,indx)
      do 40 j= 1,n
          k= indx(j)
          sla(j)= temp(k)
40     continue

C ..... Compute final values of sla
      nml= n-1
      do 50 j= 1,nml
          temp(j)= sum(sla(j+1),n-j)
50     continue
      temp(n)= 0.

C ..... Reorder elements of sla to correspond to dbh
      do 60 j= 1,n
          k= indx(j)
          sla(k)= temp(j)
60     continue
      return
      END
      SUBROUTINE sitdta
C ::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::
C This program reads in site specific data from an external file on :
C device 3. Values are then passed back to main driver.           :
C ::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::
      common/plotq/elev,rock,till,soilm,text,excess,pltsiz,ifg
      common/climat/dmin(7),dopt(7),dmax(7),baset(12),basep(12),baseh
      common/hdata/phi,xmbar(8),degd,ainc(7),binfest(8),ibcycle(8),brr
      common/sites/ occur(500),rh,wind,ttheta,t
      common/polut/ndyr(7),dmoist
      common/fuel5/ amc(7),bmc(7),cmc(7),dmc(7),mmc(7),tmc,emc(7)
      character*10 name

      open(unit=3,file='SITE.DAT',form='formatted',
&        recl=150,pad='yes')

C ..... Read in site specific data for simulation plot
      read (3,1000) name, (baset(j),j=1,12)
      write(5,1000) name, (baset(j),j=1,12)
      read (3,1000) name, (basep(j),j=1,12)
      write(5,1000) name, (basep(j),j=1,12)
      read (3,2000) name, baseh
      write(5,2000) name, baseh
      read (3,2000) name, excess
      write(5,2000) name, excess
      read (3,2000) name, phi
      write(5,2000) name, phi
      read (3,2000) name, text
      write(5,2000) name, text
      read (3,2000) name, rock
      write(5,2000) name, rock
      read (3,2000) name, elev
      write(5,2000) name, elev

```

```

      read (3,3000) name, ifg
      write(5,3000) name, ifg
      read (3,2000) name, till
      write(5,2000) name, till
      read (3,2000) name, rh
      write(5,2000) name, rh
      read (3,2000) name, wind
      write(5,2000) name, wind
      read (3,2000) name, ttheta
      write(5,2000) name, ttheta
      read (3,2000) name, t
      write(5,2000) name, t
      read (3,2000) name,pltsiz
      write(5,2000) name,pltsiz
      read (3,4000) name,(emc(j),j=1,7)
      write(5,4000) name,(emc(j),j=1,7)
      read (3,2000) name,dmoist
      write(5,2000) name,dmoist
      read (3,2000) name,brr
      write(5,2000) name,brr
      rewind 3
      close(3)
      return
1000 format(a10,12f5.2)
2000 format(a10,f10.3)
3000 format(a10,i10)
4000 format(a10,7f10.3)
      END
      SUBROUTINE site
C ::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::
C This subroutine calculates all site parameters that are used in the :
C various algorithms throughout the program. Actual and potential :
C evapotranspiration are calculated along with water stress growth :
C reduction factors. New calculations are passed to main program. :
C ::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::
      dimension sitet(12),pp(12)
      dimension pei(12),actei(12),stori(12)
      common/water/grws(7),ws0(7),wsm(7),nws(7),wr,grdd(7),grbar(7)
      common/oper/ ns,nspan,nruns,clrcut,nwrstr,ifire,sburn,ibr,impb
      common/plotq/elev,rock,till,soilm,text,excess,pltsiz,ifg
      common/climat/ dmin(7),dopt(7),dmax(7),baset(12),basep(12),baseh
      common/hdata/phi,xmbar(8),degd,ainc(7),binfest(8),ibcycle(8),brr
      character*6 nsoilq,nheati,nsoilm,nape*4,nspe*4,nwra*4
      character*5 ndiff,ndegd,ngrws,na*2,npe*3,nacte,nstor
      character nwr*3,nsat*4,nwrs*4
      integer clrcut
      data nsoilq/' soilq'//,ndiff/' diff'//,ndegd/' degd'//
      data nheati/' heati'//,na/' a'//,npe/' pe'//,nacte/' acte'//
      data nsoilm/' soilm'//,nstor/' stor'//
      data nwr/' wr'//,ngrws/' grws'//,nsat/' sat'//
      data nwra/' wra'//,nape/' ape'//,nwrs/' wrs'//,nspe/' spe'//

      rocky= (100.- rock)/100.

C ..... Rock is percent of surface area in rock outcrop
C ..... Till is depth of watering or root zone in feet.
C ..... Text is amount of available water for storage in mm/m

      till=till/3.2808
      xmbar(ifg) = xmbar(ifg)*rocky

```



```

diff=baseh-elev
tmin=baset(1)+(2.2*diff/1000.)
tmax=baset(7)+(3.6*diff/1000.)
tave=(tmax+tmin)/2.
t=40.
if(tmin.gt.t) write(5,98)

98 format(1h , ' ----- you cant use minimum january temperature',
1's greater than 40',1h , 'without modifying SUBROUTINE ',
2'site -----')

if(tmax.lt.tmin) write(5,99)

99 format(1h , '----- to work in the southern hemisphere one ',
1'must modify SUBROUTINE site -----')

degd=(365./(2.*3.14159))*(tmax-tmin)-(365./2.)*(t-tave) + (
1(365./3.14159)*(t-tave)**2 )/(tmax-tmin)

C ..... Calculation of actual and potential evapotranspiration.
heatl=0.
soilm=0.
do 10 i=1,12
    sitet(i)=baset(i) + 3.6*diff/1000.
    sitet(i)=(5./9.)*(sitet(i)-32.)
    pp(i)=basep(i)*25.4
    if(sitet(i).le.0.0) go to 10
C ..... Calculation of intermediate heat index
    heatl=heatl+(sitet(i)/5.0)**1.514
10 continue

C ..... Calculation of intermediate exponent in thornwaithes equation
a=(9.675*(heatl**3.)-77.1*heatl**2+17920.*heatl+492390.)*.000001
m=1

C ..... Computation of storage capacity of soil
strmax=aminl(till,10.)*text*rocky

C ..... Calculation of the water balance equation
do 250 i=1,12
    if(sitet(i).le.0.0) go to 250
    pe=16.*(((10.*sitet(i))/heatl)**a)
    if(m.gt.1) go to 220
    stor=strmax
    m=2
220    if(pe.ge.stor + excess*pp(i)) go to 230
    acte=pe
    go to 240
230    acte=stor+excess*(aminl(pp(i),strmax))
240    stor=aminl(strmax,stor-acte+pp(i))
    soilm=soilm + acte
    pei(i)=pe
    acte(i)=acte
    stori(i)=stor
250 continue
ape=0.0
do 300 i=1,12
    ape=ape+pei(i)
300 continue

```

```

C ..... Calculation of the water stress reduction factor parameters
C ..... Ape=annual potential evapotranspiration
C ..... Soilm= annual actual evapotranspiration
C ..... Spe=seasonal potential evapotranspiration
C ..... Sat= seasonal actual evapotranspiration
C ..... Wra=annual actual et/annual potential et
C ..... Wrs=seasonal actual et/seasonal potential et
      spe=0.0
      sat=0.0
      do 301 i=4,10
          spe=spe+pei(i)
          sat=sat+actei(i)
301      wra=soilm/ape
          wrs=sat/spe
          wr=wra
C ..... Call wrstrs to figure reduction factor then write results to file
      call wrstrs
      write(5,3000)
      write(5,1000) nsoilq,xmbar(ifg)
      write(5,1000) ndiff,diff
      write(5,1000) ndegd,degd
      write(5,1000) nheat,heat
      write(5,1000) na,a
      write(5,1000) nsoilm,soilm
      write(5,2000) npe,(pei(k),k=1,12)
      write(5,2000) nacte,(actei(k),k=1,12)
      write(5,2000) nstor,(stori(k),k=1,12)
      write(5,1000) nwr,wr
      write(5,4000) ngrws,(grws(k),k=1,ns)
      write(5,4000) ndegd,(grdd(k),k=1,ns)
      write(5,1000) nwra,wra
      write(5,1000) nape,ape
      write(5,1000) nwrs,wrs
      write(5,1000) nspe,spe
      write(5,1000) nsat,sat
1000 format(1x,a8,f10.3)
2000 format(a8,12f5.1)
3000 format(10x,'calculated parameters in site')
4000 format(a8,7f10.4)
      return
      END
      SUBROUTINE snag(dbh,branch,kk)
C ::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::
C This subroutine adds the branchwood material of a dead tree to :
C the woody fuel components. BRANCH variable holds the total :
C biomass of the dead woody branchwood until subroutine FIRE then :
C equal values of BRANCH go into the three woody fuel types WOOD. :
C ::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::
      character*1 imoist,ishade,spp*4
      common/types/ishade(7),imoist(7),spp(7)
      common/leaf/aside(7),c(7),alpha(7),b2(7),b3(7),cext(8),crat(7),
&          sigma(7),ap(7),betap(7)
C ..... Calculate the downed woody fuel from a dead snage
      dbh = dbh*0.3937
      if(spp(kk) .eq. 'abla') then
          wt = (alpha(kk) + c(kk)*(dbh)**(2.0))*0.045359
      else
          wt = exp(alpha(kk)+c(kk)*alog(dbh))*0.045359
      endif

```

```

C ..... Calculate the weight of needlefall
  call foil(pfoil,dbh,kk)
  branch = branch + wt*(1.0 - pfoil)

  return
  END
  SUBROUTINE sortp(a,n,b)
C *****
C This subroutine sorts leaf area by height of individual trees, then *
C passes the manipulated array back to subroutine GROW. *
C *****
  dimension a(n)
  integer b(n)
  dimension iu(16),il(16)
  integer p

  i=1
  j=n
  m=1
  5 if(i.ge.j) go to 70

C first order a(i),a(j),a((i+j)/2), and use median to split the data
  10 k=i
  ij=(i+j)/2
  t=a(ij)
  it=b(ij)
  if(a(i).le.t) go to 20
  a(ij)=a(i)
  b(ij)=b(i)
  a(i)=t
  b(i)=it
  t=a(ij)
  it=b(ij)
  20 l=j
  if(a(j).ge.t) go to 40
  a(ij)=a(j)
  b(ij)=b(j)
  a(j)=t
  b(j)=it
  t=a(ij)
  it=b(ij)
  if(a(i).le.t) go to 40
  a(ij)=a(i)
  b(ij)=b(i)
  a(i)=t
  b(i)=it
  t=a(ij)
  it=b(ij)
  go to 40
  30 a(1)=a(k)
  b(1)=b(k)
  a(k)=tt
  b(k)=itt
  40 l=l-1
  if(a(1).gt.t) go to 40
  tt=a(1)
  itt=b(1)
C split the data into a(i to l).lt.t, a(k to j).gt.t
  50 k=k+1

```

```

        if(a(k).lt.t) go to 50
        if(k.le.1) go to 30
        p=m
        m=m+1
C split the larger of the segments
        if(1-i.le.j-k) go to 60
        il(p)=i
        iu(p)=1
        i=k
        go to 80
    60 il(p)=k
        iu(p)=j
        j=1
        go to 80
    70 m=m-1
        if(m.eq.0) return
        i=il(m)
        j=iu(m)
C short sections are sorted by bubble sort
    80 if(j-i.gt.10) go to 10
        if(i.eq.1) go to 5
        i=i-1
    90 i=i+1
        if(i.eq.j) go to 70
        t=a(i+1)
        it=b(i+1)
        if(a(i).le.t) go to 90
        k=i
    100 a(k+1)=a(k)
        b(k+1)=b(k)
        k=k-1
        if(t.lt.a(k)) go to 100
        a(k+1)=t
        b(k+1)=it
        go to 90
    END
    SUBROUTINE starter(ntrees,dbh,age)
C *****
C This subroutine exchanges dbh and age information from temporary *
C arrays to the working arrays. This initially places the trees in *
C the simulation plot. *
C *****
        common/init/ ntrees0(7),dbh0(4000),ncount(20,7),nbins,width
    1 ,age0(4000),agein(20,7)
        common/limits/ mxtrs,maxspc,mxdd,mxyrs,maxbin
        common/oper/ ns,nspan,nruns,clrcut,nwrstr,ifire,sburn,ibr,impb
        integer clrcut,agein
        dimension ntrees(1),dbh(1),age(1)

        do 10 j= 1,ns
            ntrees(j)= ntrees0(j)
    10 continue

        do 20 j= 1,mxtrs
            dbh(j)= dbh0(j)
            age(j)=age0(j)
    20 continue
        return
    END
    SUBROUTINE tree(nl,crop,cblock)

```

```

C .....:
C This subroutine reads in species and fuel specific data for model sim- :
C lation area (NRM). Each input value is stored in appropriate COMMON :
C block or brought back to main driver. Each value is also printed in :
C a file on device 5 for proof of correct entry. Values are stratified :
C by species (dimensioned to seven) or fire group (dimensioned to eight)..:
C .....:
common/plotq/elev,rock,till,soilm,text,excess,pltsiz,ifg
common/limits/ mxtrs,maxspc,mxdd,mxyrs,maxbin
common/water/grws(7),ws0(7),wsm(7),nws(7),wr,grdd(7),grbar(7)
common/leaf/aside(7),c(7),alpha(7),b2(7),b3(7),cext(8),crat(7),
&
sigma(7),ap(7),betap(7)
common/trunk/g(7),agemx(7),dm(7),hm(7),spm(8),ysc(7)
common/hdata/phi,xmbar(8),degd,ainc(7),binfest(8),ibcycle(8),brr
common/climat/ dmin(7),dopt(7),dmax(7),baset(12),basep(12),baseh
common/birthk/sura(7),surb(7),dbulk(8,2),disequ(2,7),rdelay(8)
common/wbark/ cmax,agecon,dbhmin,birds, spc, spcac, cyr(4), fmax, cpt,
&
pfind,ssc
common/types/ishade(7),imoist(7),spp(7)
common/fuel1/ mext(2),rhop(2,7),bulk(2,8),mois(2,7)
common/fuel2/ mps(2,7),lhv(2,7),st(2,7),se(2,7)
common/fuel3/ dkl(7),dkd(7),dkf(7),ltd(7)
common/fuel4/ abm(7),ffl(7),fyr(3,8),fload(3,8)
common/fuel5/ amc(7),bmc(7),cmc(7),dmc(7),mmc(7),tmc,emc(7)
common/mort/ dl(7),d2(7),d3(7),bc(7)
common/polut/ndyr(7),dmoist
common/cfire/cbd(7),vfl(7),cfmc(7),vfmc(7),cflm(7),csvr(7),
&
vsvr(7),bl(7)
common/oper/ ns,nspan,nruns,clrcut,nwrstr,ifire,sburn,ibr,impb
integer clrcut,count,cblock(7),fyr
real mext,lhv,mmc,mps,ltd,mois,crop(7),cyr
character*10 mark,chr,name,spp*4
character*1 imoist,ishade
data mark/'$$$$$$$$$$'/

open(unit=2,file='TREE1.DAT',form='formatted',
& recl=150,pad='YES')

nl= 2
C ..... Find number of species
count= 0
10 count= count+1
read(2,1000,end=100) chr

if (chr.ne.mark) go to 10
rewind 2
ns= count-1
if (ns.gt.maxspc) call error(7)
C ..... Write header information
do 20 i= 1,ns
read(2,2000) spp(i)
write(5,2000) spp(i)
20 continue
write(5,1000) mark
read (2,1000) mark
read (2,3000) name, (hm(j),j=1,ns)
write(5,3000) name, (hm(j),j=1,ns)
read (2,3000) name, (dm(j),j=1,ns)
write(5,3000) name, (dm(j),j=1,ns)
read (2,3000) name, (agemx(j),j=1,ns)

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write(5,3000) name, (agemx(j),j=1,ns)
read (2,3000) name, (dmin(j),j=1,ns)
write(5,3000) name, (dmin(j),j=1,ns)
read (2,3000) name, (dopt(j),j=1,ns)
write(5,3000) name, (dopt(j),j=1,ns)
read (2,3000) name, (dmax(j),j=1,ns)
write(5,3000) name, (dmax(j),j=1,ns)
read (2,8000) name, (spm(j),j=1,8)
write(5,8000) name, (spm(j),j=1,8)
read (2,6000) name, (aside(j),j=1,ns)
write(5,6000) name, (aside(j),j=1,ns)
read (2,3000) name, (c(j),j=1,ns)
write(5,3000) name, (c(j),j=1,ns)
read (2,6000) name, (alpha(j),j=1,ns)
write(5,6000) name, (alpha(j),j=1,ns)
read (2,3000) name, (sigma(j),j=1,ns)
write(5,3000) name, (sigma(j),j=1,ns)
read (2,6000) name, (ap(j),j=1,ns)
write(5,6000) name, (ap(j),j=1,ns)
read (2,6000) name, (betap(j),j=1,ns)
write(5,6000) name, (betap(j),j=1,ns)
read (2,8000) name, (cext(j),j=1,8)
write(5,8000) name, (cext(j),j=1,8)
read (2,5000) name, (ishade(j),j=1,ns)
write(5,5000) name, (ishade(j),j=1,ns)
read (2,5000) name, (imoist(j),j=1,ns)
write(5,5000) name, (imoist(j),j=1,ns)
read (2,8000) name, (xmbars(j),j=1,8)
write(5,8000) name, (xmbars(j),j=1,8)
read (2,6000) name, (crat(j),j=1,ns)
write(5,6000) name, (crat(j),j=1,ns)
read(2,3000) name, mext(1)
write(5,3000) name, mext(1)
read(2,3000) name, (amc(k),k=1,ns)
write(5,3000) name, (amc(k),k=1,ns)
read(2,3000) name, (bmc(k),k=1,ns)
write(5,3000) name, (bmc(k),k=1,ns)
read(2,3000) name, (cmc(k),k=1,ns)
write(5,3000) name, (cmc(k),k=1,ns)
read(2,3000) name, (dmc(k),k=1,ns)
write(5,3000) name, (dmc(k),k=1,ns)
read(2,3000) name, (mmc(k),k=1,ns)
write(5,3000) name, (mmc(k),k=1,ns)
read(2,3000) name, tmc
write(5,3000) name, tmc
read(2,3000) name, (rhop(1,k),k=1,6)
write(5,3000) name, (rhop(1,k),k=1,6)
read(2,8000) name, (bulk(1,k),k=1,8)
write(5,8000) name, (bulk(1,k),k=1,8)
read(2,3000) name, (lhv(1,k),k=1,6)
write(5,3000) name, (lhv(1,k),k=1,6)
do 50 i = 1,ifg
    read(2,3000) name, (mps(1,k),k=1,6)
    if(i .eq. ifg) write(5,3000) name, (mps(1,k),k=1,6)
50 continue
do 60 i = 1,8-ifg
    read(2,1000) mark
60 continue
read(2,3000) name, (st(1,k),k=1,6)
write(5,3000) name, (st(1,k),k=1,6)

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```

read(2,3000) name, (se(1,k),k=1,6)
write(5,3000) name, (se(1,k),k=1,6)
read(2,4000) name, (dk1(k),k=1,ns)
write(5,4000) name, (dk1(k),k=1,ns)
read(2,4000) name, (ltd(k),k=1,ns)
write(5,4000) name, (ltd(k),k=1,ns)
read(2,4000) name, (dkf(k),k=1,ns)
write(5,4000) name, (dkf(k),k=1,ns)
read(2,4000) name, (dkd(k),k=1,ns)
write(5,4000) name, (dkd(k),k=1,ns)
read(2,4000) name, (ffl(k),k=1,ns)
write(5,4000) name, (ffl(k),k=1,ns)
read(2,4000) name, (dl(k),k=1,ns)
write(5,4000) name, (dl(k),k=1,ns)
read(2,3000) name, (d2(k),k=1,ns)
write(5,3000) name, (d2(k),k=1,ns)
read(2,3000) name, (d3(k),k=1,ns)
write(5,3000) name, (d3(k),k=1,ns)
read(2,3000) name, (bc(k),k=1,ns)
write(5,3000) name, (bc(k),k=1,ns)
read(2,3000) name, (rhop(2,k),k=1,nl)
write(5,3000) name, (rhop(2,k),k=1,nl)
read(2,3000) name, (bulk(2,k),k=1,nl)
write(5,3000) name, (bulk(2,k),k=1,nl)
read(2,3000) name, (lhv(2,k),k=1,nl)
write(5,3000) name, (lhv(2,k),k=1,nl)
read(2,3000) name, (mps(2,k),k=1,nl)
write(5,3000) name, (mps(2,k),k=1,nl)
read(2,3000) name, (st(2,k),k=1,nl)
write(5,3000) name, (st(2,k),k=1,nl)
read(2,3000) name, (se(2,k),k=1,nl)
write(5,3000) name, (se(2,k),k=1,nl)
read(2,3000) name, (mois(2,k),k=1,nl)
write(5,3000) name, (mois(2,k),k=1,nl)
read(2,7000) name, (ndyr(j),j=1,ns)
write(5,7000) name, (ndyr(j),j=1,ns)
read(2,4000) name, (ainc(j),j=1,ns)
write(5,4000) name, (ainc(j),j=1,ns)
read(2,3000) name, (ws0(k),k=1,ns)
write(5,3000) name, (ws0(k),k=1,ns)
read(2,3000) name, (wsm(k),k=1,ns)
write(5,3000) name, (wsm(k),k=1,ns)
read(2,7000) name, (nws(k),k=1,ns)
write(5,7000) name, (nws(k),k=1,ns)
read(2,4000) name, (sura(j),j=1,ns)
write(5,4000) name, (sura(j),j=1,ns)
read(2,4000) name, (surb(j),j=1,ns)
write(5,4000) name, (surb(j),j=1,ns)
read(2,8000) name, (dbulk(j,1),j=1,8)
write(5,8000) name, (dbulk(j,1),j=1,8)
read(2,8000) name, (dbulk(j,2),j=1,8)
write(5,8000) name, (dbulk(j,2),j=1,8)
read(2,8000) name, sburn
write(5,8000) name, sburn
read(2,4000) name, (crop(j),j=1,ns)
write(5,4000) name, (crop(j),j=1,ns)
read(2,7000) name, (cblock(j),j=1,ns)
write(5,7000) name, (cblock(j),j=1,ns)
read(2,4000) name, (ysc(j),j=1,ns)
write(5,4000) name, (ysc(j),j=1,ns)

```

```

read (2,4000) name,(disequ(1,j),j=1,ns)
write(5,4000) name,(disequ(1,j),j=1,ns)
read (2,4000) name,(disequ(2,j),j=1,ns)
write(5,4000) name,(disequ(2,j),j=1,ns)
do 70 i = 1,3
    read (2,9000) name,(fyr(i,j),j=1,8)
    write(5,9000) name,(fyr(i,j),j=1,8)
70 continue
do 80 i = 1,3
    read (2,8000) name,(fload(i,j),j=1,8)
    write(5,8000) name,(fload(i,j),j=1,8)
80 continue
read (2,3000) name,(cbd(i),i=1,ns)
write(5,3000) name,(cbd(i),i=1,ns)
read (2,3000) name,(vfl(i),i=1,ns)
write(5,3000) name,(vfl(i),i=1,ns)
read (2,3000) name,(cfmc(i),i=1,ns)
write(5,3000) name,(cfmc(i),i=1,ns)
read (2,3000) name,(vfmc(i),i=1,ns)
write(5,3000) name,(vfmc(i),i=1,ns)
read (2,3000) name,(cflm(i),i=1,ns)
write(5,3000) name,(cflm(i),i=1,ns)
read (2,3000) name,(csvr(i),i=1,ns)
write(5,3000) name,(csvr(i),i=1,ns)
read (2,3000) name,(vsvr(i),i=1,ns)
write(5,3000) name,(vsvr(i),i=1,ns)
read (2,3000) name,(bl(i),i=1,ns)
write(5,3000) name,(bl(i),i=1,ns)
read (2,8000) name,(binfest(i),i=1,8)
write(5,8000) name,(binfest(i),i=1,8)
read (2,9000) name,(ibcycle(i),i=1,8)
write(5,9000) name,(ibcycle(i),i=1,8)
read (2,8000) name,(rdelay(i),i=1,8)
write(5,8000) name,(rdelay(i),i=1,8)

do 90 i = 1,ns
    if(spp(i) .eq. 'pial') then
        read(2,9100) name,cmax,agecon,dbhmin,birds,spc,spcac,
&                pfind,(cyr(j),j=1,4),fmax,cpt,ssc
        write(5,9100) name,cmax,agecon,dbhmin,birds,spc,spcac,
&                pfind,(cyr(j),j=1,4),fmax,cpt,ssc
        go to 99
    endif
90 continue
99 close(2)
return

100 call error(8)
close(2)
return

```

C ##### FORMATS #####

```

1000 format(a10)
2000 format(a4)
3000 format(a10,7f10.3)
4000 format(a10,7f10.4)
5000 format(a10,7(9x,a1))
6000 format(a10,7f10.7)
7000 format(a10,7i10)

```



```

8000 format(a10,7f10.4,/,10x,f10.4)
9000 format(a10,7i10,/,10x,i10)
9100 format(a10,7f10.1,/,10x,7f10.4)
END
SUBROUTINE wrstrs
C ::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::
C This subroutine computes the growth reduction factor due to      :
C water stress. This is a value between 0 and 1 and is stored    :
C in the array GRWS(i).                                         :
C ::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::
common/oper/ ns,nspar,nruns,clrcut,nwrstr,ifire,sburn,ibr,impb
common/water/grws(7),ws0(7),wsm(7),nws(7),wr,grdd(7),grbar(7)
common/hdata/phi,xmbar(8),degd,ainc(7),binfest(8),ibcycle(8),brr
common/climat/ dmin(7),dopt(7),dmax(7),baset(12),basep(12),baseh
integer clrcut

do 10 i=1,ns

C ..... Calculate growth reduction factor for water stress
      if(nwrstr .ne. 0) then
        grws(i)=1.- ( (wsm(i)-wr)/(wsm(i)-ws0(i)) )**nws(i)
        if(grws(i).lt.0.0) grws(i)=0.0
      else
        grws(i) = 1.0
      endif

C ..... Calculate climatic reduction factor using degree-days
      if(degdeg .gt. dmin(i) .and. degdeg .lt. dmax(i)) then
        v = (dmax(i) - dopt(i)) / (dopt(i) - dmin(i))
        grdd(i) = ((degdeg - dmin(i)) * (dmax(i)-degdeg)**v) /
&                (((dmax(i)-dopt(i))**v) * (dopt(i) - dmin(i)))
      else
        grdd(i) = 0.0
      endif

10 continue
return
END
FUNCTION isum(vect,n)
C *****
C This function sums all items in vector VECT from 1 to n and    *
C returns the summed number stored in variable ISUM.            *
C *****
integer vect(n)
isum= 0
if (n.le.0) return
do 10 j= 1,n
  isum= isum+vect(j)
10 continue
return
END
FUNCTION risk(ck,dbh,j)
C ::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::
C : Function RISK computes the probability of death from fire for :
C : tree under consideration. Equation is from Ryan and Rheinhardt :
C : (1986). Also presented is Bevins (1978) equation for small re- :
C : generation. Major variables are:                               :
C : d1,d2,d3 ... coefficients for one year mortality equation     :
C : bc(j) ..... thickness of bark in cm                           :
C : c1,c2,c3,c4 ... coefficients for exponential equation.         :

```

```

C ::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::
      common/mort/ d1(7),d2(7),d3(7),bc(7)
      data d0/12.7/
      data r/10./,c1/1.466/,c2/-1.914/,c3/0.1792/,c4/0.000535/

C ..... Calculate the constants in the mortality equation
      a0 = d1(j)
      a1 = d2(j)*bc(j)
      a2 = d3(j)
      b0 = alog(r)+a0
      b1 = a1+2.*alog(r)/d0
      b2 = -alog(r)/d0**2

C ..... Mortality equation from Ryan and Rhienhardt 1986
      risk= 1./(1.+exp(-(c1+c2*bc(j)*dbh+c3*
&          (bc(j)*dbh)**(2.0)+c4*ck**(2.0))))

C *****
C ..... Previous mortality equation for trees under 5 in DBH ***
C      if (dbh.lt.d0) risk= 1.-1./(1.+exp(b0-b1*dbh-b2*dbh**2.0 *
C      &          +a2*hs)) *
C *****
      return
      END
      FUNCTION sum(vect,n)
C ::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::
C : Function SUM adds real elements 1 to n of an array.           :
C ::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::
      real vect(n)
      sum= 0.
      if (n.le.0) return
      do 10 j= 1,n
          sum= sum+vect(j)
      10 continue
      return
      END
      FUNCTION itable(t)
C ::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::
C This function computes the various properties of air at a      :
C specified temperature level.                                   :
C ::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::::
      if(t .ge. 0.0 .and. t .lt. 250.0) itable = 1
      if(t .ge. 250.0 .and. t .lt. 300.0) itable = 2
      if(t .ge. 300.0 .and. t .lt. 350.0) itable = 3
      if(t .ge. 350.0 .and. t .lt. 400.0) itable = 4
      if(t .ge. 400.0 .and. t .lt. 450.0) itable = 5
      if(t .ge. 450.0 .and. t .lt. 500.0) itable = 6
      if(t .ge. 500.0 .and. t .lt. 550.0) itable = 7
      if(t .ge. 550.0 .and. t .lt. 600.0) itable = 8
      if(t .ge. 600.0 .and. t .lt. 650.0) itable = 9
      if(t .ge. 650.0 .and. t .lt. 700.0) itable = 10
      if(t .ge. 700.0 .and. t .lt. 750.0) itable = 11
      if(t .ge. 750.0 .and. t .lt. 800.0) itable = 12
      if(t .ge. 800.0 .and. t .lt. 850.0) itable = 13
      if(t .ge. 850.0 .and. t .lt. 900.0) itable = 14
      if(t .ge. 900.0 .and. t .lt. 950.0) itable = 15
      if(t .ge. 950.0 .and. t .lt. 1000.0) itable = 16
      if(t .ge. 1000.0 .and. t .lt. 1100.0) itable = 17

```

```
if(t .ge. 1100.0 .and. t .lt. 1200.0) itable = 18
if(t .ge. 1200.0 .and. t .lt. 1300.0) itable = 19
if(t .ge. 1300.0 .and. t .lt. 1400.0) itable = 20
if(t .ge. 1400.0) itable = 20
return
END
```

APPENDIX B: PRINTOUT OF THE EXTERNAL INPUT FILE TREE.DAT, WHICH CONTAINS VARIOUS SPECIES AND SITE PARAMETERS FOR EQUATIONS IN FIRESUM

Variables not defined in text are described in Keane and others (1989a) and Keane and others (1989b).

pip							
abgr							
psme							
pico							
laoc							
abla							
pien							
\$\$\$\$\$\$\$\$							
hm	6562.500	5333.700	5715.000	4115.000	6857.500	4175.700	5456.700
dm	250.500	139.400	208.840	110.000	250.000	126.700	234.400
agemx	450.000	275.000	350.000	220.000	450.000	180.000	320.000
dmin	2249.900	2496.600	1810.400	1215.300	1817.400	801.800	801.400
dopt	4010.000	4200.000	4200.000	4200.000	4200.000	3800.000	4200.000
dmax	8608.000	7194.000	7194.000	6500.000	7194.000	6200.000	6200.000
spm	1.000	3.000	6.000	2.000	4.000	3.000	5.000
spm-cont	5.000						
aside	3.5400000	2.040000	2.850000	3.5400000	3.5400000	2.040000	2.0400000
c	2.074	1.608	1.582	1.882	1.679	1.255	1.710
alpha	0.2680000	1.3090000	1.1370000	0.1220000	0.4370000	7.3450000	1.0400000
sigma	57.600	72.900	69.100	64.700	184.000	70.000	54.200
ap	0.5580000	1.5920000	0.4840000	0.4930000	0.3470000	0.5970000	0.5780000
betap	-0.0475000	0.0590000	-0.0210000	0.0117000	-0.0434000	-0.0425000	-0.0325000
cext	0.4260	0.5250	0.5250	0.4260	0.4260	0.4260	0.4260
cext cont	0.525						
ishade	I	T	M	I	I	T	M
imoist	T	I	T	T	I	I	I
xmbar	0.0071	0.0089	0.0149	0.0074	0.0091	0.0107	0.0083
xmbar cont	0.0111						
crat	0.4000000	0.800000	0.800000	0.4000000	0.4000000	0.800000	0.8000000
mext	.250						
amc	1.651	1.651	1.651	1.651	1.651	1.651	1.651
bmc	0.493	0.493	0.493	0.493	0.493	0.493	0.493
cmc	19.350	19.350	19.350	19.350	19.350	19.350	19.350
dmc	10.880	10.880	10.880	10.880	10.880	10.880	10.880
mmc	.320	.320	.320	.320	.320	.320	.320
tmc	24.000						
rhop	.510	.390	.390	.390	.510	.510	.510
bulk	0.0158	0.0088	0.0068	0.0080	0.0115	0.0071	0.0126
bulk cont	0.0080						
lhv	18586.700	18586.700	18586.700	18586.700	18586.700	18586.700	18586.700
mps-fg1	57.410	8.890	3.480	0.950	3.156	91.8560	3.0000
mps-fg2	57.410	11.760	2.880	0.980	3.156	91.8560	3.0000
mps-fg3	57.410	16.000	3.077	0.980	3.156	91.8560	3.0000
mps-fg4	57.410	16.000	3.077	0.980	3.156	91.8560	3.0000
mps-fg5	57.410	16.000	3.077	0.980	3.156	91.8560	3.0000
mps-fg6	57.410	16.000	3.077	0.980	3.156	91.8560	3.0000
mps-fg7	57.410	11.760	2.880	0.980	3.156	91.8560	3.0000
mps-fg8	57.410	11.760	2.880	0.980	3.156	91.8560	3.0000
st	.055	.055	.055	.055	.055	.055	.055
se	.010	.010	.010	.010	.010	.010	.010
dkl	.1116	.0667	.1167	.1116	.2000	.0667	.0667
ltd	.5500	.6500	.6550	.6600	.8500	.6500	.6500
dkf	.0575	.0339	.0339	.0440	.1310	.0339	.0339
dkd	.2210	.2210	.2210	.2210	.3210	.2210	.2210

ffl	.1200	.1200	.1200	.1200	.1200	1.0000	.1200
d1	.1688	.1688	.1688	.1688	.1688	.1688	.1688
d2	1.969	1.969	1.969	1.969	1.969	1.969	1.969
d3	.306	.306	.306	.306	.306	.306	.306
bc	.070	.033	.065	.014	.071	.015	.022
rhop	0.513	0.513					
bulk	0.001	0.001					
lhv	18595.000	18595.000					
mpe	49.200	91.860					
st	.055	0.055					
se	.010	0.010					
mois	1.000	1.500					
ndyr	4	7	5	3	1	7	6
ainc	0.0120	0.0050	0.0070	0.0150	0.0160	0.0080	0.0080
ws0	.25	.47	.32	.38	.38	.65	.65
wsm	1.	1.	1.	1.	1.	1.	1.
nws	2	2	2	2	2	2	2
sura	10.5900	40.0100	38.6900	14.1200	20.1700	40.0100	40.0100
surb	2.7400	5.1150	4.2400	2.2800	5.5900	6.1150	6.1150
dbulk(1,i)	15.8000	36.2000	41.6000	21.9000	25.3000	35.0000	43.3000
cont	38.1000						
dbulk(2,i)	76.9000	76.9000	145.7900	76.9000	110.6300	110.6300	139.4800
cont	142.7000						
sburn	0.7500						
crop	0.3950	0.3330	0.4460	0.3180	0.3680	0.3330	0.1670
cblock	2	2	1	2	2	2	3
ysc	20.0000	25.0000	20.0000	15.0000	25.0000	25.0000	25.0000
disequ(1j)	13.1251	13.4099	14.1251	12.6760	14.3257	13.4099	12.7470
disequ(2j)	0.0255	0.0183	0.0222	0.0376	0.0148	0.0183	0.0251
fyr-lhr	40	40	40	40	30	30	40
fyr-lhr	50						
fyr-10hr	40	40	40	40	30	30	40
fyr-10hr	50						
fyr-100hr	40	40	40	40	30	30	40
fyr-100hr	50						
fload-lhr	0.0210	0.1350	0.2710	0.0638	0.0520	0.0520	0.1776
fload-lhr	0.0748						
fload-10hr	0.0833	0.2650	0.1548	0.2619	0.1879	0.1879	0.4294
fload-10hr	0.1960						
fload100hr	0.1546	1.6475	0.1055	0.5484	0.5635	0.5635	4.7022
fload100hr	0.5459						
cbd	1.106	0.577	0.304	1.202	1.042	.000	.000
vfl	1.058	0.593	0.561	0.721	0.529	.000	.000
cfmc	1.050	1.050	1.050	1.050	1.050	.000	.000
vfmc	.100	.100	.100	.100	.100	.000	.000
cflm	1.000	1.000	1.000	1.000	1.000	.000	.000
csvr	60.700	64.700	184.000	72.900	54.200	.000	.000
vsvr	10.000	20.000	10.000	30.000	30.000	.000	.000
bl	0.1	0.10	0.1	0.100	0.100	0.100	0.100
binfest	0.660	0.800	0.800	0.450	0.640	0.660	0.440
bin(cont)	0.800						
ibcycle	10	10	10	10	10	10	10
ibcycle c	10						
rdelay	10.000	25.000	8.000	11.000	12.000	8.000	15.000
rdelay	20.000						
cmax	600.0	60.0	20.0	3.0	58.8	3.7	0.800
icyr	0.3521	0.4673	0.7823	1.0000	7.0	60.0	0.120
end							

APPENDIX C: PRINTOUT OF THE EXTERNAL INPUT FILE SITE.DAT, WHICH CONTAINS VARIOUS SITE PARAMETERS FOR EQUATIONS IN FIRESUM

Variables not defined in text are described in Keane and others (1989a) and Keane and others (1989b).

```

baset      17.8 21.1 23.5 31.7 40.1 51.0 64.0 63.0 55.0 38.9 26.5 21.4
basep      6.12 4.69 3.90 4.10 3.65 2.81 1.92 2.56 2.00 2.94 4.38 5.62
baseh      8000.000
excess     0.250
phi        1.000
text       133.300          site = Sabe Mountain
rock       0.100
elev       7200.000
ifg        2
till       3.000
rh         40.00
wind       3.200
ttheta    0.26
t          19.000
pltsiz    400.000
emc        0.080          0.080          0.080          0.080          0.100          0.080          0.100
dmoist     0.7500
brr        0.01
END

```

**APPENDIX D: PRINTOUT OF THE EXTERNAL INPUT FILE CONTRL.DAT,
WHICH CONTAINS VARIOUS INITIAL STAND PARMETERS THAT ARE USED
TO CREATE THE SIMULATION STAND IN FIRESUM**

Variables not defined in text are described in Keane and others (1989a) and Keane and others (1989b).

```

nspan      500
nruns      5
clear cut  0
ifire      600
iblist     600
ibeetle    600
dsize      20.0  20.0  20.0  20.0  20.0  20.0  20.0
nwrstr     1
nbins      10
width      5.0
count 1    18    0    0    4    0
count 2     3    0    0    1    0
count 3     3    0    0    0    0
count 4     3    0    0    0    0
count 5     6    0    0    0    0
count 6     7    0    0    0    0
count 7     3    0    0    0    0
count 8     3    0    0    0    0
count 9     0    0    0    0    0
count10    2    0    0    0    0
age 1      38    0    0    65   0
age 2     96    0    0    53   0
age 3     60    0    0    0    0
age 4     70    0    0    0    0
age 5    300    0    0    0    0
age 6    250    0    0    0    0
age 7    350    0    0    0    0
age 8    370    0    0    0    0
age 9     0    0    0    0    0
age 10   450    0    0    0    0
END

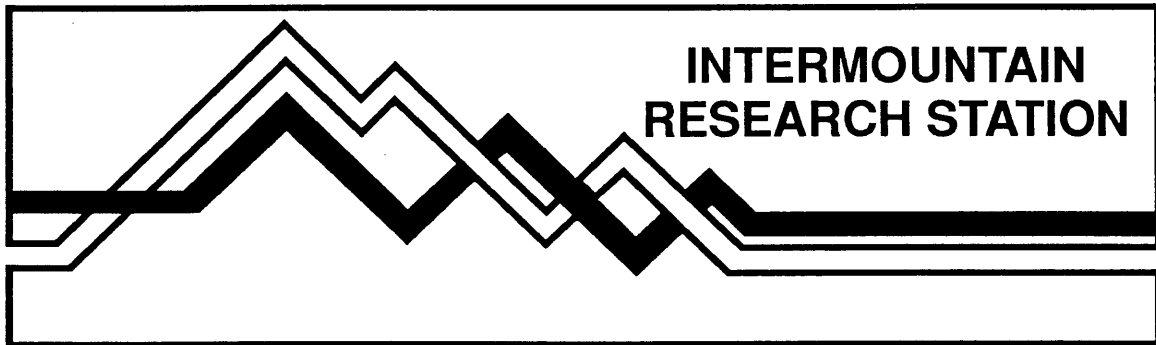
```

SITE: ONE HORSE RIDGE CLIMAX STAND

Keane, Robert E.; Arno, Stephen F.; Brown, James K. 1989. FIRESUM—an ecological process model for fire succession in western conifer forests. Gen. Tech. Rep. INT-266. Ogden, UT: U.S. Department of Agriculture, Forest Service, Intermountain Research Station. 76 p.

Describes an ecological process model of succession that simulates long-term stand dynamics in forests of the Northern Rocky Mountains. This model is used to evaluate the effects of various fire regimes, including prescribed burning and fire suppression, on the vegetation and fuel complex of a simulation stand. This report documents the model FIRESUM (a **FIRE SU**ccession Model), examples of model output, and sensitivity analysis and validation results.

KEYWORDS: fire effects, fire regime, succession, documentation, computer program, wildland fire, fire management, fire ecology, forest succession, fire effects, fire regime



The Intermountain Research Station provides scientific knowledge and technology to improve management, protection, and use of the forests and rangelands of the Intermountain West. Research is designed to meet the needs of National Forest managers, Federal and State agencies, industry, academic institutions, public and private organizations, and individuals. Results of research are made available through publications, symposia, workshops, training sessions, and personal contacts.

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